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COLLIMATION SYSTEMS IN THE NEXT LINEAR COLLIDER*

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ABSTRACT

Experience indicates that beam collimation will be an essential element of the next generation e^+e^- linear colliders. A proposal for using nonlinear lenses to drive beam tails to large amplitudes was presented in a previous paper [1]. Here we study the optimization of such systems including effects of wakefields and optical aberrations. Protection and design of the scrapers in these systems are discussed.

I. INTRODUCTION

Experience with the SLC has indicated that backgrounds caused by transverse and energy tails of the beam distribution will be a fundamental problem of next generation linear colliders. Despite efforts to shield the detectors against beam-caused backgrounds, particles in the tails of the beam distribution can produce unacceptably large backgrounds. Any collimation design for the next generation linear colliders must satisfy the following requirements:

(1) It must provide an effective scraping despite the small (of the order of a micron) beam sizes. It should scrape particles with transverse positions greater than 5σ in both planes as well as energy tails.

(2) It must protect scrapers against mis-steered beams which may hit them and possibly damage them. There are two problems associated with a train of 10 bunches of 10^{10} electrons per bunch at 250 GeV hitting a scraper [2]. The first problem occurs at the surface of the scraper which may melt because of energy deposited in a small area. More quantitatively we are interested in the largest spot size to cause failure of the scraper surface. If failure is defined as the melting temperature of the material, then for Ti, which is one of the best candidates according to SLC experience, the area to cause failure is [2]

$$\sigma_x \sigma_y \simeq 900 \ \mu\text{m}^2 \quad . \tag{1}$$

The second problem occurs within the body of the scraper where the energy deposition from the shower peaks, typically at several radiation lengths (RL) ($\simeq$ 8 RL for Ti).

(3) It must keep scraper-induced wakefield kicks on the beam below a tolerable level. If the beam does not pass exactly through the middle of the scrapers, it gets transverse deflections due to geometric and resistive wall wakefields. If these kicks are comparable to the angular divergence of the beam, the emittance will increase.

An expression for the kick of the beam due to geometric wakefields which includes the effect of both edges of a scraper has been derived analytically and verified numerically [3] under the assumptions that the scraper gap is small compared to the scraper length, and the bunch length σ_z is greater than or equal to the scraper gap. It is also assumed that the transverse deflection of a particle is produced by the dipole wakefield only and hence it is proportional to $\Delta\langle y\rangle/g$ where $\Delta\langle y\rangle$ is the beam offset from the middle of the scrapers and $2g$ is the scraper gap. This expression is given by

$$\Delta y' = \theta_{\text{max}} \frac{\Delta\langle y\rangle}{g} \tag{2}$$

where

$$\theta_{\text{max}} = \left(\frac{2e^2 Z_0 c}{4\pi\sqrt{2\pi}}\right) \frac{2N}{E\sigma_z} \tag{3}$$

and N, E are the beam intensity and energy, respectively, and Z_0 is the impedance of free space. Using typical parameters for the Next Linear Collider (NLC), namely $N = 1 \times 10^{10}$ particles per bunch, $\sigma_z = 75\ \mu$m, $E = 250$ GeV, we arrive at

$$\Delta y' = 1.2 \times 10^{-6} \frac{\Delta\langle y\rangle}{g} \quad \text{rad} \quad . \tag{4}$$

To reduce the effect of the geometric wakefield kick, one can taper the scrapers with a taper angle θ_{tap}. ($\theta_{\text{tap}} = \pi/2$ for a step scraper.) For small taper angles ($\theta_{\text{tap}} \leq 100$ mrad) the dependence on the taper angle is linear [4,5],

$$\Delta y' = 3\theta_{\text{max}} \frac{\Delta\langle y\rangle}{g} \left(\frac{2\theta_{\text{tap}}}{\pi}\right) \quad . \tag{5}$$

The kick due to the resistive wall wakefield is proportional to $\Delta\langle y\rangle/g^3$. Specifically it is given by

$$\Delta y' = C_{\text{max}} \frac{\Delta\langle y\rangle}{g^3} L_{\text{scr}} \tag{6}$$

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where L_{scr} is the scraper length,

$$C_{\max} = \frac{4r_e N}{\gamma\pi}\left(\frac{c/\sigma}{l}\right)^{1/2} f(s) \quad , \qquad (7)$$

and $\gamma = E/mc^2$, σ is the conductivity of the material, $l = 2\sigma_z$, and $f(s)$ is a function of the longitudinal coordinate within the bunch, varying between 0 and 1. For typical NLC parameters and for a scraper made of Ti,

$$\Delta y' = 0.85 \times 10^{-13} \frac{\Delta\langle y\rangle}{g^3} L_{scr} \quad \text{rad} \quad . \qquad (8)$$

The function $f(s)$ has been approximated by 1/2 to account for the head to tail variation of the wakefield. For small gaps this is the dominant wakefield effect.

