

## PERFORMANCE of the CRID at SLD\*

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### Abstract

This paper describes the performance of a large  $4\pi$  Cherenkov Ring Imaging Detector (CRID) in the SLD experiment at the SLC at SLAC. We compare the most recent SLD results with those obtained during the R&D period, discuss various design features, and highlight some specific lessons derived from three years of operation.

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## 1. INTRODUCTION

The concept of the CRID at SLD benefited from the pioneering work of J. Seguinot and T. Ypsilantis.<sup>1</sup> The design is similar to that of the DELPHI<sup>2</sup> RICH and both groups benefited from each other's work. The early R&D development of CRID was summarized in ref.3.

In this paper we describe the performance of the barrel portion of the CRID detector. By making use of both liquid and gaseous radiators in the Barrel CRID,  $\pi/K/p$  separation will be possible up to about 30 GeV/c, and  $e/\pi$  separation up to about 6 GeV/c.

## 2. CRID DESIGN FEATURES

Fig.1 shows the basic CRID geometry, and more detail about its electrostatic design can be found in ref.4. The CRID includes 40 TPC's, 40 liquid radiator trays containing liquid  $C_6F_{14}$ , a vessel containing 76%  $C_5F_{12}$ +24%  $N_2$  gas radiator, and a system of 400 spherical mirrors.<sup>5</sup> The Cherenkov photons are focused into the TPC's as shown in Fig.2. The photoelectron drifts to a wire chamber where its position is reconstructed using a combination of drift time (z-coordinate), wire address (x-coordinate) and charge division (y-coordinate) with a precision of 1x1x2 mm. The expected Cherenkov angles are  $3.04^\circ$  and  $38.5^\circ$  ( $\beta = 1$  particle) with expected resolutions of 4-5 and 12-15 mrad for gas and liquid rings respectively, and on average 7-9 and 13 -16 photoelectrons are expected on gas and liquid rings respectively - see chapter 3.11 for  $N_0$  estimate. The TPC gas is  $C_2H_6$ + TMAE(~0.1%). The maximum drift length is 1.2 m, and the maximum operating voltage is 55 kV giving a drift field of 400 V/cm. The system operates at 33-35°C with the TMAE bubbler temperature set at 26°C. The system has 3720 anode wires, 7440 amplifiers, 64000 field shaping electrodes and 6520 corona preventing field wires.

We are presently commissioning the End Cap portion of the CRID which will be described in a future publication. It will operate with a  $C_4F_{10}$  gas radiator only, and includes 10 TPC's and 120 mirrors. The TPC gas is 85%  $C_2H_6$ +15%  $CO_2$ +TMAE(~0.1%); the maximum drift length is 28 cm; and the maximum voltage is 15 kV, giving a 400 V/cm drift field. The system has 1280 anode wires.

## 3. REVIEW OF THE SYSTEM PERFORMANCE

### 3.1. Overall experience

Here, we highlight a few major issues where we differ from other CRID/RICH devices now in operation.

To define the drift field in the TPC's we decided to use a simple geometry with field cage wires rather than a volume degrader. Our experience so far at SLD with the high voltage is excellent indicating that it is not necessary to build a volume degrader for voltages up to 60 kV and distances of 8-10 cm to ground, provided that a gas with good dielectric properties fills the volume.

We also decided to require that the detectors be easily removable for repairs. However, it is well known that TMAE attacks most elastomers. Our choice of Viton O-rings<sup>6</sup> has proven to be satisfactory. After 3 years of TMAE operation, we have not seen any deterioration of the O-ring.

The electrodes on two sides of the TPC were made of G-10 with copper traces. It was necessary to coat the G-10 surface with a TMAE resistant epoxy to prevent possible outgassing. The epoxy had to have a sufficiently low surface and volume resistivity to prevent charging effects. We found that most epoxies reduce their resistivity by almost two orders of magnitude if the temperature is increased from 20° to 40°C.<sup>4,7</sup> This has led to a choice of DP-190 epoxy which gives  $10^{12} \Omega/\text{sq.}$  at 40°C.

Early R&D showed that the presence of TMAE in the gas increases the wire aging rates by a significant factor - see section 3.5. We have implemented a system of nA-meters to monitor the current far below the capability of a typical commercial power supply.<sup>4,8</sup> If the SLC background exceeds a certain limit, causing a current 6 nA per detector, the high voltage is automatically reduced to 80%. This limits accumulation of large charge doses. In principle, such a system could also avoid damage due to Malter currents.<sup>9</sup> One detector developed such a current after ~2 years exposure to TMAE in the 1992 run. The current was observed only in the presence of gating (when gating is on, the positive ions travel toward the gating wire plane<sup>4</sup>). When TMAE was removed from the gas the problem went away. The Malter effect is a particular problem for the "CRID type" of detector operating with TMAE, because unlike all other wire detectors, we cannot add any substantial amount of water or alcohol to our gas (for example, the SLD drift chamber has 0.4% water in the gas mixture). TMAE becomes highly resistive as its purity is increased.

Since 1991 we have broken several 7  $\mu\text{m}$  carbon wires and, of course, this has caused concern. On the other hand, the use of high resistance wire (~40 k $\Omega$ /10 cm) makes the chamber very stable, because the wire acts as an impedance in the initial spark formation.

### 3.2. Design of the single electron detector.

Fig.3a shows the design of the single electron detector. It is based on single stage wire amplification. To prevent the avalanche photons from entering the TPC

drift volume, a system of Cu-Be blinds was constructed.<sup>4</sup> To have a good electron transmission to the anode wire, we run a ratio between the drift field within the detector and the drift field in the TPC of close to 6. This makes the structure relatively insensitive to misalignments.<sup>10</sup> For the CRID detector condition, UV photons are created by three carbon excitations<sup>11</sup> - see Fig.3b. The measured rate of afterpulses per avalanche caused by the secondary avalanche photons is less than 1% at our operating point.<sup>4</sup> It depends on the total avalanche charge and not on the electric field near the wire.<sup>4</sup> The Cu-Be blind structure gives us a factor of 7-8 reduction in the rate of the afterpulses - see Fig.3c. Although we block the avalanche photons efficiently with our blinds and prevent them from reaching the active drift volume, they are still generated and can reach the cathode surfaces to create photoelectrons (it takes 10 cm of gas to absorb the C\*-1561 A<sup>0</sup> line). This could contribute to the detector instability, if  $\eta G > 1$  ( $\eta$  is ratio of photo-electrons per avalanche electron and G is the wire gain).<sup>12</sup> The fact that the system of 3720 anode wires has been stable for more than 2 years of TMAE operation proves that our design and its operating point are sound.

### 3.3. Charge division performance.

One needs to measure the y-coordinate along the depth of the drift box to limit the broadening of the photon detection resolution - see Fig.4a. In our case we use charge division to determine this depth. Figs.4b,c show the effect of including charge division on the Cherenkov rings using cosmic rays at SLD. From Figs.4d,e we conclude that the correction for the depth coordinate gives us an improvement in the Cherenkov angle resolution of about 40%.

Fig.5 shows a schematic model of the variables involved in the charge division measurement. The charge division resolution can be calculated from the following formula<sup>13</sup>:

$$\left(\frac{\sigma_z}{\ell}\right) \cong \sqrt{\left(\frac{\sigma_j}{Q_{L+R}^{vis}}\right)^2 + \left(\frac{\sigma_{amp}/\sqrt{2}}{Q_{L+R}^{vis}}\right)^2 \left[\left(\frac{R_{wire} + 2R_{contact} + 2r_{amp}}{R_{wire}}\right)^2 + \left(\frac{2z}{\ell}\right)^2\right]}, \quad (1)$$

where

$$\sigma_j = 2.718 \sqrt{\frac{kT\tau}{2(R_{wire} + 2R_{contact} + 2r_{amp})}}$$

$$\sigma_{amp} \cong 2.718 \sqrt{\frac{kTR_{eq}(C_{in} + C_{ch})^2}{2\tau}}$$

In eq.(1), k is the Boltzmann constant; T is absolute temperature;  $\tau$  is the amplifier shaping time (65 ns);  $R_{eq}$  is the equivalent noise resistance of the FET

( $\sim 50 \Omega$ );  $C_{in}$  is the amplifier input capacitance ( $\sim 10$  pf);  $C_{ch}$  is the detector capacitance ( $\sim 15$  pf);  $Q_{L+R}^{vis}$  is the visible charge ( $1-2 \times 10^5$  el.);  $R_{wire} = 41.3 \pm 2.64$  k $\Omega$ ;  $R_{contact} = 94.6 \pm 116 \Omega$ ; and  $r_{amp} = 680 \pm 50 \Omega$ . For typical choices of the amplifier parameters the Johnson noise dominates the problem, so that one needs to use a wire of about 25 k $\Omega$ /10 cm of wire length and a gas gain  $G \sim 2 \times 10^5$  to reach 1% resolution. In practice, we had only two choices of wires, the 7  $\mu$ m carbon wire and the 33  $\mu$ m carbon wire ( $R_{wire} \sim 5.2$  k $\Omega$ /10 cm).<sup>13</sup> Using equation (1), one gets  $\sigma_j \sim 960$  electrons (with  $\sigma_{amp} \sim 530$  electrons) for the first wire, and  $\sigma_j \sim 2480$  electrons for the second wire.<sup>13</sup> R&D tests indicated  $\sigma_z / \ell \sim 0.7\%$  for the first wire, and 1.4% for the second.<sup>4,13</sup> This lead us to choose the 7  $\mu$ m carbon wire, even though the thinner wire is substantially weaker and more difficult to handle. Unfortunately, the final amplifier layout had worse noise performance ( $\sigma_{amp} \sim 1600$  electrons), somewhat weakening the argument. Fig.6a shows the R&D test performance with the 7  $\mu$ m wire. Fig.6b compares the R&D test data with the calculation using the equation (1) - the dashed line shows the calculated results while the solid line is also corrected for the UV gun source width. Fig.6c shows the present SLD performance as obtained using the inclined UV calibration fibers. We get about 2.2 mm for the final resolution after subtracting 1 mm in quadrature due to the source width. The resolution is indeed dominated by the electronics noise ( $\sim 1.7$  mm).<sup>14</sup> If it were not for the wire aging we could increase the wire gain slightly and obtain better results. Other contributors to the charge division resolution are the amplifier gain calibration, amplifier input impedance variation, contact resistance to the carbon wire,<sup>13,15</sup> wire nonuniformity, and wire gain variations.

The overall noise performance of the whole system at SLD is about 2000 electrons. At this noise level a 33  $\mu$ m carbon wire would provide almost the same resolution. The 33  $\mu$ m wire would also allow a larger decoupling cathode capacitor resulting in about half the cross-talk.<sup>16</sup>

### 3.4. Electronics performance.

Since the CRID electronics has a number of novel features compared to other detectors,<sup>17</sup> it is worthwhile discussing a few points in detail. We placed the amplifiers, analog storage, ADC's and a control and multiplexing circuitry on the detector. Only a few serial optical fibers lead to the Fastbus located in the electronics control room. Fig.7 shows the amplifier design. It is based on JFETs and Plessey 3703 semicustom chips. To simplify the deconvolution analysis,<sup>18</sup> it uses RC-CR timing resulting in an exponential pulse waveform response with a shaping time of 65 ns. The amplifier charge gain is about 2.7  $\mu$ V /electron. To limit the heating problems,

all components use pulsed power except the first JFET. The analog storage (HAMU) needs to be calibrated every few days; the amplifier gain is calibrated once per run. The essential requirement of a charge division system is the ability to perform amplifier gain calibrations accurately. Equation (2) shows the variables in the problem ( $g_i$  are the amplifier gains).

$$y = \frac{g_1 Q_1 - g_2 Q_2}{g_1 Q_1 + g_2 Q_2} \frac{R_{\text{wire}} + 2(r_{\text{amp}} + R_{\text{contact}}) \ell}{R_{\text{wire}}} \frac{\ell}{2} \quad (2)$$

To be able to determine the  $g_i$  constants accurately, we actively laser trimmed the resistor in the calibration circuit (R90 in Fig.7) to equalize the response of the amplifier to calibration circuit and the real inputs to 1%.

Equation (3) describes the shape of the single electron pulses by convoluting the amplifier response and the positive ion response<sup>13,19</sup> :

$$C(t) = \int_0^t [t' \exp(-\frac{t'}{\tau})] (\frac{1}{t-t'+t_0}) dt' = \exp(-\frac{t+t_0}{\tau})(t+t_0) \quad (3)$$

$$\times \{ \ln(1 + \frac{t}{t_0}) + \sum_{n=1}^{\infty} (\frac{t_0}{\tau}) \frac{1}{n \cdot n!} [(1 + \frac{t}{t_0})^n - 1] \} - \tau [1 - \exp(-\frac{t}{\tau})]$$

The data agree very well with equation (3) (with  $t_0 = 0.1$  ns) as one can see in Fig.8, which shows the results of an R&D test done with CH<sub>4</sub> gas and a 7  $\mu$ m diameter anode wire.

The amplifier-detector combination has cross-talk at a level of +1.1% in the first neighbor and about -0.25% for a distant neighbor.<sup>18</sup> This may seem small, but a typical charged track deposits about 1000 electrons in the TPC so that the cross-talk problem becomes significant. The amplifier response is complicated for very large pulses. Fig.9a shows the amplifier response to a charge of about  $3 \times 10^7$  electrons. The amplifier recovery to such charges creates spurious pulses and also affects the measurement of real pulses as one can see in Fig.9b. This is a major complication to the CRID analysis in the core of jets where many tracks overlap. We are still working on various cleaning algorithms.

The ability of our electronics to measure the pulse waveforms has many advantages. Fig.10 shows a complicated event involving a spiraling electron. Such analysis would probably have been impossible with conventional digital electronics.

### 3.5. Wire aging.

Since the complete waveforms are recorded, wire aging can be studied by monitoring the average single electron pulse height using the UV fibers. Fig.11a shows results of our R&D tests.<sup>20</sup> The TMAE molecule<sup>21</sup> is very susceptible to

polymerization because of its double bond structure between carbons and the relative fragility of its other constituents. The prediction from the R&D tests was that a modest detector current of about 5-10 nA would cause a 50% gain drop in about 1-2 years. Fig.11b shows the wire aging at SLD indicating about a 15% gain drop in two years, a result consistent with the R&D data (a typical current 2-4 nA per detector).

