

THE NLC L-BAND BUNCH COMPRESSOR*

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Abstract

The first stage bunch compressor in the NLC injector complex compresses the e⁺/e⁻ beams from a bunch length of 5 mm rms to 0.5 mm rms at the beam energy of 2 GeV. To obtain this compression ratio, the compressor rf section operates with an rf frequency of 1.4 GHz and a voltage of about 140 MV while a magnetic wiggler is used to generate an $R_{56} = 0.5$ m. The bunch compressor is designed to operate with a beam from the damping ring that has a bunch spacing slew of 20ps across the bunch train due to the transient loading in the damping rings. The compressor RF section is required to produce a specific energy profile along the bunch train so that the bunch spacing can be corrected in the compressor bending section. Further, the 1-amp beam heavily loads the compressor linac and beam loading compensation is essential to prevent a phase variation along the bunch train in the downstream linacs. In this paper, we will present simulation results of the beam loading compensation using a ΔT scheme assuming various initial bunch spacing arrangements. We will study the impact of the different compressor energy profiles on the beam energy, energy spread, and bunch length at the IP.

1 INTRODUCTION

The NLC bunch compressor is a two-stage system [1] designed to compress each bunch of a 95-bunch train from a length of 5 mm at 2-GeV damping ring (DR) extraction energy, to a 90- μ m rms bunch length at the beam interaction point (IP). The two-stage system includes L-band, S-band, and X-band RF components and has been designed to be relatively insensitive to extraction phase errors initiated in the damping rings [2]. The system is shown schematically in Figure 1.

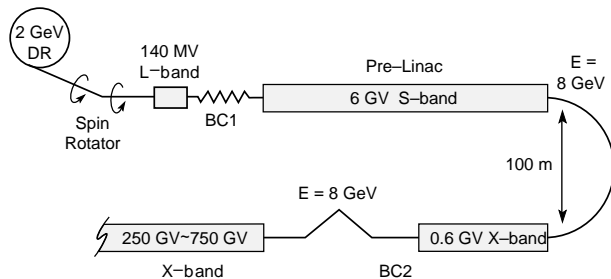


Figure 1. NLC compressor system.

The first stage of compression (BC1) is effected using a short L-band linac followed by a 10-bend wiggler. The L-band linac accelerates the beam at an RF phase of 102

degrees off crest to produce an approximately linear energy correlation of 1% rms along the bunch. The magnetic wiggler, with an R_{56} of 0.485-m, compresses the bunch length from 5-mm to 0.5-mm. The BC1 system effectively rotates the longitudinal phase space of the beam 90 degrees, converting the long bunch-length into a finite energy spread. Table 1 lists the parameters of the first stage compressor system.

Table 1. Parameters of first compression stage.

Parameter	symbol	Value	unit
bunch population	N	7.5	10^9
bunches/train	N_b	95	
bunch spacing	Δt_b	2.8	ns
ring energy	E	1.98	GeV
DR rms energy spread	$\sigma_{\delta DR}$	0.1	%
DR rms bunch length	$\sigma_{z DR}$	5.0	mm
final rms bunch length	σ_z	0.5	mm
final rms energy spread	σ_δ	1.0	%
length of L-band RF	L	10	M
voltage of L-band RF	V	139	MV
phase of L-band RF	ϕ	102	Deg
frequency of L-band	f	1428	MHz
R_{56} of wiggler	R_{56}	0.485	M

The compressor wiggler or chicane converts energy deviations into bunch spacing errors and vice versa. In the heavily loaded compressor linacs, it is essential to implement effective beam loading compensation schemes to remove unwanted energy deviations due to the beam loading. In addition, the BC1 compressor system is required to operate with beams from the damping ring that have a bunch spacing slew of 20-ps across the bunch train. The compressor RF section is required to produce a specific energy profile along the bunch train so that the bunch spacing errors will be corrected in the compressor wiggler section, preventing phase deviations in the downstream linacs.

The second stage of compression (BC2), consisting a X-band linac followed by a chicane, compresses the bunch length from 0.5-mm to 90- μ m at 8-GeV. The design issues in the BC2 are similar as in the BC1 and will not be covered here. In this paper, we will present a design for the first stage compressor. We will study the effects of the BC1 on the IP parameters by tracking the beams produced by the BC1 system through the whole linac. In these tracking studies, the BC2 was treated as an ideal system. This assumption was validated in separate

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studies with a design of the BC2 that meets the requirements.