Next we shall demonstrate that mechanical collimation is precluded for the vertical degree of freedom as a workable collimation technique for the NLC, on the basis of the above issues. In the following section we present the nonlinear collimation scheme as a possible alternative. We first write the conditions that must be satisfied. These conditions determine a set of lattice parameters for the collimation systems. Then we present a possible lattice design, calculate its tolerances and discuss our ideas on energy collimation. Before we conclude we examine the possibility of nonlinear collimation with octupoles and decapoles. Finally we summarize the issues and point out the problems of the current design as well as questions remaining to be answered.

II. MECHANICAL COLLIMATION

NLC beams are flat with a ratio of horizontal to vertical emittance equal to 100 to 1. The incoming beam to the collimation section, which is assumed to be at the end of the linac and before the final focus, has horizontal and vertical emittances equal to

$$\epsilon_x = 10^{-11} \text{ m rad} \ , \quad \epsilon_y = 10^{-13} \text{ m rad} \quad . \qquad (9)$$

The beam energy is 250 GeV. We now investigate the possibility of mechanical collimation for the vertical plane. The design of the collimation section must satisfy the following requirements:

(a) The scraper gap must be equal to $5\sigma_y$,

$$g_y = 5\sigma_y \quad . \qquad (10)$$

(b) The rms value of the geometric wakefield kick must be less than 1/5 σ'_y,

$$(\Delta y'_{\rm gw})_{\rm rms} \le \frac{1}{5}\sigma'_y \quad . \qquad (11)$$

This requirement leads to an increase of the spot size which is less than or equal to 2%.

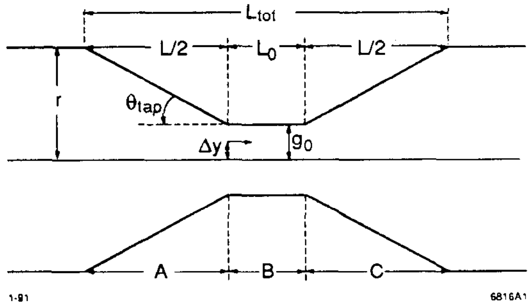

Figure 1: Definition of the various parameters entering the calculation of tapered scrapers.

(c) The rms resistive wall wakefield kick must be less than 1/5 σ'_y,

$$(\Delta y'_{\rm rw})_{\rm rms} \le \frac{1}{5}\sigma'_y \quad . \qquad (12)$$

(d) The area of 1σ beam at the scrapers must be greater than 900 μm^2, in order to ensure protection of the scrapers when a mis-steered beam hits them,

$$\sigma_x\sigma_y \ge 900 \ \mu\text{m}^2 \quad . \qquad (13)$$

One can easily verify that the geometric wakefield condition (b) is satisfied for an extremely small β-function at the scraper ($\beta_y \le 0.07$ m) which implies that the gap would be 0.4 μm. Such a gap is too small for practical considerations. We clearly have to use tapered scrapers. However tapered scrapers are necessarily longer and hence the resistive wall wakefield is increased as it varies proportionally with the length of the scraper. Therefore we must evaluate the resistive wall wake for tapered scrapers and find the common solution of both conditions (11) and (12).

To calculate the resistive wall wake of a tapered scraper we can, to a first approximation, substitute L_{scr}/g^3 by the integral

$$I = \int_0^{L_{\rm TOT}} \frac{dz}{g^3(z)} \qquad (14)$$

where $L_{\rm TOT}$ is the total length of the scraper (see Fig. 1), and $g(z)$ is the gap as a function of z.

Assuming the geometry of Fig. 1 where the scraper varies linearly with the longitudinal coordinate z in the regions A and C, we have

$$g(z) = \begin{cases} r + \frac{2}{L}(g_0 - r)z & \text{for } 0 \le z \le \frac{L}{2} \\ g_0 & \text{for } \frac{L}{2} \le z \le L_0 \ . \end{cases} \qquad (15)$$