To regenerate the wire gain we have shown in R&D tests that we can either wash the detectors with alcohol<sup>20,22</sup> or evaporate the deposits by heating the carbon wires.<sup>16</sup> Because of this problem, we run the detectors at as low a wire gain as possible (average gain at  $1-2 \times 10^5$ ), which worsens the charge division performance slightly.

### 3.6. Distortions due to positive ions.

Fig.12a shows a schematic of the R&D test setup with a laser to measure the distortions induced by positive ions created by a UV lamp.<sup>23</sup> Figs.12b,c show distortions due to the attraction of the drifting electrons by the positive ions located uniformly throughout the TPC volume for two values of the ion concentrations. Fig.12d shows that gating can eliminate the distortions by preventing the positive ions from entering the TPC volume. In the SLD, we monitor this type of distortion by observing the x-coordinate of the UV fiber located at a side of the TPC - see Fig.12e. Fig.12f indicates that we have not seen any change in the distortions due to positive ions at a level of 1 mm during the last run.

### 3.7. Distortions due to the radial magnetic field component $B_r$ .

Fig.13 shows the measured mean positions of UV fiber hits together with the expected position (solid line) in the x-y plane. Fig.13a shows the pattern of the UV fibers located near the detector for the magnet being off. This and other similar studies<sup>4,23,24</sup> indicate that the distortions for field off are at a level of 1-2 mm at worst. Fig.13b shows the same pattern from UV fibers located at the high voltage end of the TPC with the magnet on. The measured positions of the fibers have clearly shifted from the expected field off positions. To understand this, we calculate the distortion for the  $B_r$  component of the magnetic field using the following method. We start with a general equation describing the drift velocity :

$$\vec{v} = \frac{\mu}{1 + (\omega \tau)^2} \left[ \vec{E} + \frac{\omega \tau}{B} [\vec{E} \times \vec{B}] + (\omega \tau)^2 \frac{\vec{E} \cdot \vec{B}}{B^2} \vec{B} \right] \quad (4)$$

We assume the following initial conditions :

$$\vec{B}(0, B_r, B_z), \vec{E}(0, 0, E_z), B = |\vec{B}| \approx B_z, B_r(r, z) = B_r^0 \frac{r z}{r_0 z_0}.$$

After appropriate integration we obtain the following corrections :

$$\Delta y = \frac{(\omega \tau)^2}{1 + (\omega \tau)^2} K r (z_1^2 - z_0^2)$$

$$\Delta x = \frac{\omega \tau}{1 + (\omega \tau)^2} K r (z_1^2 - z_0^2)$$
(5)

where  $z_1$  is the fiber z-position at the high voltage end;  $z_0$  is the z-position of the entrance to the detector;  $\mu$  is electron mobility;  $\omega$  is the Larmor frequency;  $\tau$  is the mean time between collisions;  $K$  is a constant; and the result is  $\Delta x \sim 9.9$  mm and  $\Delta y \sim 8.6$  mm. If one makes the  $B_r$  correction using equations (5), one gets good agreement between the reconstructed and expected position of the UV fibers - see Fig.13c. (on the north side it was necessary to introduce an additional systematic correction by rotating all detectors by a few mm about the beam line).

### 3.8. TPC gas purity.

The  $C_2H_6$  gas is cleaned in the standard way,<sup>25</sup> i.e., we use mechanical filters, Oxisorbs<sup>26</sup> and 13X molecular sieves<sup>27</sup>. In addition, we use electropolished stainless steel tubing as is common practice in Silicon Valley industry. However, U.S. suppliers of ethane have sulfur contamination problems. The sulfur impurity level varies depending on which oil well is used. As much as 200 ppm of sulfur has been reported. The sulfur can exist in ethane as elemental sulfur,  $CS_2$ ,  $H_2S$ ,  $SO_2$  and  $COS$ . Our initial ethane supply was contaminated at a level of only 1-3 ppm, but that was enough to completely plug up the pressure regulator after one year of operation. We are now using a nickel getter<sup>28</sup> to remove this contaminant. It is delivered with  $CO_2$  to stabilize it. It is then purged with hydrogen gas at elevated temperature to remove the  $CO_2$  in order to activate the nickel. Fig.14a shows that the drift velocity dropped when the nickel cartridge was introduced into the system. This may be explained by the presence of only 0.25% of  $CO_2$  in the ethane gas<sup>29</sup>. One can also see day-to-night variations in the drift velocity. There was also a small release of oxygen over a period of time prompting us to introduce another Oxisorb cartridge. Nevertheless, as one can see in Fig.14b, we did achieve our goal precision for the drift velocity of less than 0.1%. This experience illustrates that some very active substances used in modern cleaning filters can give rise to very complicated chemistry. One possible solution for this particular problem is to buy sulfur-free ethane in Europe.

The TMAE is cleaned by the CRID group by (a) washing it with deionized water, (b) filtering through silica gel and 3A and 5A molecular sieves, and (c) pumping<sup>32</sup> it at about 20 Torr for 2-6 hours. This operation resulted in a reproducible production of good quality TMAE by removing various contaminants, including TMO, which is



soluble in water (it has 40x times higher electron capture rates compared to oxygen<sup>30</sup>). Before the TMAE is used in the TPC's, it is "certified" in a small ionization chamber.<sup>31</sup> During the run we rely primarily on the self-monitoring of each TPC by measuring an average TPC z-coordinate formed from single electron pulses and plotting it as a function of time.

Fig.15 shows the photon absorption length in TMAE as measured by various people. Our measurements, using both gas rings and a UV lamp, agree with data of Anderson,<sup>32</sup> perhaps because everyone integrates over the peak in the absorption coefficient at 1900 Å.

### 3.9. Gas radiator purity.

Our gas radiator recirculation system operates as a heat engine. This was not originally intended, but it was realized that this technique stabilizes the purity. The returning gas mix from the vessel enters a -80°C tank where the C<sub>5</sub>F<sub>12</sub> liquefies and the N<sub>2</sub> gas is vented (requiring about 1 kW in cooling power). The C<sub>5</sub>F<sub>12</sub> liquid is then evaporated again and mixed with the N<sub>2</sub> gas. The overall flow is one complete change every 10-11 hours. In parallel, the C<sub>5</sub>F<sub>12</sub> liquid is circulated through a system of silica gel<sup>33</sup>, elemental copper<sup>34</sup>, and Oxisorb filters. The logic is that the silica gel protects the other filters<sup>35</sup>. We do not regenerate any of these cartridges because of the fear of the possible dissociation of freon molecules during the heating process. We still have the original 1993 set of cartridges in place 5 months after the start of the 1993 run. Fig.16 shows the UV transmission of a sample taken from the -80°C tank during the run (solid line). The dashed curve indicates the transmission of a sample taken after the tank warmed up at the end of the 1992 run. A subsequent analysis of this sample by the 3M company indicated 84.3% C<sub>5</sub>F<sub>12</sub>, 11.6% C<sub>6</sub>F<sub>14</sub>, 1.01% C<sub>7</sub>F<sub>16</sub>, 1.87% C<sub>8</sub>F<sub>18</sub>, and 1.22% of some other fluorocarbon. Our tests indicate that neither C<sub>7</sub>F<sub>16</sub> nor C<sub>8</sub>F<sub>18</sub> are responsible for the loss of transmission. Therefore, it is the unknown fluorocarbons or other trace components which are likely to be responsible for the loss of transmission. During a run, C<sub>8</sub>F<sub>18</sub> and heavier liquids are frozen in the -80°C tank and kept there until it is warmed up at the end of the run. Similarly, at the end of the run we have found a heavy fluorocarbon (possibly C<sub>17</sub>F<sub>30</sub>) at the bottom of the evaporator. Therefore, we believe that the simple distillation and freezing cycle in our heat engine recirculation system helps to maintain the required purity of the radiator gas.

Our typical oxygen level in the vessel is 5 ppm and the water level is 40-50 ppm. The gas radiator mixture is continuously monitored by sonar.<sup>35</sup>

### 3.10. Liquid radiator purity.

Fig.17a,b shows our liquid radiator purity during the run. The dashed curve indicates what happens if we stop the recirculation for a long time period. The liquid is initially de-oxygenated and purified by bubbling N<sub>2</sub> gas through it. During the run, the liquid is purified by pumping it through an Oxisorb cartridge. The recirculation flow is one radiator volume every 2 hours. The Oxisorb is changed every 3 months. In this system the Oxisorb is not protected by silica gel. In view of recent findings in the DELPHI group,<sup>37</sup> perhaps this could be a mistake in the long run. However, we do know that 3M Co. uses silica gel to clean the liquid before shipping, and our experience to date is satisfactory.

### 3.11. Approximate estimate of N<sub>0</sub>.

Fig.18 shows some components of the efficiency for the transport and the conversion process into photoelectrons. They are derived from a collection of efficiencies either measured during the construction period (transmission of quartz, mirror reflectivity and TMAE quantum efficiency<sup>11,38</sup>), efficiencies measured during the run (UV transmission of fluorocarbons, oxygen and water effects), and estimates for other factors such as absorption by the field cage wires, chamber efficiencies, and electron lifetime. The resulting final efficiency is shown by the open circles in Fig.18, and is then integrated as a function of wavelength to estimate N<sub>0</sub>. The final estimated N<sub>0</sub> is 56-66 cm<sup>-1</sup> for the gas rings and 32-42 cm<sup>-1</sup> for the liquid rings (if the gaps between TPC's are not taken into account the latter number increases to 45-55 cm<sup>-1</sup>). The range of estimated N<sub>0</sub> depends on the assumptions, such as, for example, what TMAE quantum efficiency is used<sup>11,38</sup>. This method does not include effects such as confusion in the middle of jets (and small electron losses due to the Lorentz angle in the liquid rings). Therefore, it is expected to be most useful for simple events, such as cosmic rays, di-muons, Bhabhas, etc. Such data appear to support more optimistic values for N<sub>0</sub>. For example, for the cosmic rays we observe : 17-18 photo-electrons per full liquid ring, and ~8 per gas ring, which implies N<sub>0</sub> = 45 cm<sup>-1</sup> for liquid and 63 cm<sup>-1</sup> for gas.

## 4. RESULTS AT SLD

Fig.19 shows liquid rings from hadronic Z<sub>0</sub> events. The present background situation can be understood from Fig.20, where we show the effect of removing different background hits : (a) corresponds to all photoelectron hit candidates; (b) also includes removing hits with a long TMAE absorption length; and (c) includes the

cross-talk and amplifier recovery cleaning cuts. One can see that the last cut removes a significant amount of background, but also removes signal hits. It is still being refined. The local Cherenkov angle resolution per photon is about 12 mrad, close to the design value; however, we still have about 10 mrad of systematic errors due to various global misalignments. Fig.21 shows the first attempt at particle identification using fitted liquid rings.

Fig.22 shows gas rings in the hadronic  $Z_0$  events. We get about 7-8 photoelectrons per ring, and the local resolution with respect to the ring is close to the design value of 4-5 mrad (FWHM). Again, we still are dealing with systematic alignment errors at a level of 10 mrad.

## 5. WHAT DID WE LEARN ?

One can summarize briefly what we have learned during the CRID development (For the benefit of newcomers to this field we would like to stress that some items were far from obvious when we started) :

1. Single electron detection on a large scale is possible.
2. Charge division on single electrons works.
3. It is possible to build a 60 kV system without a field degrader.
4. Positive ion distortions during SLD data taking have not yet been seen.
5. TMAE wire aging does indeed exist, and the rate is consistent with R&D results.
6. Glues and materials selected during the R&D phase have behaved as predicted. Long electron lifetimes can be maintained.
7. It is possible to make a large system which is leak tight to less than 1 ppm of oxygen level, which is needed in the TPC's.
8. Fluorocarbons can be cleaned and recirculated.
9. Ethane can have a sulfur contamination; active surfaces of the filters, such as nickel, can introduce complicated chemistry problems.
10. Given the noise performance in a large system, we could have used the 33  $\mu\text{m}$  carbon wire instead of 7  $\mu\text{m}$  carbon wire. It would improve the mechanical integrity of the anode wires.
11. A substantial technical effort is required to keep the system operational for many years.
12. The thick TPC causes very large  $dE/dx$  deposits to which the amplifier responds in rather complicated ways; in retrospect, a logarithmic amplifier response might have avoided some of these problems.

13. It takes a large effort to tune the software analysis to obtain even minimal performance in a large  $4\pi$  CRID detector.

**FIGURE CAPTIONS :**

1. Schematic of the SLD barrel CRID.
2. Principle of photoelectron detection in the barrel CRID.
3. (a) Geometry of the single electron detector; (b) sensitivity to carbon excitation lines in CRID; (c) rate of afterpulses as a function of total visible charge in the avalanche with and without blinds.
4. Equivalent model of charge division and its variables.
5. (a) Principle of parallax broadening of the image due to depth of the TPC; liquid rings (b) with and (c) without charge division; and resulting Cherenkov angle resolution (d) with and (e) without the charge division information (about 40% worse) .
6. (a) Measured R&D results on charge division resolution in  $C_2H_6$  gas with  $7\ \mu m$  diameter carbon wires at cathode voltage  $V_C = -1.55\ kV$ ;<sup>13</sup> (b) Measured R&D results integrated over all pulse heights on a single photoelectron as a function of z-coordinate along the wire on  $7\ \mu m$  ( $\square$ ) and  $33\ \mu m$  ( $\Delta$ ) wires;<sup>13</sup> calculation done using equation (1) assuming the average visible charge of  $2.25 \times 10^5$  and  $2.5 \times 10^5$  electrons for both types of wires (dashed lines include  $400\ \mu m$  beam size); and (c) present SLD measured charge division result on the system of 3700 wires at  $V_C = -1.50\ kV$  (it includes  $1\ mm$  contribution from the UV fiber beam size).
7. CRID amplifier circuit including the calibration circuit with the laser trimmed resistor (R90).
8. 11. (a) The average measured single electron pulse shape obtained with  $7\ \mu m$  wires in  $CH_4$  gas;<sup>13</sup> (b) Comparison of an average measured test pulse shape ( $\Delta$ ) and the calculated amplifier response  $t \exp(-t / \tau)$  (solid line), and the average single-electron measured pulse shape ( $\square$ ) and its calculated shape (dashed line) using eq.(3).<sup>13</sup>
9. (a) Response of the amplifier to very large pulses ( $3 \times 10^7$  electrons); and (b) spurious points on the Cherenkov ring due to the amplifier recovery and/or its effect on real pulses.
10. Power of waveform readout utilizing charge division to disentangle complicated events; (a,b) signal from the two wire ends; and (c) reconstructed spiraling track.