2 THE BC1 COMPRESSOR LINAC

The first stage compressor linac is composed of two L-band (1.428 GHz) accelerator structures, which are identical to the e^+ booster accelerator structures[3], to produce a compression voltage of 140-MV along the bunch train. The linac is heavily loaded by a beam current of 1-Ampere. The beam loading energy spread must be compensated since the bunch-to-bunch energy variation will be converted into bunch spacing, or RF phase, errors by the wiggler. Unlike in the accelerator linacs, the beams in the compressor linac are approximately in phase quadrature with the RF. Under nominal operation conditions, the RF voltage does not provide compensation to the beam loading.

2.1 Beam loading compensation schemes

The natural choice for beam loading compensation for the compressor linac is the ΔF method. However, this method requires an additional off-frequency RF system, which adds extra cost and complications.

In the present design, we adopted a ΔT compensation scheme. In the ΔT scheme, both phase and amplitude modulations are needed on the RF input. The phase modulation introduces an “in-phase” component of voltage to the beam that compensates the loading voltage, while the amplitude modulation is to produce the flat compression voltage along the bunch train. To obtain a phase-amplitude modulated RF waveform, we need to combine two klystrons running at different phases, but full in RF power for stability. The phase modulation of each klystron is done at low power RF control. A schematic of the ΔT scheme using two phase-modulated klystrons is shown in Figure 2.

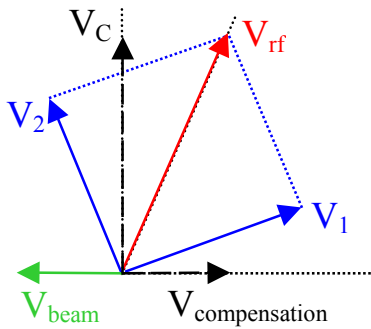


Figure 2. A schematic of ΔT beam loading compensation.

The low frequency linacs in the NLC (L-band e^+ booster linac and S-band pre-linacs) are powered by SLED-I[4] pulse compression systems. Although a SLED-I pulse compression system should work just fine for the compressor linacs, it is found that a pair of klystrons alone can provide enough power to drive the two accelerator sections to produce the 140-MV

compression voltage. Without SLED-I pulse compression, the klystrons are required to provide 74-MW of power and 1.5- μ s of pulse length. As a comparison, the system with SLED-I pulse compression would require 37-MW in klystron power and 5.5- μ s in pulse length. Without pulse compression, the system is more efficient and cost effective, and is simpler to operate. The RF configuration of the L-band compressor linac is shown in Figure 3.

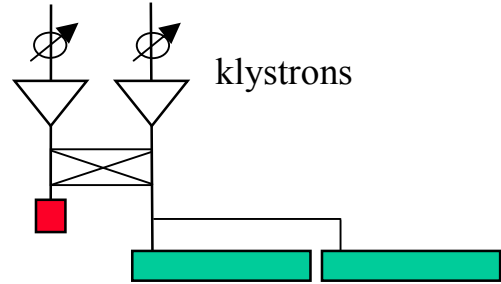


Figure 3. The L-band compressor RF configuration.

2.2 RF profile for nominal bunch spacing

We first optimize the RF profile for a beam with nominal bunch spacing. In the present design, the bunches are about 102 degrees off RF crest, which induces a small non-linearity term in the bunch energy profile to compensate the higher order terms (T566) in the wiggler lattice. At this phase, the RF decelerates the beam slightly in the compressor linac. After the beam is injected at one filling time (1- μ s) of the structure, the beam loading adds to the deceleration effect. The phase of the input RF is therefore moved toward “acceleration” to cancel the beam-loading field. In addition, the amplitude of the RF is lowered accordingly to maintain a flat compression voltage.

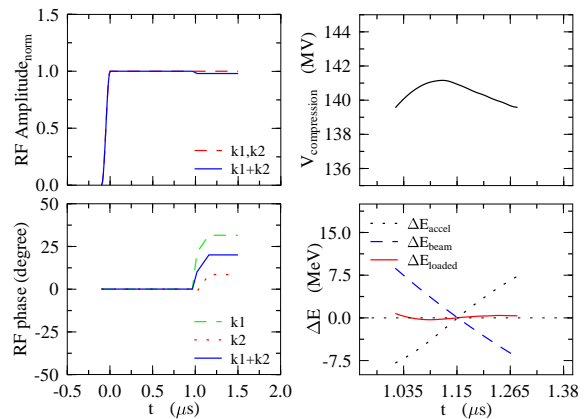


Figure 4. Beam loading compensation for the L-band compressor linac. Left: the RF pulse profile; Right: the compression voltage and energy deviation along the bunch train.

In Figure 4 are shown the RF profiles, the compression voltage and the energy deviation after compensation for a beam with nominal bunch spacing. The compression

voltage of 140-MV is achieved with two 74-MW klystrons. The deviation of the compression voltage is less than $\pm 1\%$. The bunch-to-bunch energy deviation is within a fraction of a MeV. The phase modulation on the klystrons is small and is obtainable using phase control at low power.