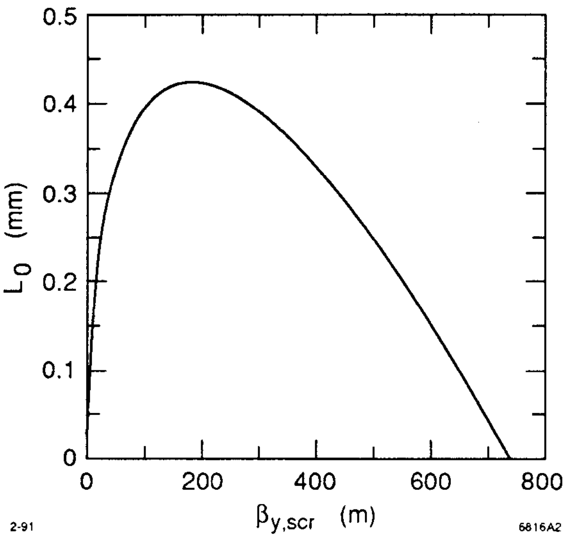

Figure 2: Mechanical collimation in the vertical plane: Scraper length as a function of the β-function at the scraper. The allowed region is below the curve.

Then the integral I is

$$I = \frac{L(r+g_0)}{2g_0^2 r^2} + \frac{L_0}{g_0^3} \quad . \tag{16}$$

Hence the resistive wall wakefield condition becomes

$$C_{\max}\Delta y \left[\frac{L(r+g_0)}{2g_0^2 r^2} + \frac{L_0}{g_0^3}\right] \leq \frac{1}{5}\sigma_y' \quad . \tag{17}$$

The geometric wakefield condition on the other hand becomes

$$3\theta_{\max}\frac{\Delta\langle y\rangle}{g_0}\frac{2}{\pi}\frac{2(r-g_0)}{L} \leq \frac{1}{5}\sigma_y' \tag{18}$$

where we have approximated θ_{tap} by

$$\theta_{\text{tap}} \simeq \frac{2(r-g_0)}{L} \quad . \tag{19}$$

If we now require that the equalities of both Eqs. (17) and (18) be satisfied, we can solve for β_y at the scraper as a function of L_0. For an offset equal to 1/5 σ_y the solution is shown in Fig. 2 where the area below the curve displays the allowed solution space.

Notice that the maximum L_0 in the allowed space is 0.43 mm, which corresponds to about 1/100 of a radiation length for Ti. Such a thin scraper however will not be able to disrupt the beam sufficiently in order for significant change of beam parameters to take place. We conclude that simple mechanical collimation for the vertical plane is impossible.

III. NONLINEAR COLLIMATION

A. THE BASIC PRINCIPLE

The idea here is to blow up the part of the beam we want to collimate so that mechanical scrapers can be used effectively without inducing significant wakefield kicks. Throughout this process the core, which contributes to the luminosity of the machine, must remain unaffected.

Linear optical magnification has been excluded as we demonstrated in the preceding section. On the other hand, higher-order multipoles such as decapoles, dodecapoles, etc., are not useful because they don't penetrate to the small distances necessary. However, for a TeV linear collider beam, sextupole and octupole fields, placed at a point where the beam size is large, seem promising. The proposed nonlinear collimation scheme [1] works as follows.

The initial beam distribution goes through a nonlinear lens, followed by a rotation in betatron phase by $\pi/2$. Mechanical scrapers placed at this point cut off the long position tails. The core, which has been modified in the process, can be put back together by adding to the above lattice section its mirror image [6]. This technique is well known. Two nonlinear elements of the same or opposite polarity (depending on their multipolarity), π apart in phase advance, amount to the identity transformation (up to a $\pm$ sign).

Since in a real machine both position and angle tails cause background problems, one would like to clean up the beam profiles in both phases (say x and x'). The following scheme takes this into account. It includes two lattice sections, each of which consists of two nonlinear elements π apart; thus collimation in both phase space directions is possible. The two lattice sections are next to each other separated by a phase advance of $\pi/2$. Next we demonstrate how this scheme can be used for collimation in the vertical plane for the NLC.

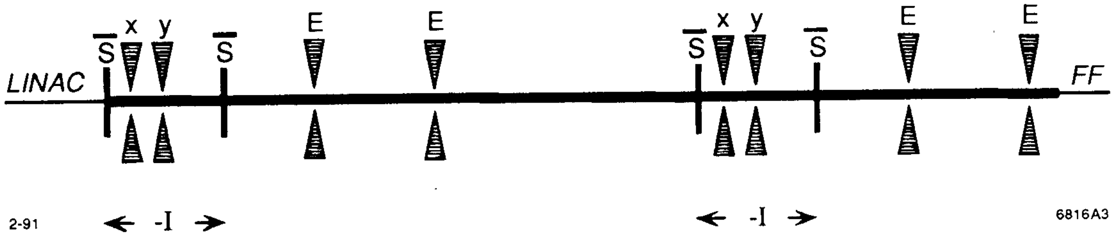

Figure 3: Schematic representation of the collimation systems in the NLC, located between the linac and final focus (FF). $\overline{S}$ stands for skew sextupole; x,y,E stand for horizontal, vertical and energy scraper, respectively.