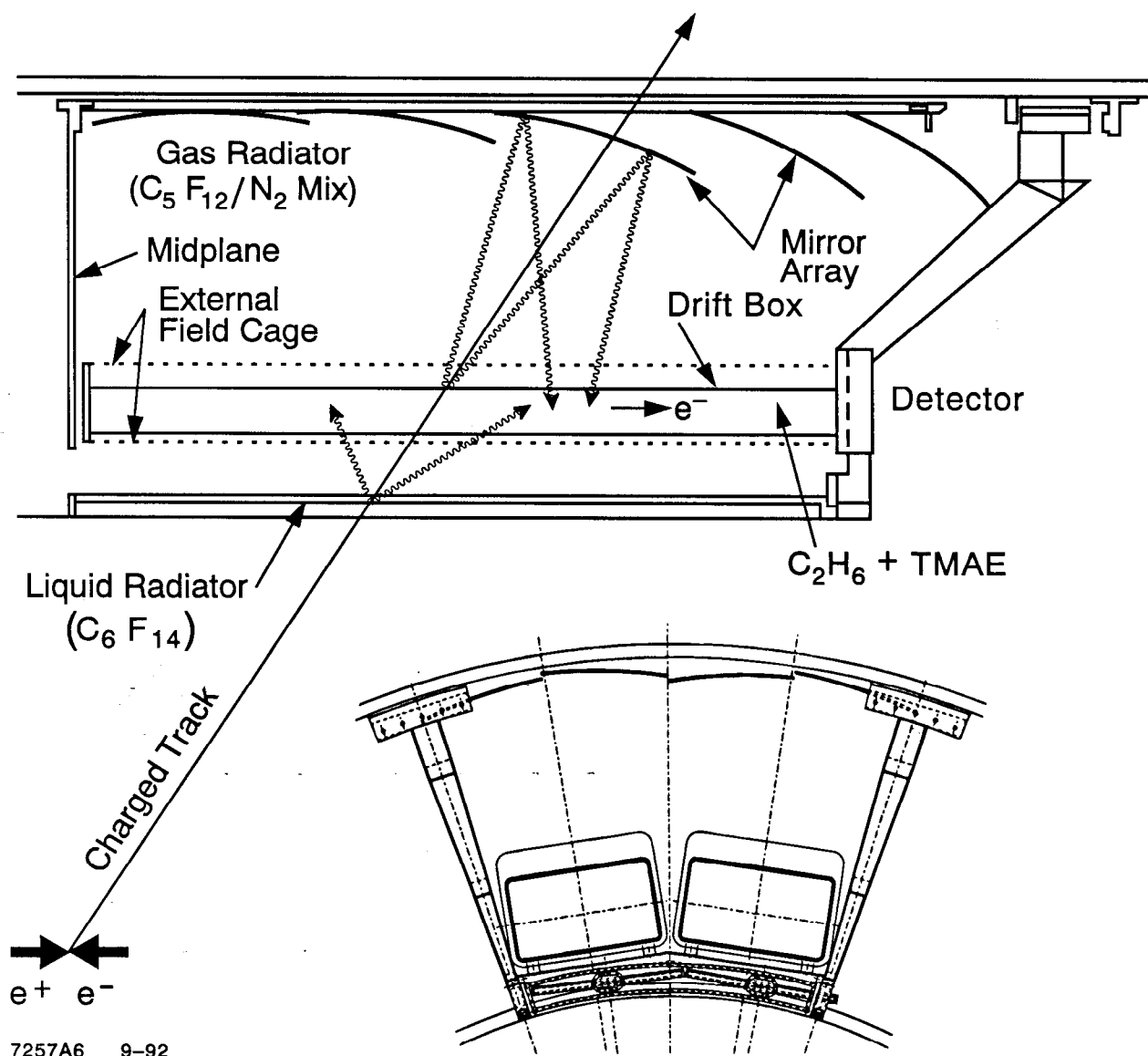
11. Measured wire aging rate using 7  $\mu\text{m}$  diameter carbon wires with TMAE during :
  - (a) R&D tests<sup>20</sup> (CRID uses  $\text{C}_2\text{H}_6$  gas - ( $\Delta$ ) points); and (b) the SLD results (15% gain drop in two years of running).
12. R&D tests : (a) Distortion of a laser track due to positive ions for (b)  $0.5 \times 10^6$  ions/ $\text{cm}^3$ ; (c)  $2.5 \times 10^6$  ions/ $\text{cm}^3$ ; (d) as (b), but with the gating on; SLD performance : (e) distortion of UV fiber x-coordinate due to positive ions; (f) its time history (no effect at 1 mm level seen).
13. Measured mean position of UV fibers in the SLD with magnet off : (a) fibers at the detector end; and with the magnet on : (b) before ( $\Delta x \sim 9.9$  mm,  $\Delta y \sim 8.6$  mm); and (c) after the correction for the  $B_r$  effect.
14. (a) Drift velocity in  $\text{C}_2\text{H}_6 + \text{TMAE}$  measured in the TPC's before and after the introduction of the nickel filter to remove the sulfur contamination (data are consistent with a model<sup>29</sup> that 0.25% of  $\text{CO}_2$  is causing the drift velocity drop); (b) a spline fit indicating that the 0.1% precision in the drift velocity monitoring was achieved.
15. Photon absorption in TMAE as a function of the TMAE bubbler temperature from various sources including CRID.
16. Measured UV transmission in 1 cm liquid  $\text{C}_5\text{F}_{12}$  during the CRID operation (solid line), and after the  $-80^\circ\text{C}$  tank warmed up at the end of run (dashed line).
17. (a) Measured UV transmission in 1 cm liquid  $\text{C}_6\text{F}_{14}$  during CRID operation (solid line), and effect of epoxy outgasing when circulation stopped for many hours (dashed line); and (b) time history of the UV transmission at 1800  $\text{A}^\circ$  indicating the CRID purity stability in the 1993 run.
18. CRID final estimated efficiency (open circles) for (a) gas and (b) liquid rings; several examples of the main efficiency factors also included (TMAE quantum efficiency taken from ref.37, other factors taken from either SLD monitoring or the R&D test data).
19. (a) Full and (b) half liquid rings integrated over many hadronic  $Z_0$  events taken by CRID at SLD (all cleaning cuts applied to data).
20. Typical photoelectron background in the liquid rings in the hadronic  $Z_0$  events (a) before cuts; (b) after TMAE depth cut; (c) as (b), but also include the electronics cross-talk and recovery cleaning cuts.
21. The first attempts to do particle identification using the liquid rings in hadronic  $Z_0$  events by CRID at SLD.

22. (a) Gas rings integrated over many hadronic  $Z_0$  events; (b) ring radius with typical photoelectron background; (c) average number of photoelectrons per ring; and (d) typical local resolution in respect to a ring.

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Fig. 1



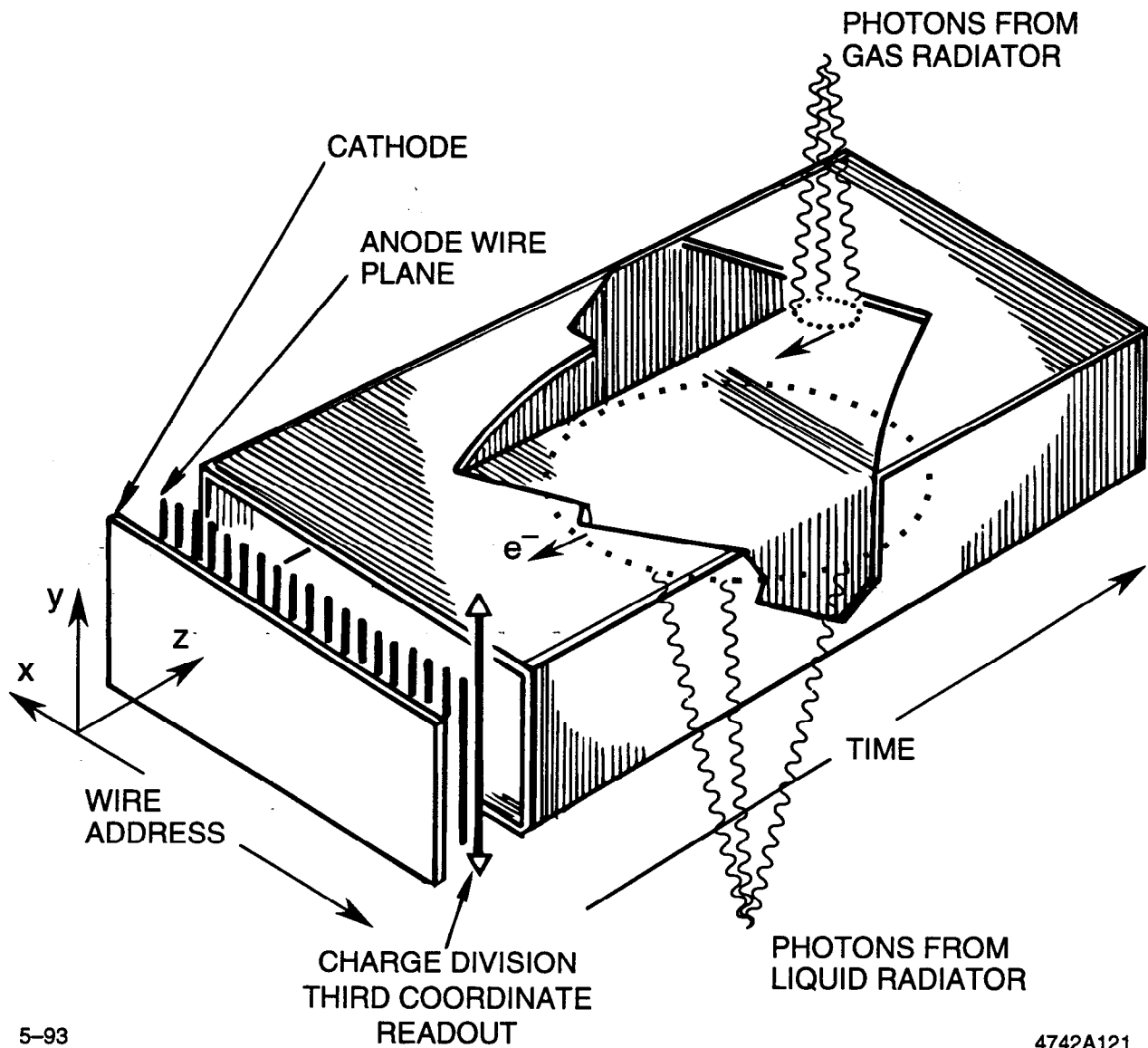
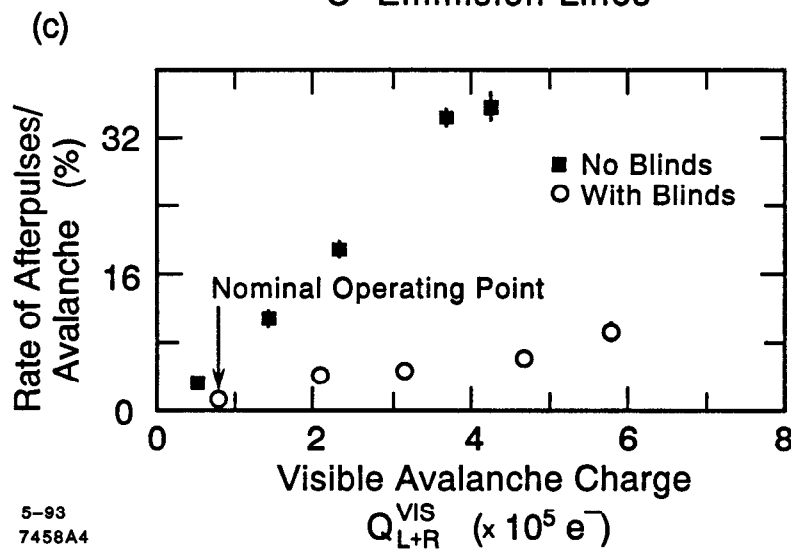
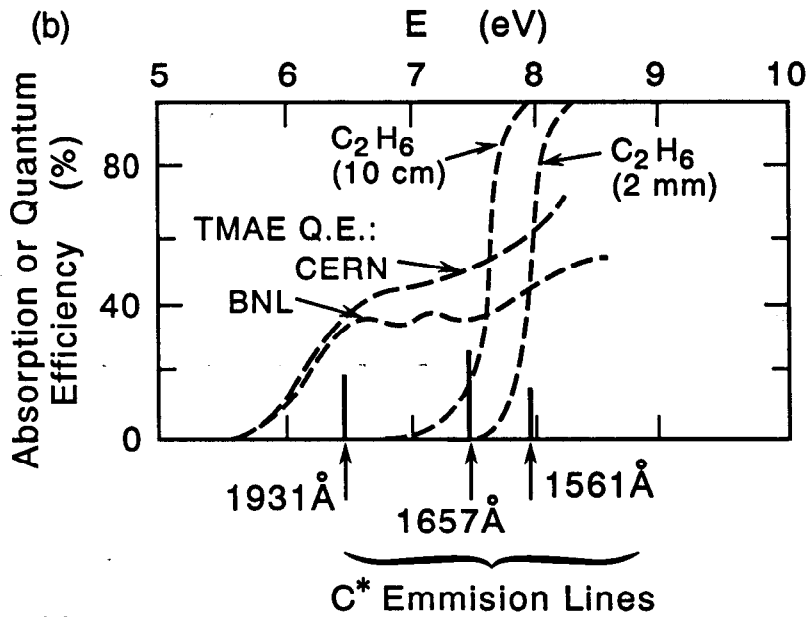
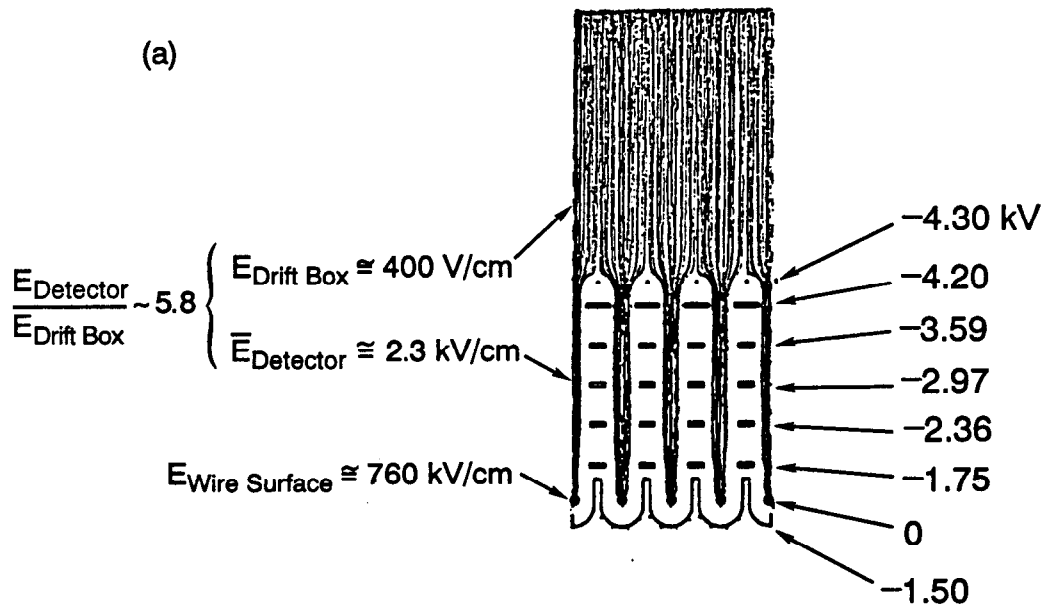