2.3 Single and multi bunch energy profiles

The initial 20-ps bunch-spacing slew causes the bunches to be accelerated on different RF phases. The phase span ($\Delta\psi$) due to this spacing slew (across the whole train) is one forth of the phase span of a single bunch. The energy distribution along the bunch train in the $\Delta\psi$ frame is the same as the energy profile of a single bunch. So that the bunch spacing error can be corrected the same manner as bunch length compression. An additional effect of the non-nominal bunch spacing is the phase slippage between beam loading fields of individual bunches, which results in additional non-linearity to the beam loading profile and may require additional effort to compensate. With the present beam parameters, this effect has been shown to be small in the L-band system. One can apply the same RF waveform as optimized for the nominal beams to the NLC damping ring beams.

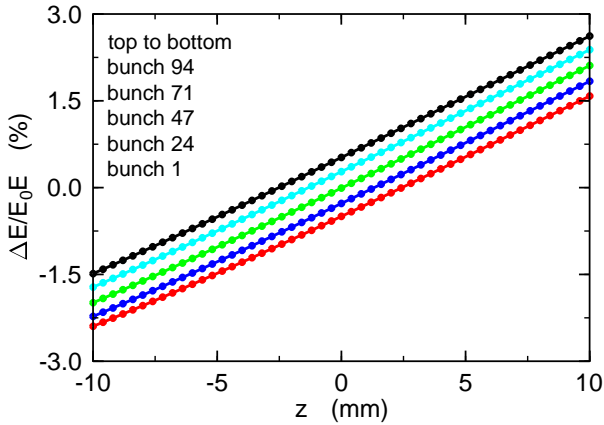


Figure 5. Energy profiles of five selected bunches along the bunch train.

Figure 5 shows the energy correlations of five bunches along the bunch train. The energy shifts among these curves are due to initial spacing errors. These shifts are converted into spacing adjustments by the wiggler, which corrects the spacing error at the exit of the compressor. As a result, there is no phase error in the S-band pre-linacs.

3 SIMULATION RESULTS

The stability of the longitudinal parameters over the bunch train at the IP have been studied by simulating the effect of the transient beam loading in the ring, with the added loading compensation. The nominal bunch is shown in Figure 6. The 95-bunch train is ‘stretched’ or ‘contracted’ by 17-ns (5-mm) at ring extraction and five representative bunches (1, 25, 48, 72, and 95) are tracked

through the entire system. The final IP energy, energy spread, bunch length, and arrival ‘time’ are shown versus bunch number in Figure 7.

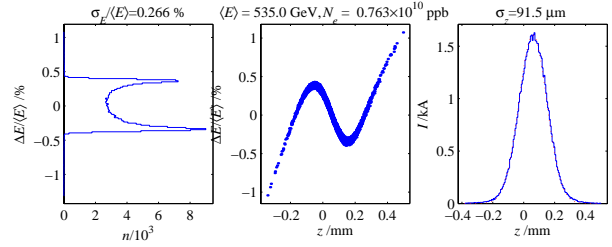


Figure 6. Energy spread (left), phase space (center), and temporal distribution (right) at IP at 535 GeV.

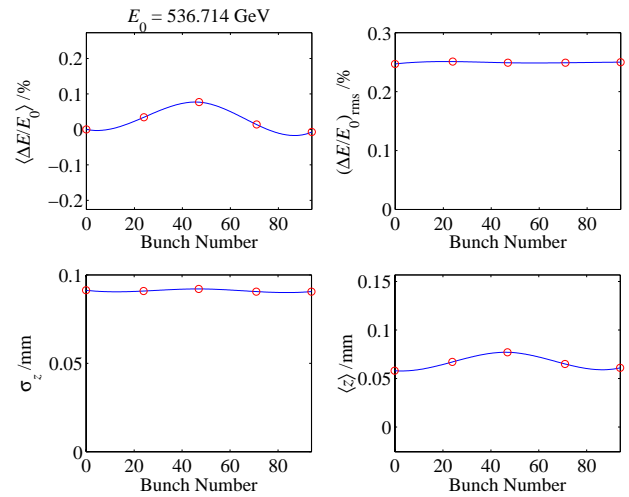


Figure 7. Final IP energy (top left), energy spread (top right), bunch length (bottom left), and relative arrival ‘time’ (bottom right) are shown versus bunch number.

The energy is constant over the train to a level of $<0.1\%$, while the energy spread and bunch length are almost unaffected. The arrival ‘time’ of the bunch varies by <36 -fsec (<12 - μm) which is $\sim 10\%$ of the bunch length and should have no significant effect.

4 REFERENCES

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