B. NONLINEAR COLLIMATION IN THE NLC

B1. SCHEME WITH SKEW SEXTUPOLE PAIRS

Collimation in the NLC is proposed to be done mechanically in the horizontal plane and nonlinearly in the vertical plane (scheme with skew sextupole pairs). The horizontal scrapers will be placed at high horizontal beta function points, interleaved with the vertical scrapers. Energy scraping takes place right after transverse scraping. A schematic representation of the collimation section of the NLC is shown in Fig. 3. The collimation design must satisfy all of the following conditions.

(a) It must scrape transverse tails beyond 5σ in both planes.

(b) It must scrape energy tails.

(c) Resistive wall wakes at both horizontal and vertical scrapers must be controlled.

(d) Geometric wakes at both horizontal and vertical scrapers must be controlled.

(e) Geometric and resistive wall wakes at the sextupoles must be controlled.

(f) Long sextupole aberrations must be controlled.

(g) It must ensure protection of horizontal, vertical and energy scrapers.

(h) Stability tolerances on sextupole and scraper offsets must be acceptable.

(i) The collimation systems must not create unacceptable optical aberrations.

Next we elaborate on each of the above conditions and thus arrive at the allowed design parameters of the collimation system.

Scraping in the vertical plane

This condition implies that particles whose vertical coordinates are greater or equal to $5\sigma_y$ at the sextupole must be mapped into vertical positions greater or equal to g_y at the scraper,

$$\Delta y_{\rm scr}(|y_{\rm sext}| \geq 5\sigma_{y,{\rm sext}}) \geq g_y \quad . \tag{20}$$

A 5σ particle at the skew sextupole will experience a kick

$$\Delta y'_{\rm sext} = S(5\sigma_y)^2 \tag{21}$$

where S is the integrated sextupole strength,

$$S = \frac{B_{\rm pole} L_{\rm sext}}{a^2(B\rho)} \quad . \tag{22}$$

Here $B_{\rm pole}$ denotes the pole-tip field, $L_{\rm sext}$ is the sextupole length, a is the pole-tip radius of the sextupole and $B\rho$ is the magnetic rigidity. This kick will in turn give rise to an offset at the scraper

$$\Delta y_{\rm scr} = R_{12} \Delta y'_{\rm sext} \quad , \tag{23}$$

where R is the transfer matrix between sextupole and scraper. Combining the above equations we arrive at the condition

$$C_1 R_{12} \beta_{\rm sext} \geq g_y \tag{24}$$

where

$$C_1 = 25 S \epsilon_y \quad . \tag{25}$$

Resistive wall wakes at the vertical scrapers

As we showed earlier the resistive wall wakefield kick at the scraper is given by

$$\Delta y'_{\rm scr} = C_{\rm max} \frac{\Delta \langle y_{\rm scr} \rangle}{g_y^3} L_{\rm scr} \tag{26}$$

which becomes at the downstream sextupole

$$\Delta y_{\rm sext} = R_{12} \Delta y'_{\rm scr} \quad . \tag{27}$$

An offset through the skew sextupole gives rise to a normal quadrupole kick of magnitude

$$\Delta y'_{\rm sext} = (2S\Delta y_{\rm sext})y \quad . \tag{28}$$

We require that the rms value of these kicks be less than 1/5 σ'_y (to avoid unacceptable longitudinal jitter of the final focal point),

$$(2S\Delta y_{\rm sext})y_{\rm rms} \le \frac{1}{5}\sigma'_y \quad . \tag{29}$$

We wish to allow a 1σ jitter of the incoming beam centroid, hence we take

$$\Delta\langle y_{\rm scr}\rangle = \sigma_{y,{\rm scr}} \tag{30}$$

in Eq. (29), which combined with Eqs. (26) and (27) gives

$$C_2 R_{12}^2 L_{\rm scr}\beta_{\rm sext}^{1/2} \le \frac{1}{5}g_y^3 \tag{31}$$

where

$$C_2 = 2SC_{\rm max}\epsilon_y^{1/2} \quad . \tag{32}$$

Long sextupole aberrations

The potential for long-sextupole aberrations is given by [7,8]

$$V_{LS} = \frac{1}{12}S^2 L_{\rm sext}y^4 \tag{33}$$

assuming small horizontal beam size. Therefore the long-sextupole kick is

$$\Delta y' = \frac{1}{3}S^2 L y^3 \tag{34}$$

and we require

$$(\Delta y')_{\rm rms} \le \frac{1}{5}\sigma'_y \quad . \tag{35}$$

This leads to the condition

$$\frac{5\sqrt{15}}{3}S^2 L_{\rm sext}\epsilon_y\beta_{y,{\rm sext}}^2 \le 1 \quad . \tag{36}$$