Fig. 2



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Fig. 3

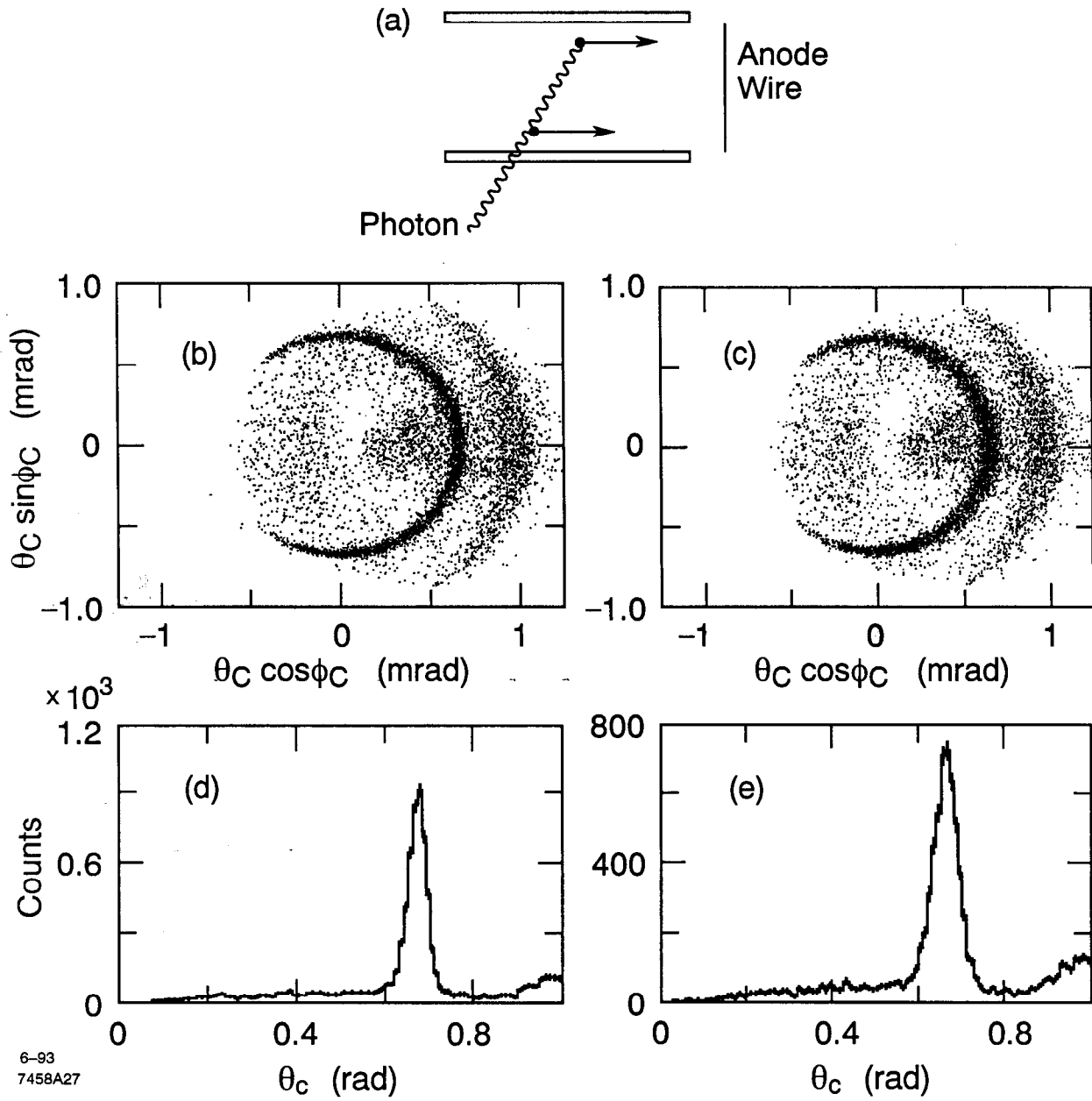
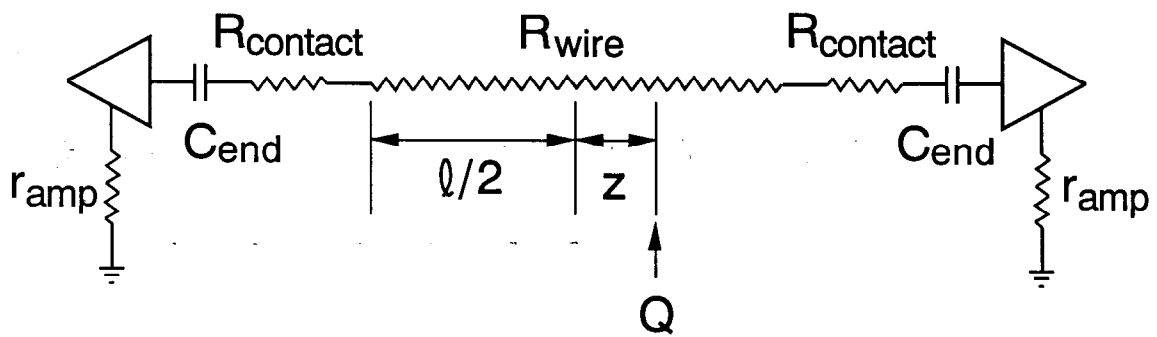


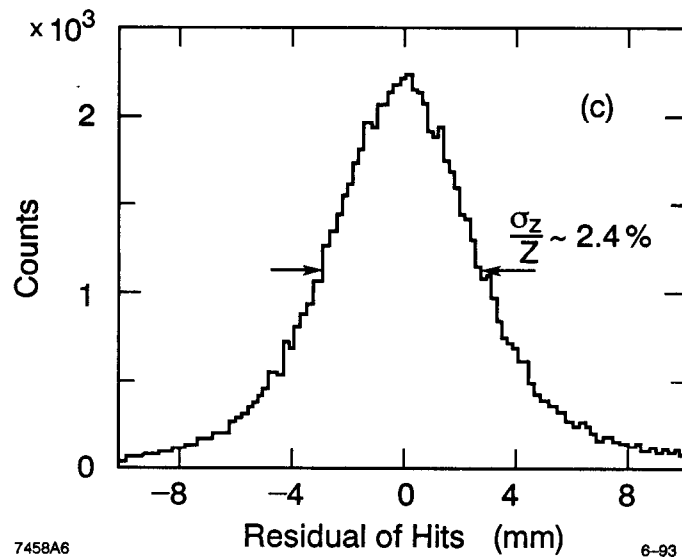
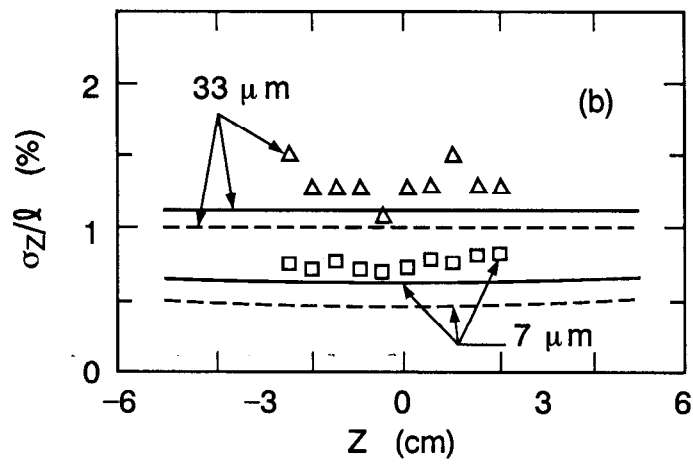
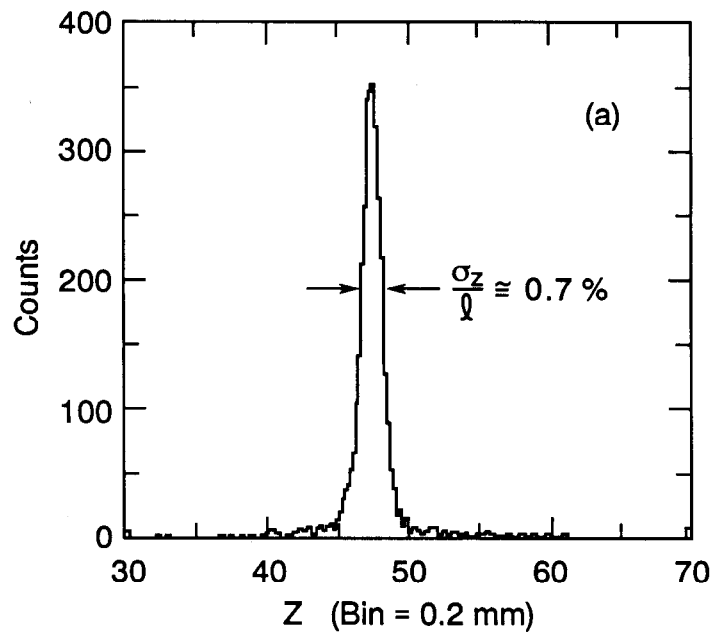
Fig. 4