For the two sextupoles of the $-I$ transformation, the above equation determines the maximum allowed vertical β-function,

$$\beta_{y,{\rm sext}} \le 23,000 \quad {\rm m} \quad . \tag{37}$$

In deriving this we have assumed a pole-tip field of 1 Tesla, pole-tip radius of 1 mm and sextupole length of 10 cm.

Equations (24), (31) and (37) determine the parameter space for the vertical plane, once the values of R_{12} and $L_{\rm scr}$ are specified. The scraper length was chosen to be equal to 3 RL of Ti, namely 11.3 cm. To arrive at this value we used the code EGS [9] to calculate the number of electrons that make it through the 3 RL of Ti, with energies between 245 and 250 GeV.

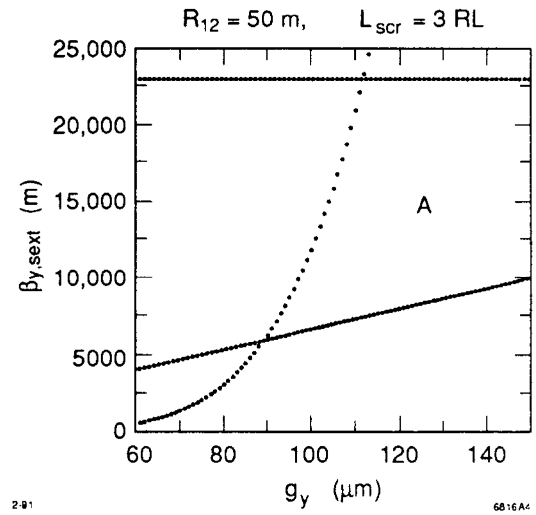

Figure 4: Parameter space for nonlinear collimation with sextupoles.

We found that 1 out of 10^{12} electrons belongs to this energy bin. Although more accurate EGS calculations should be performed these preliminary results indicate that 3 RL of Ti change the beam energy sufficiently in order for subsequent energy scraping to collimate the beam.

The value of R_{12} is directly related to the total length of the system and hence it should be kept minimum. For $R_{12} = 50$ m (which corresponds to a length between sextupole and scraper of about 30 m), and an 11.3 cm long scraper we plotted the above equations in Fig. 4.

The region A enclosed by the three curves corresponds to the allowed space. Now we can choose the parameters of the collimation design in the vertical plane:

$$\beta_{y,{\rm sext}} = 6,000 \ {\rm m} \quad {\rm and} \quad g_y = 90 \ \mu{\rm m} \quad . \tag{38}$$

Next we check to see that the geometric wakefield condition is satisfied both at the scrapers and the sextupoles for the above choice of parameters.

Geometric wakefields at the vertical scrapers

Following arguments similar to the ones employed before, and assuming untapered scrapers, we arrive at

$$\beta_{y,{\rm sext}} \le \frac{g_y^2}{C_3^2 R_{12}^4} \tag{39}$$

where

$$C_3 = 10S\theta_{\rm max}\epsilon_y^{1/2} \quad . \tag{40}$$

This equation implies that

$$\beta_{y,\text{sext}} \leq 6,250 \quad \text{m} \ , \tag{41}$$

which is satisfied.

Geometric and resistive wall wakes at the sextupoles

The geometric wakefield condition Eq. (11) at the sextupoles, for an offset

$$\Delta\langle y\rangle = 1 \ \sigma_{y,\text{sext}} \quad , \tag{42}$$

is satisfied for $\beta_{y,\text{sext}} \leq 170$ m. In our design however, $\beta_{y,\text{sext}} = 6,000$ m, so we clearly have to taper the beam pipe at the sextupoles. In order for Eq. (11) to be satisfied, the taper angle must be

$$\theta_{\text{tap,sext}} \leq 15 \ \text{mrad} \quad . \tag{43}$$

Each tapered section of the sextupoles is then 30 cm long, assuming that the beam pipe radius is 5 mm.