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Fig. 5



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Fig. 6

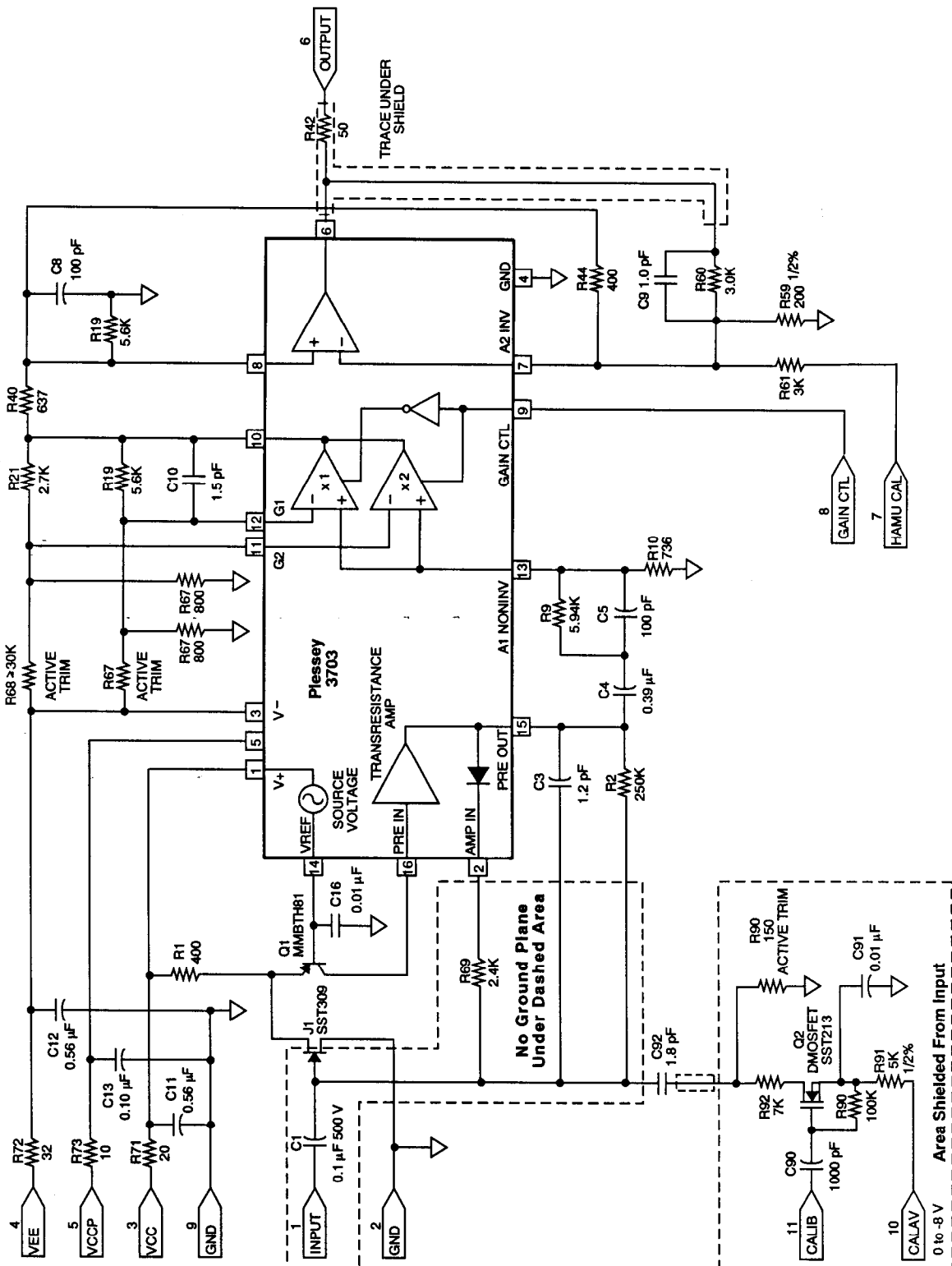
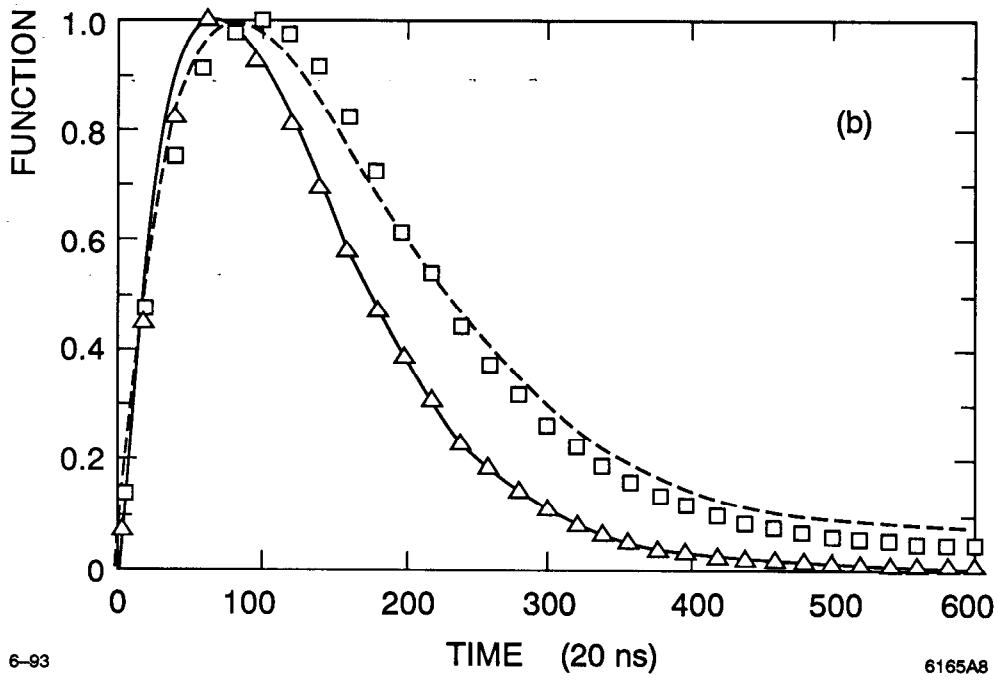
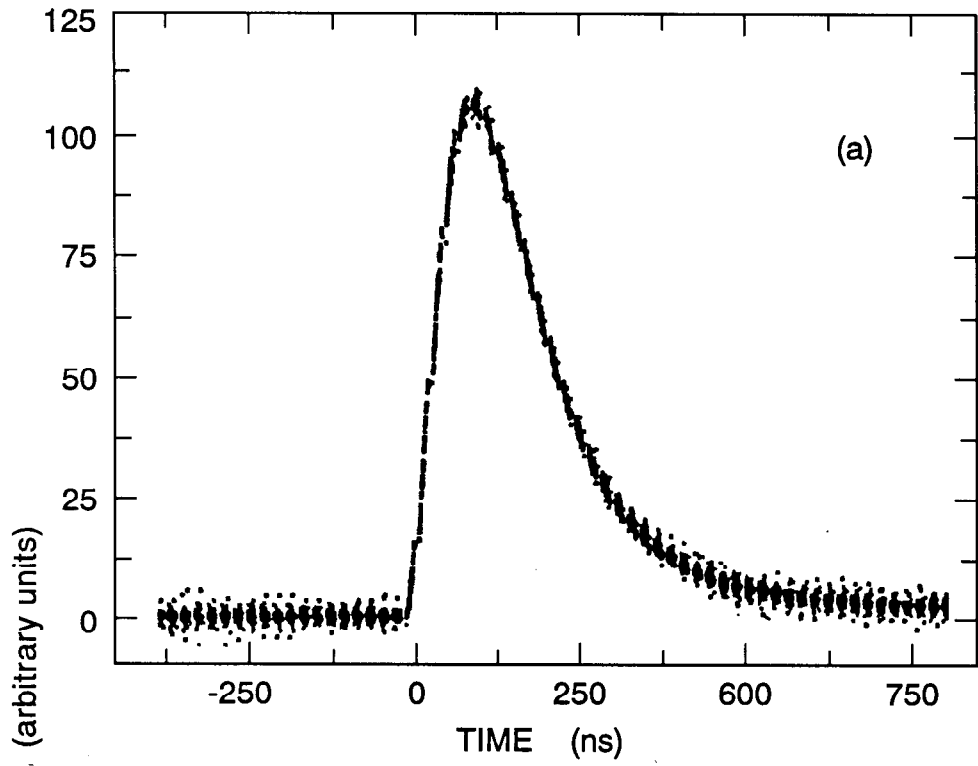


Fig. 7



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Fig. 8

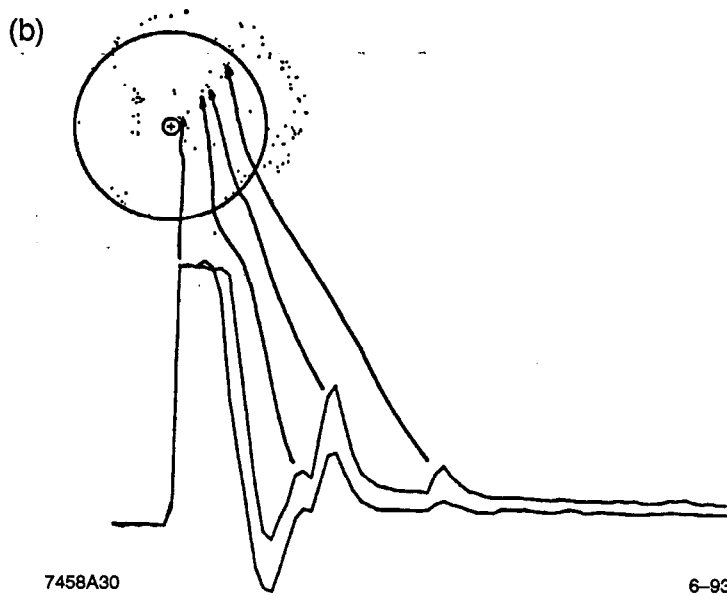
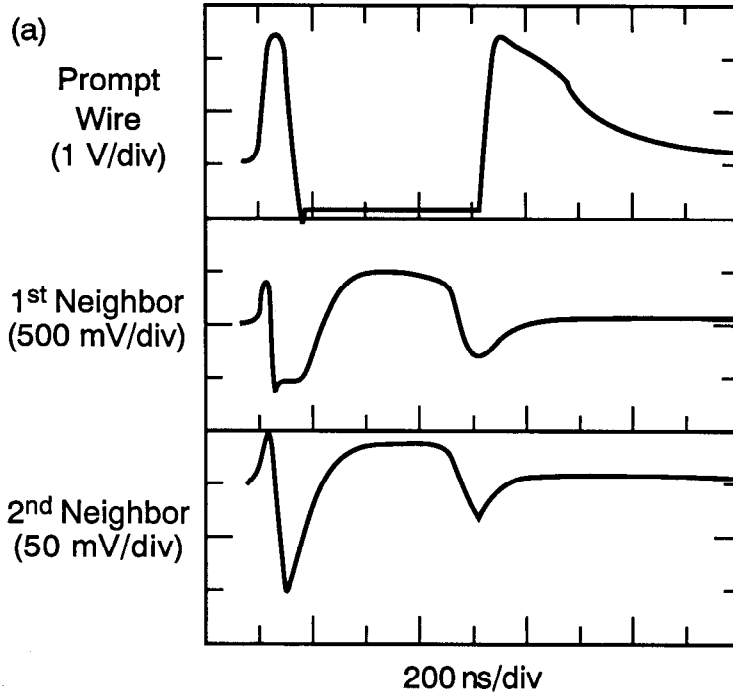
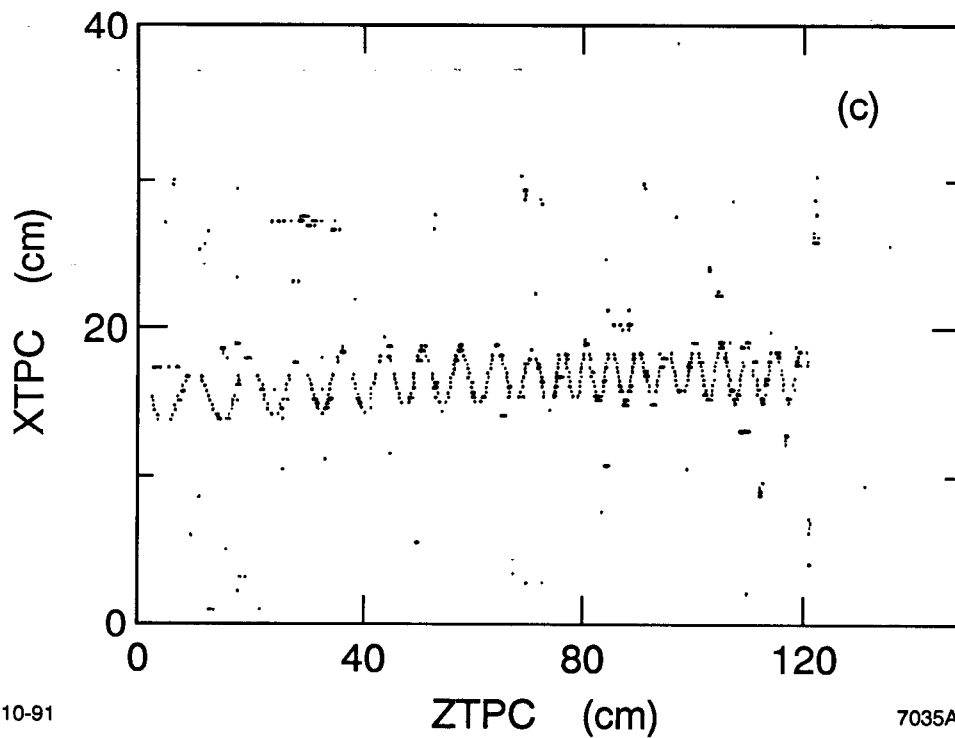
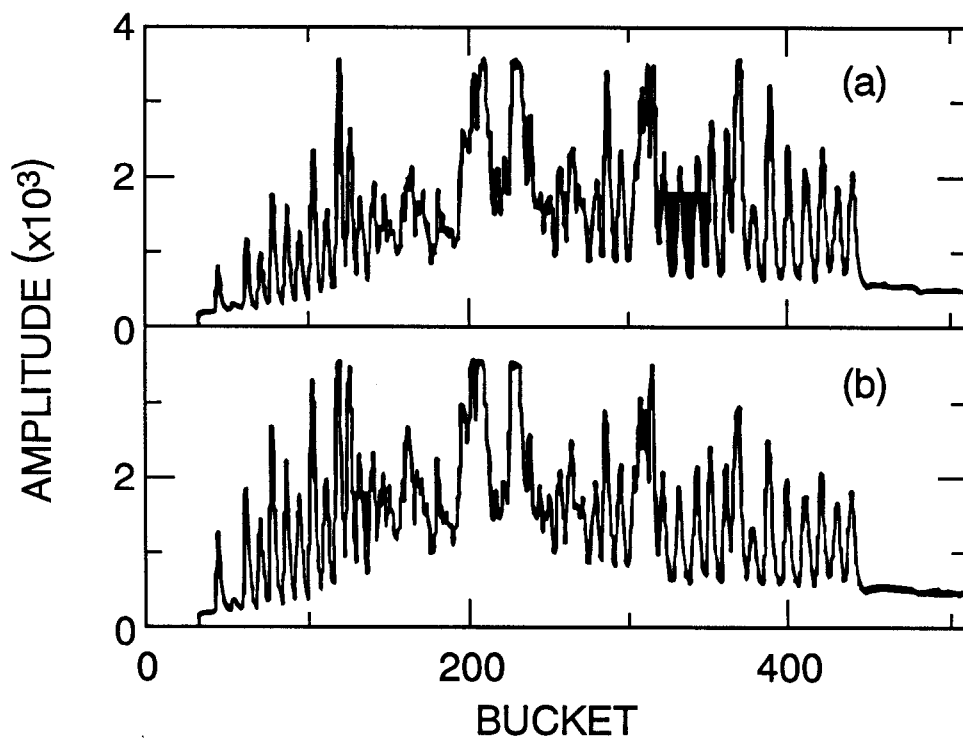