To calculate the magnitude of the resistive wall wakes from the tapered sextupoles we use Eq. (17) with $L_0 = 10$ cm, $L/2 = 30$ cm and $g_0 = 1$ mm. For $\Delta y = 1 \ \sigma_{y,\text{sext}}$,

$$(\Delta y')_{\text{rw,rms}} \simeq \frac{1}{10}\sigma'_{y,\text{sext}} \quad , \tag{44}$$

hence the resistive wall wakefield condition is satisfied at the sextupoles.

Horizontal considerations

An important consideration that determines the x-plane parameters is the $x - y$ coupling at the sextupoles. To minimize coupling effects we must ensure that at the sextupoles,

$$Sy^2 \gg Sx^2 \quad , \tag{45}$$

which establishes a condition on β_x at the sextupoles,

$$\beta_{x,\text{sext}} \ll \beta_{y,\text{sext}} \frac{\epsilon_x}{\epsilon_y} \quad . \tag{46}$$

In our case,

$$\beta_{x,\text{sext}} \ll 60 \ \text{m} \quad . \tag{47}$$

If we place the horizontal scrapers at a relatively high β_y point, *i.e.* at $\beta_y \simeq 600$ m, then in order to ensure scraper protection, β_x at this point must be greater than 1,400 m. In fact we chose

$$\beta_{x,\text{scr}} = 2,000 \ \text{m} \tag{48}$$

which implies a scraper gap of 700 μm for $5\sigma_x$ scraping. Once the β-function at the scraper is fixed, the β-function at the sextupoles follows,

$$\beta_{x,\text{sext}} = 0.1 \ \text{m} \quad . \tag{49}$$

We now address the question of geometric and resistive wall wakefields at the horizontal scrapers. Again here both wakefield kicks must be below 1/5 σ'_x. These conditions are simultaneously satisfied if the horizontal scrapers, assumed 10 cm long, are tapered by an angle of 30 mrad. Each tapered section of the scrapers is then 15 cm long.

Finally we check to see if the horizontal geometric wakefield kick from the sextupoles is below the 1/5 σ'_x limit. It turns out that this condition is satisfied for

$$\beta_{x,\text{sext}} \leq 170 \ \text{m} \quad , \tag{50}$$

well above our design value of 0.1 m for $\beta_{x,\text{sext}}$.

Lattice—Energy collimation

A lattice design which satisfies the above specifications is presented in Fig. 5. It starts with a $-I$ transformation where horizontal and vertical scraping of the first phase space direction takes place. This is followed by a 2π section dedicated to energy collimation. Next there is a $3\pi/2$ in the horizontal plane and $\pi/2$ in the vertical plane transformer section. A phase advance of $\pi/2$ in both planes would have been possible at the expense of considerable increase in length. The last section of the line is identical to the first one. It is used to scrape the second phase space direction and energy again. The total length of the system is about 500 m.

Energy collimation is done by transforming off-energy particles to large amplitude ones through the introduction of horizontal dispersion. There are two scrapers in each energy scraping section placed at high dispersion points. The horizontal and vertical β functions at these locations are the same as the ones at the horizontal scrapers. Both energy scrapers consist of a thin ($\simeq$ 3 RL) and a thick part ($\simeq$ 20 RL). The thin part will be responsible for the primary beam energy collimation. By making it thin we bypass protection problems that occur within the body of the scraper. The role of the thick part will be to absorb the debris from both horizontal and energy collimation that has occurred upstream.

Furthermore each of the two energy collimation sections includes a normal sextupole pair forming a $-I$ transformation. Their function is to correct the horizontal chromaticity. To correct the vertical chromaticity a small amount of vertical dispersion has been added to the lattice at the skew sextupoles. Simulations show that this entire lattice demonstrates an excellent behavior with respect to chromatic and chromo-geometric aberrations in both transverse planes.