Fig. 9





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Fig. 10

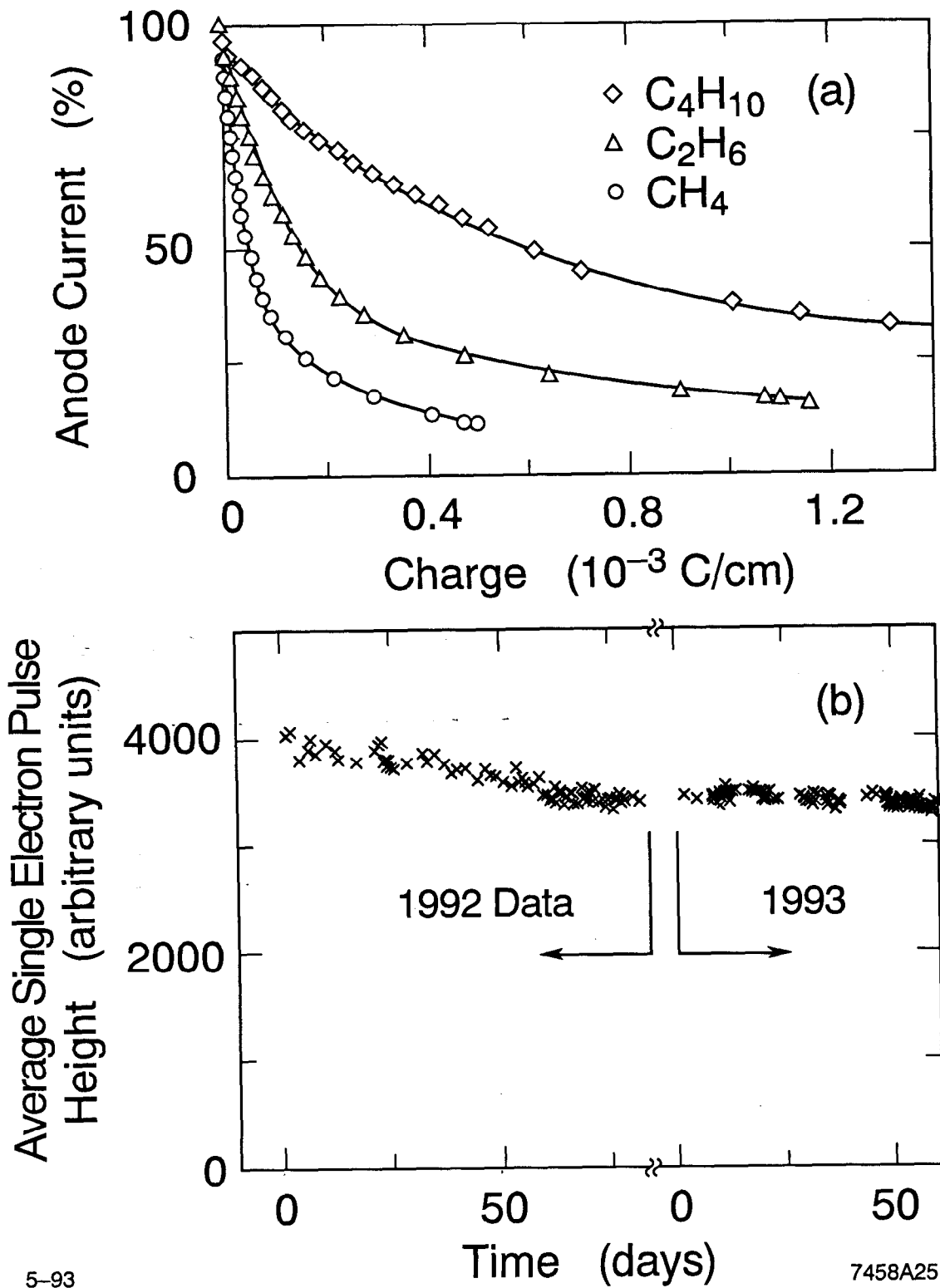
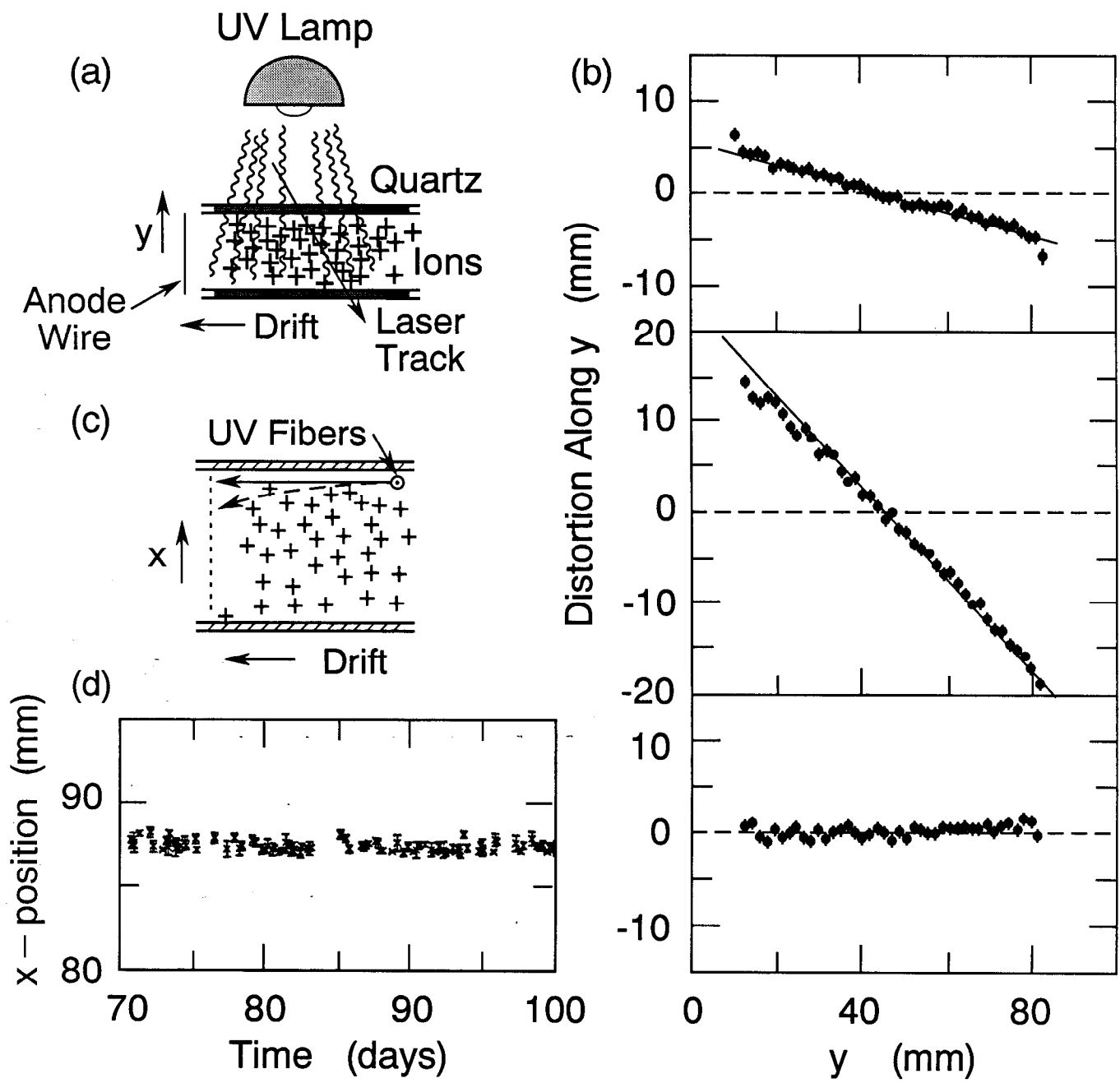