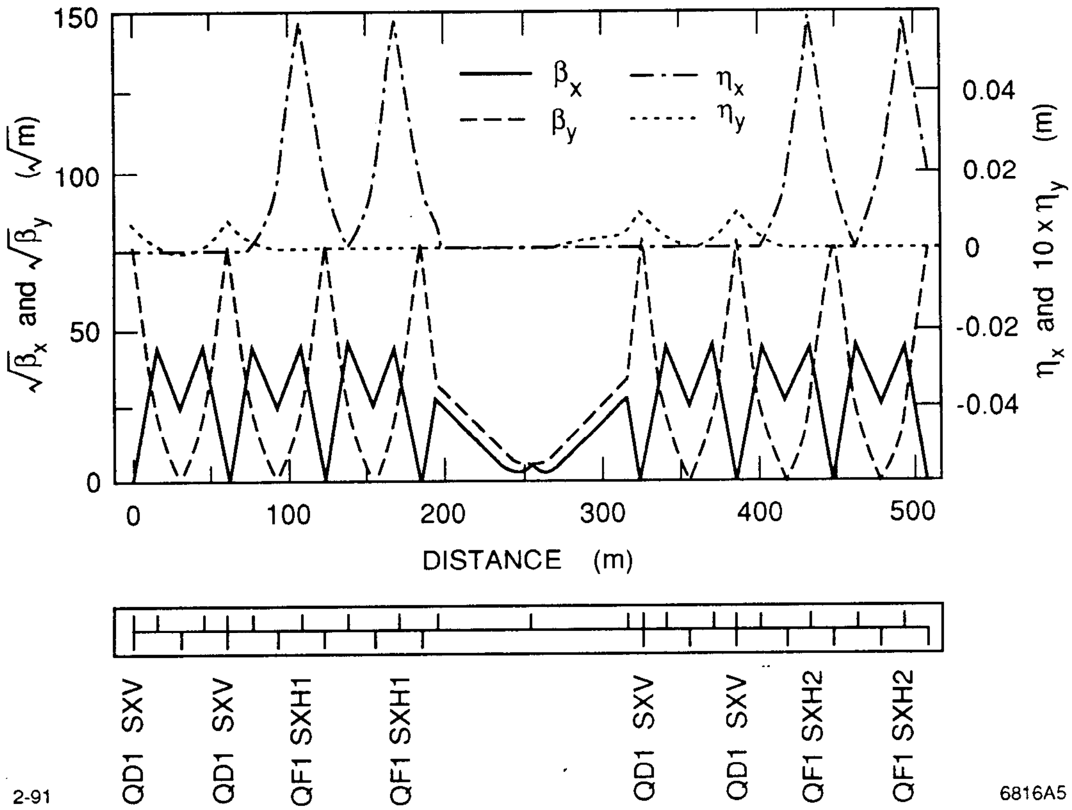

Figure 5: Optics design for the collimation systems in the NLC.

Stability tolerance on scraper offset

In deriving some of the above conditions we have assumed that the offset through the middle of the scraper is of the order of the beam size. Since the beam size at the vertical scrapers is 0.20 μm, the stability tolerance on the scraper offset is also

$$y_{0,\mathrm{scr}} \leq 0.20\ \mu\mathrm{m} \quad . \tag{51}$$

From Eq. (8) one can estimate an absolute steering tolerance by requiring that

$$(\Delta y')_{\mathrm{rw}} \leq \frac{1}{5}\sigma'_{y,\mathrm{scr}} \tag{52}$$

and solving for Δy. It turns out that this tolerance is

$$\Delta y_{\mathrm{scr}} \leq 7.4\ \mu\mathrm{m} \quad . \tag{53}$$

Stability tolerance on sextupole offsets

In order to get some insight into the question of tolerances we derive a general result for the tolerance on the sextupole offset. If we combine the scraping condition Eq. (24) with the requirement that the quadrupole-like kick due to the sextupole offset $y_{0,\mathrm{sext}}$ must satisfy Eq. (29),

$$(2Sy_{0,\mathrm{sext}})y_{\mathrm{rms}} \leq \frac{1}{5}\sigma'_y \quad , \tag{54}$$

we arrive at

$$y_{0,\mathrm{sext}} \leq \frac{5}{2}\frac{R_{12}\epsilon_y}{g_y} \quad . \tag{55}$$

Notice that the only parameters that can affect this offset tolerance are effectively the length of the system (via R_{12}) and the scraper gap. For our choice of parameters this tolerance is

$$y_{0,\mathrm{sext}} \leq 0.14\ \mu\mathrm{m} \quad . \tag{56}$$

Protection of scrapers

As we mentioned in the Introduction there are two problems associated with a train of bunches hitting the scrapers: the first occurs at the surface of the scraper while the second occurs in the body of the scraper. The surface of the scrapers is protected by design. More precisely, at the horizontal scrapers the area occupied by one σ of the beam is

$$\sigma_x\sigma_y = 140\ \mu\mathrm{m} \times 7.9\ \mu\mathrm{m} = 1,100\ \mu\mathrm{m}^2 \quad , \tag{57}$$

beyond the 900 $\mu\mathrm{m}^2$ limit quoted earlier.