Fig. 11



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Fig. 12

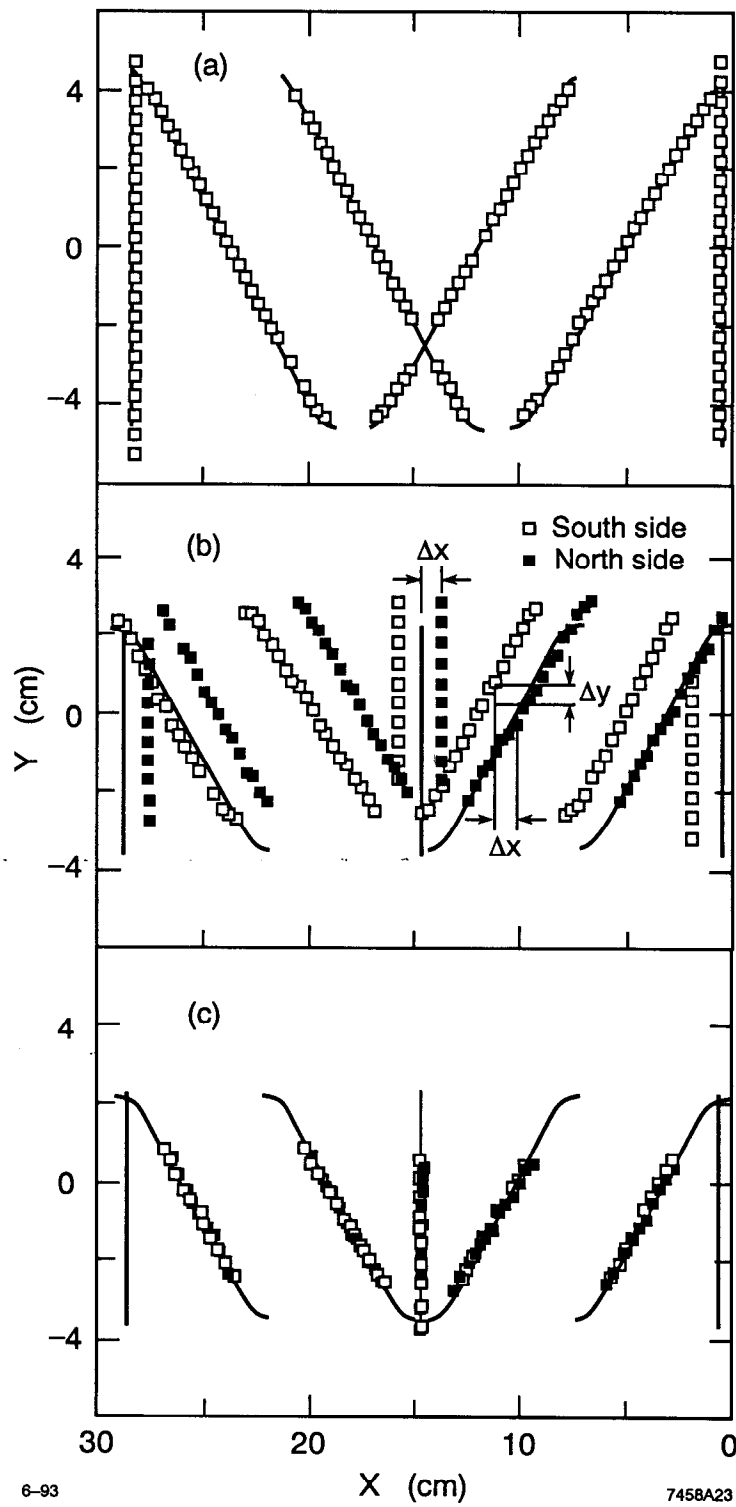


Fig. 13

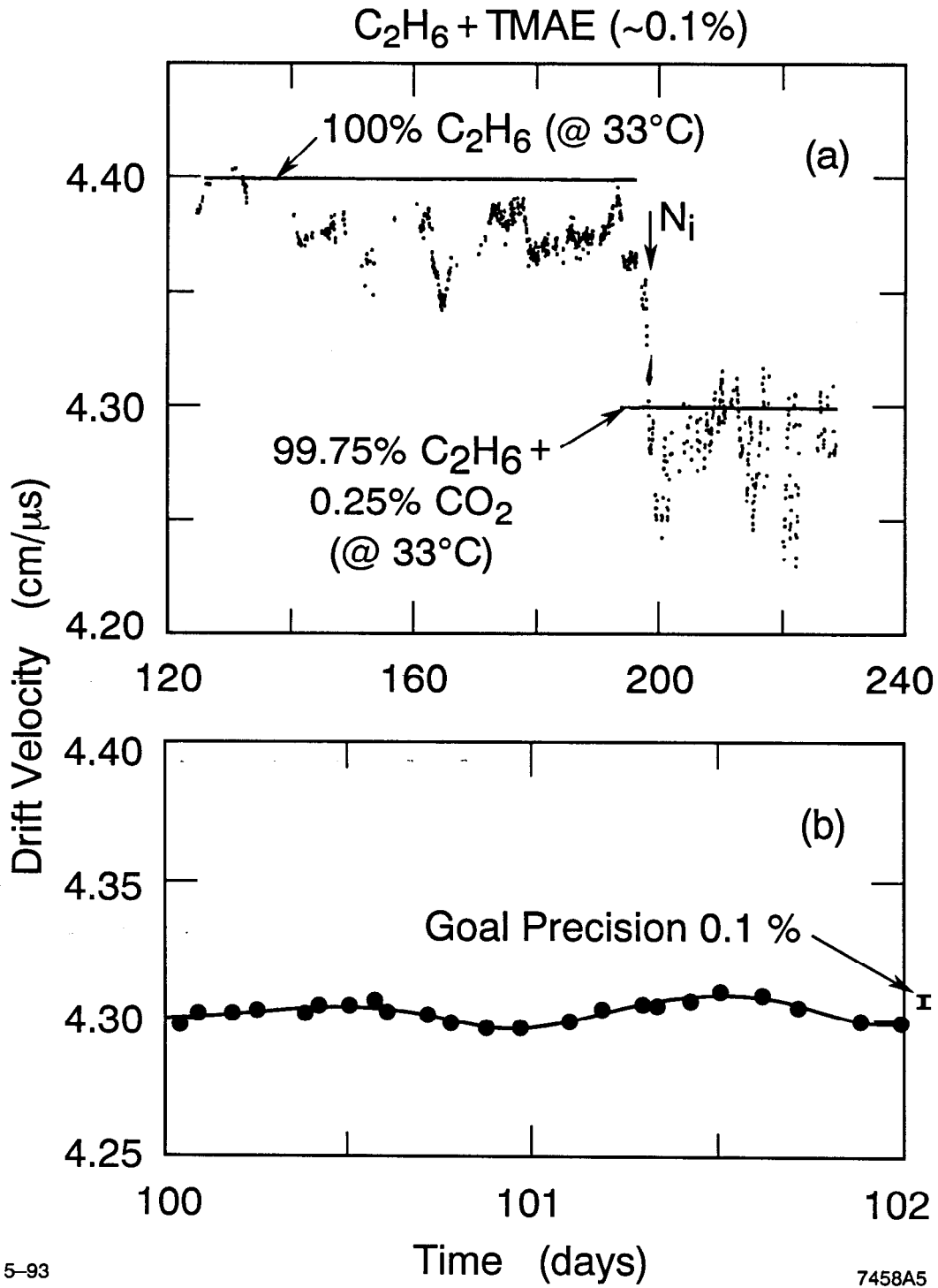


Fig. 14

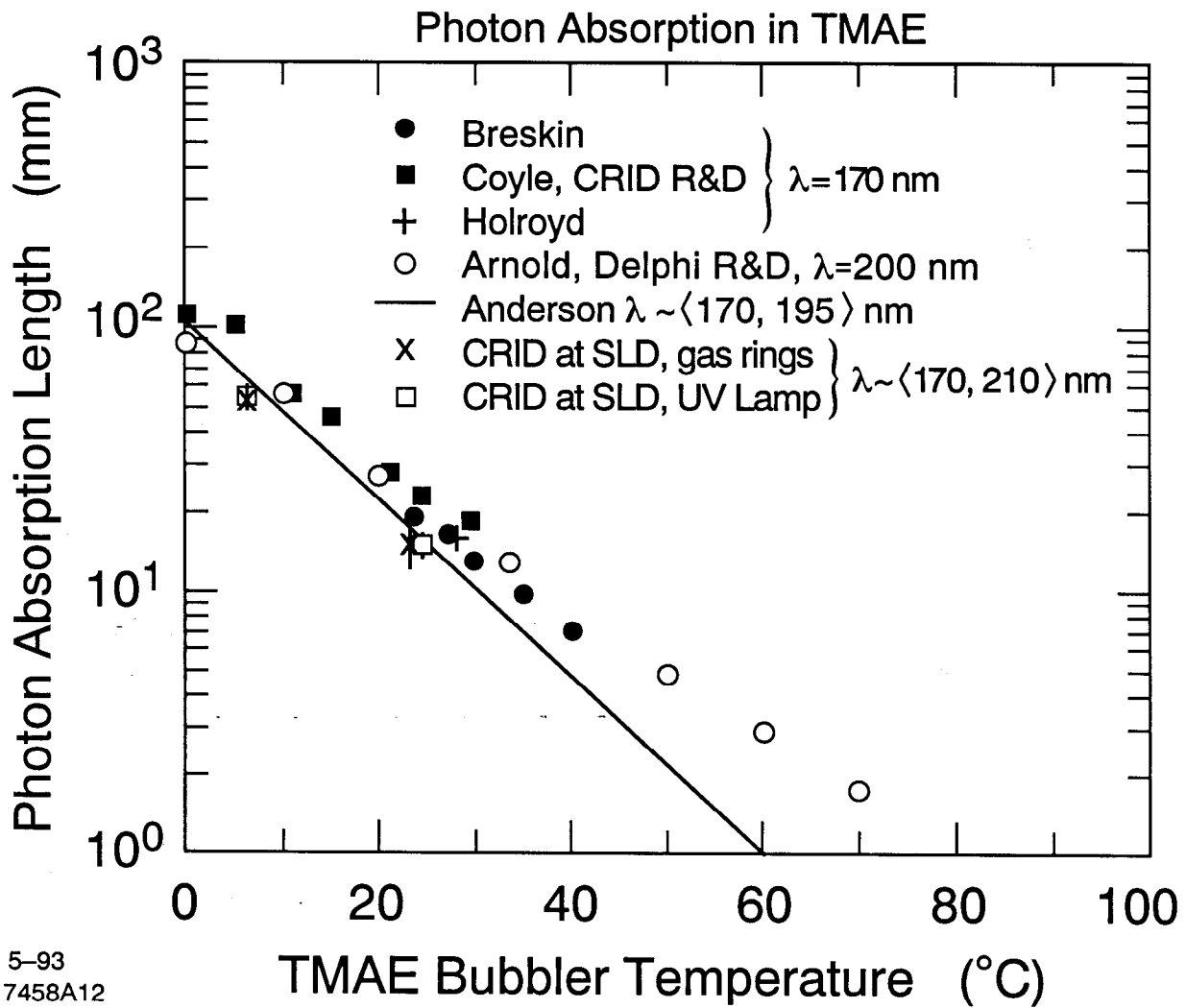
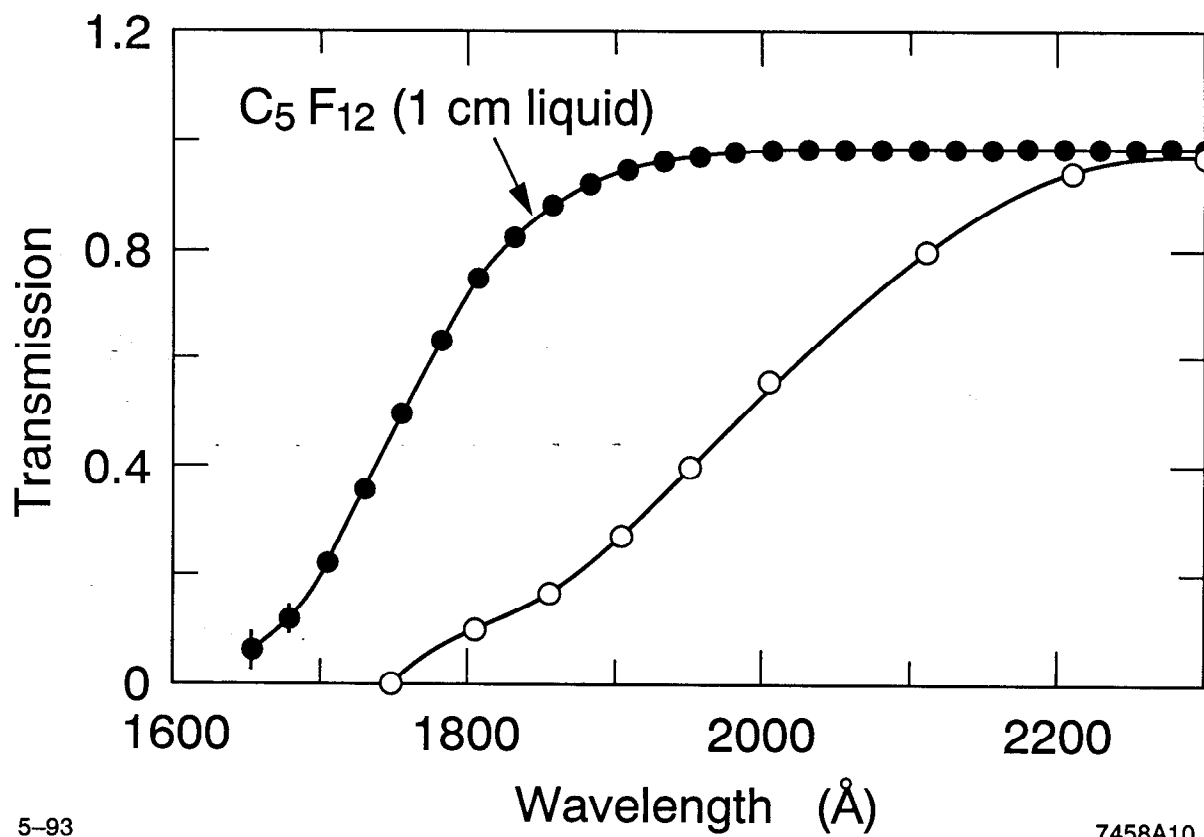


Fig. 15



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Fig. 16

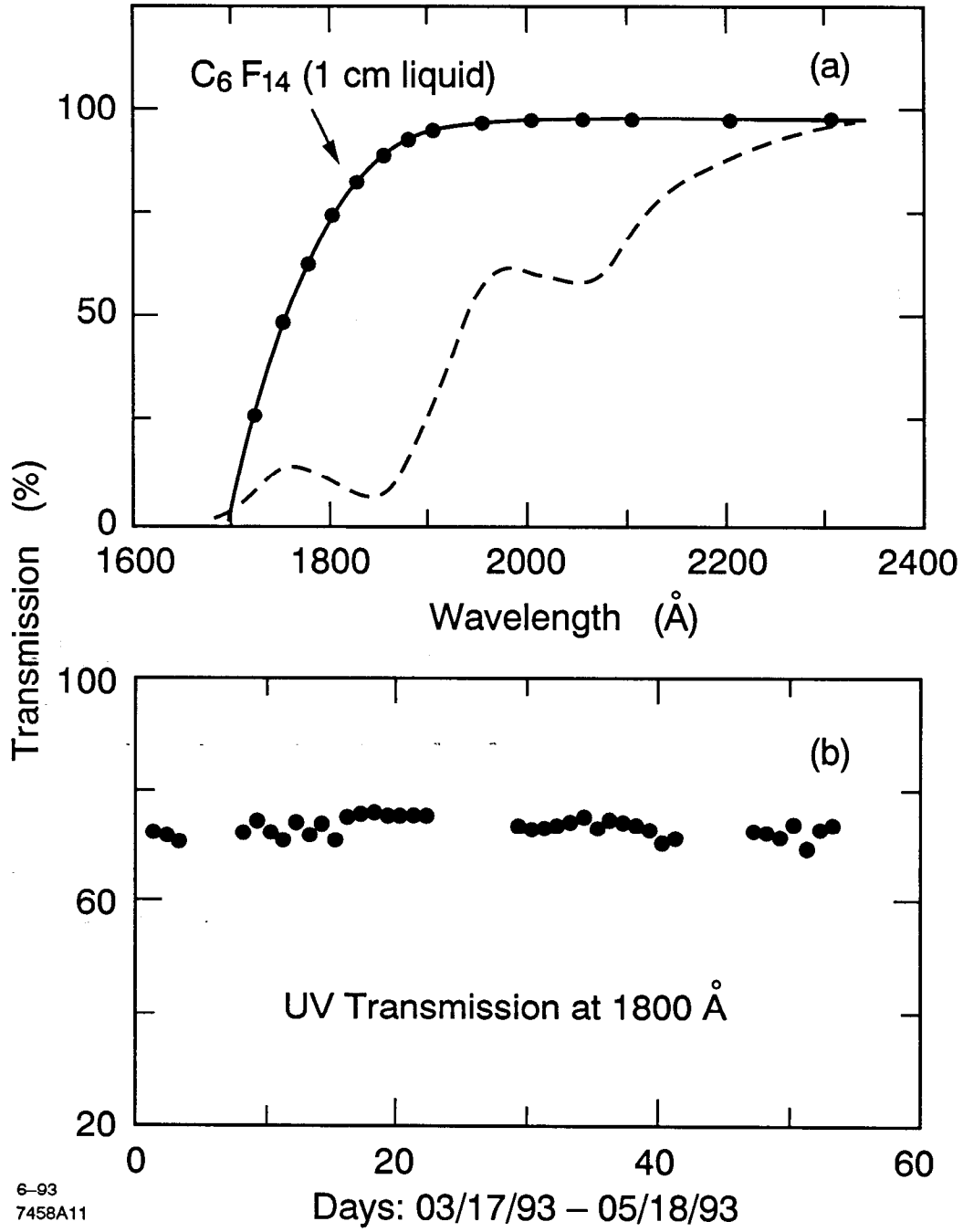


Fig. 17



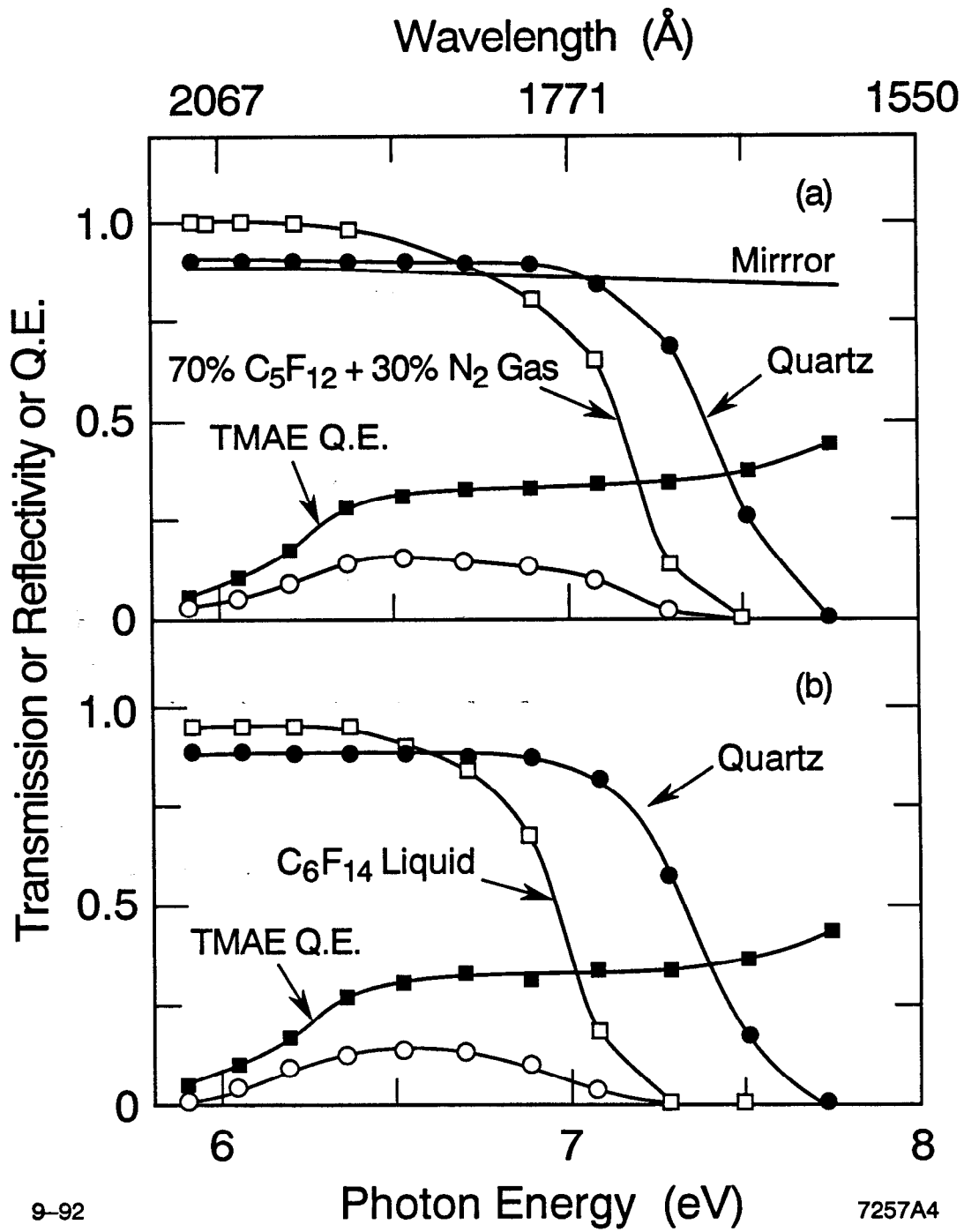


Fig. 18

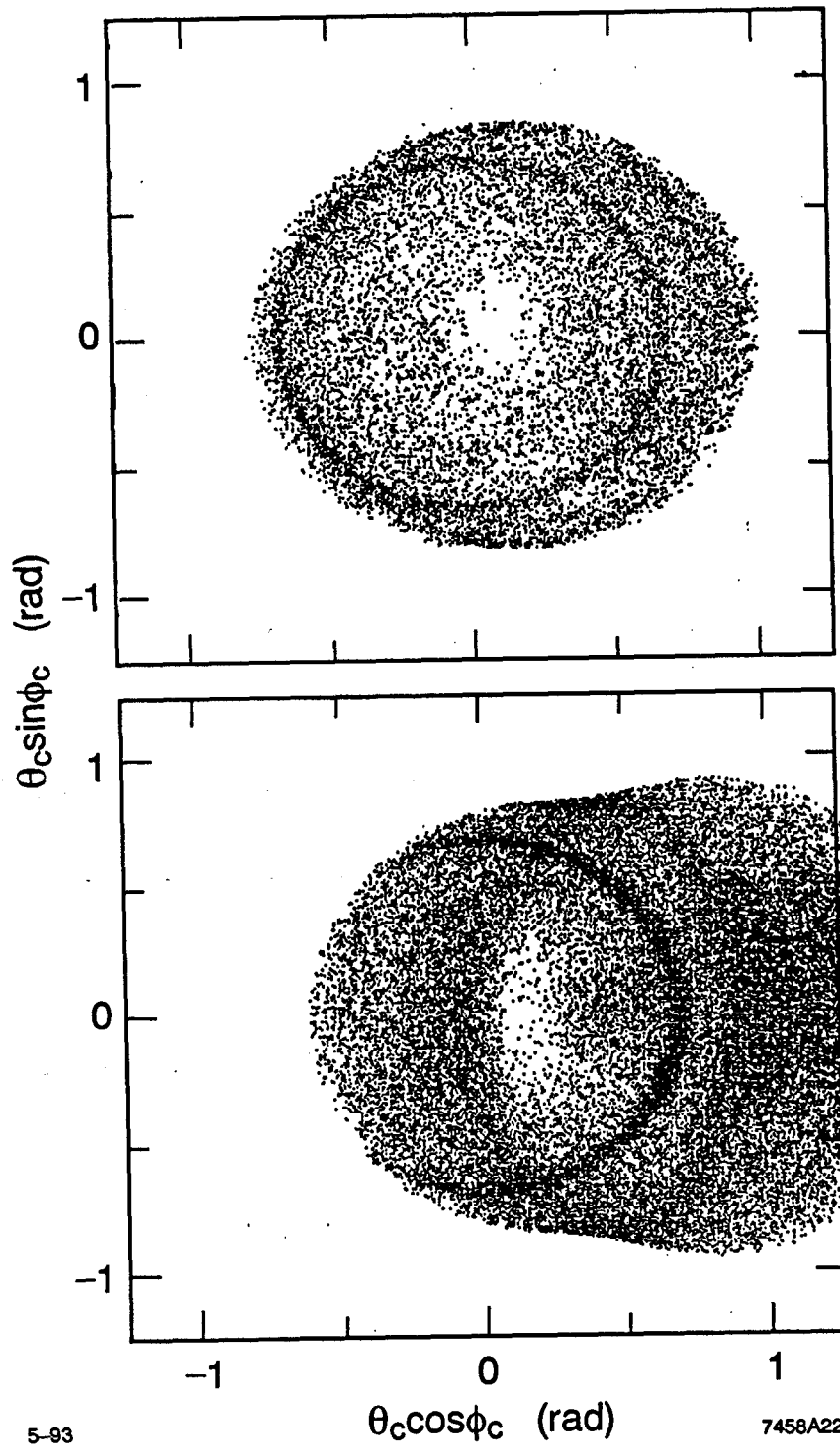
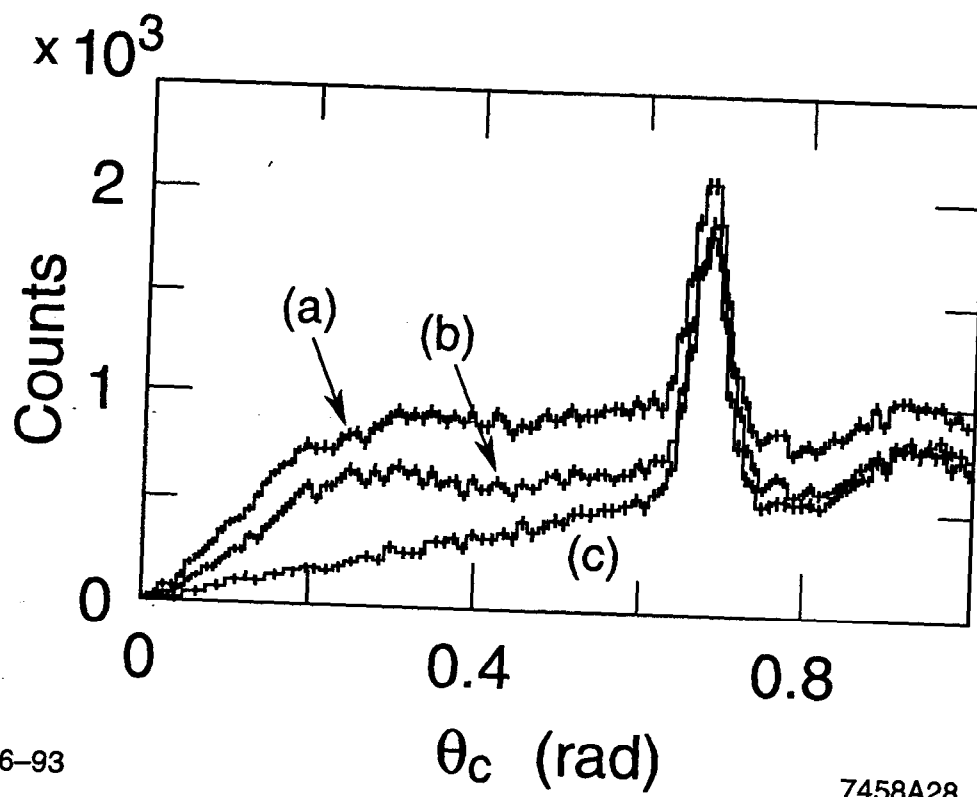


Fig. 19



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Fig.20

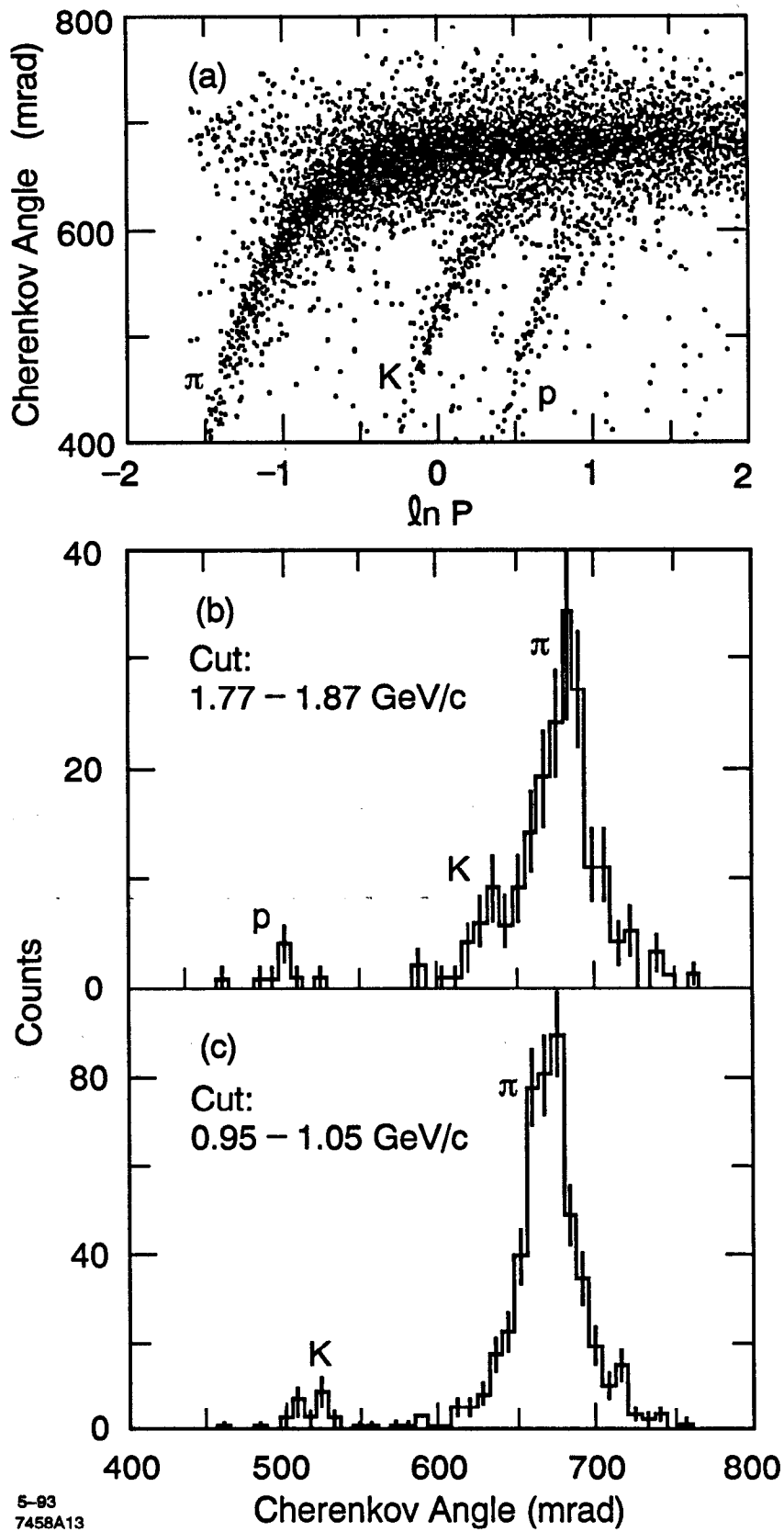


Fig. 21

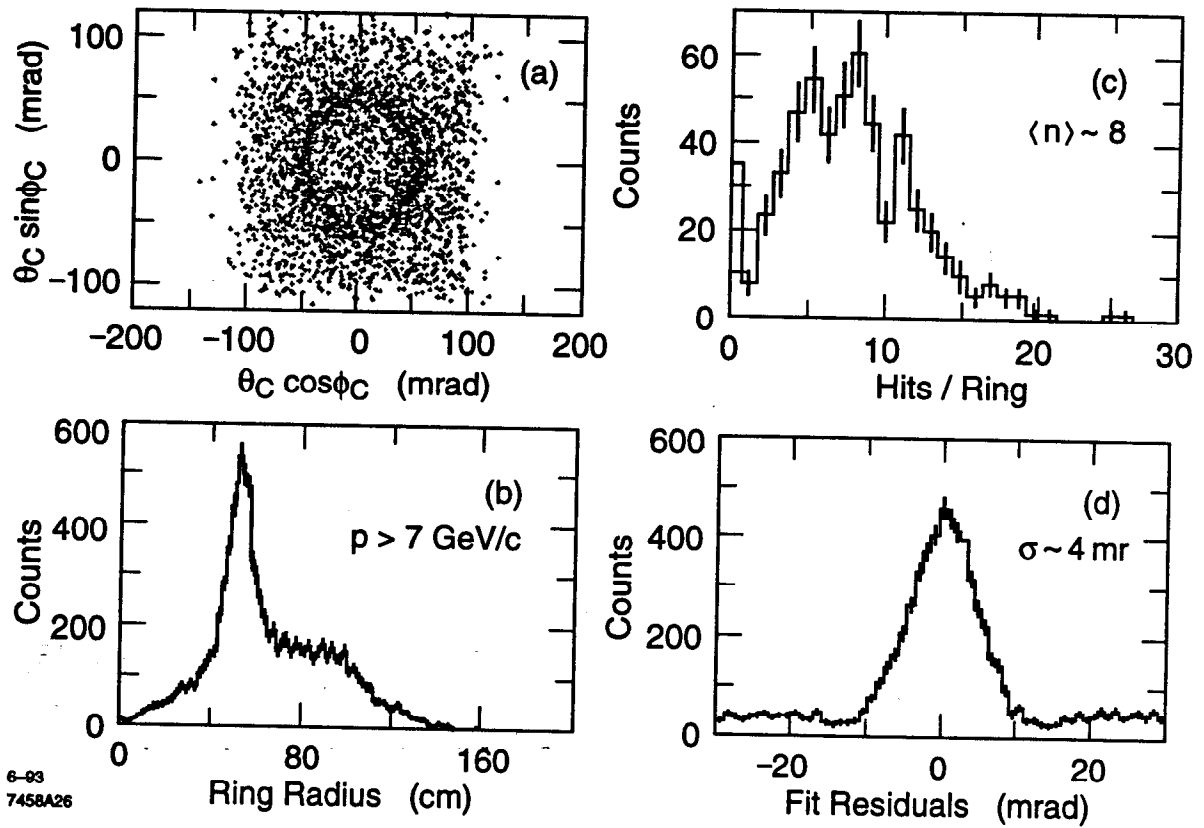


Fig.22