At the vertical scraper on the other hand, one can calculate the scraper area on which $1\sigma_x \times 1\sigma_y$ particles

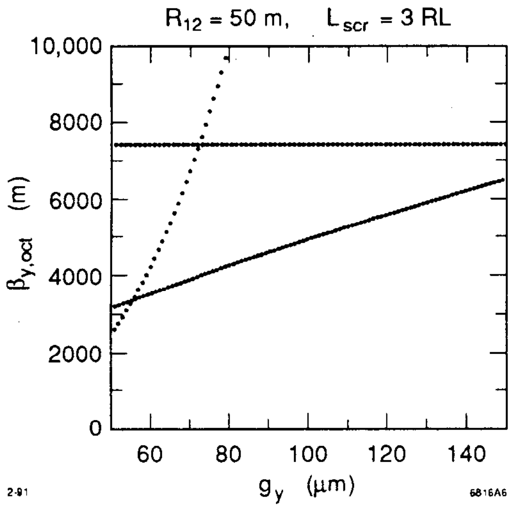

Figure 6: Parameter space for nonlinear collimation with octupoles.

at the sextupoles are mapped, if the beam is missteered by an amount greater than 5σ. It turns out to be

$$\sigma_x \text{``}\sigma_y\text{''} = 83\ \mu\text{m} \times 53\ \mu\text{m} = 4,400\ \mu\text{m}^2 \quad , \tag{58}$$

far beyond the 900 μm^2 limit.

The problem of the body of the scrapers is solved by making the scrapers short, 3 RL of the material.

B2. SCHEME WITH OCTUPOLE PAIRS

It is of interest to calculate the stability tolerances for octupole magnets. It turns out that for octupoles

$$y_{0,\text{oct}} \leq \frac{25}{3\sqrt{3}} \frac{R_{12}\epsilon_y}{g} \tag{59}$$

which leads to tolerances about a factor of 2 looser than for Eq. (55) with the same choice of parameters. We plotted the parameter space for octupoles for $R_{12} = 50$ m (Fig. 6), assuming that the octupoles have pole-tip field equal to 1.2 Tesla, pole-tip radius of 1 mm and length of 1 meter. There is indeed a solution for a scraper gap of 90 μm which will have more relaxed offset tolerances, however tracking indicates that the long-octupole aberration degrades the performance of this scheme. Also the octupoles are hard to build.

B3. COLLIMATION WITH DECAPOLES

The idea here is to use a decapole magnet to drive the beam tails to large amplitudes which can then be cut off by a mechanical scraper placed $\pi/2$ in phase advance downstream of the decapole. Since the decapole field does not vary rapidly within the small distances that correspond to the core of the distribution, one might hope that the decapole aberrations remain below a tolerable level. We examine whether the scraping requirement is indeed compatible with tolerable decapole aberrations.

Scraping with decapoles

A 5σ particle at the decapole will experience a kick

$$\Delta y' = D(5\sigma)^4 \tag{60}$$

where D is the decapole integrated strength

$$D = \frac{B_{\text{pole}} L_{\text{deca}}}{a^4 (B\rho)} \quad . \tag{61}$$

This kick will give rise to an offset at the downstream scraper

$$\Delta y_{\text{scr}} = R_{12} \Delta y'_{\text{deca}} \tag{62}$$

where R is the transfer matrix between decapole and scraper. From Eqs. (60) and (62) we derive the scraping condition

$$C_4 R_{12} \beta^2_{\text{deca}} \geq g_y \tag{63}$$

where

$$C_4 = 5^4 D \epsilon_y^2 \quad . \tag{64}$$

Decapole aberration

We require that the rms value of the decapole kick be less than 3/5 σ'_y, so that the core beam size will increase by less than about 20%. Since DC offsets do not cause emittance enlargement, we subtract the average value of the kick,

$$D(y^4 - \langle y^4 \rangle)_{\text{rms}} \leq \frac{3}{5} \sigma'_y \quad , \tag{65}$$

which implies

$$\frac{20\sqrt{6}}{3} D \epsilon_y^{3/2} \beta^{5/2} \leq 1 \quad . \tag{66}$$

Conditions (63) and (66) are plotted in Fig. 7 for $R_{12} = 100$ m and $g_y = 50$ μm.

The two curves intersect at $L_{\text{deca}} = 194$ m! Since the allowed working point must lie simultaneously above the top curve and below the bottom curve, clearly there is no solution with this scheme.

IV. CONCLUSIONS

We have illustrated several collimation schemes for a TeV linear collider. We have precluded the possibility of using mechanical scraping for the vertical plane. We presented a possible alternative which employs mechanical collimation for the horizontal plane and nonlinear collimation (scheme with skew sextupole pairs)

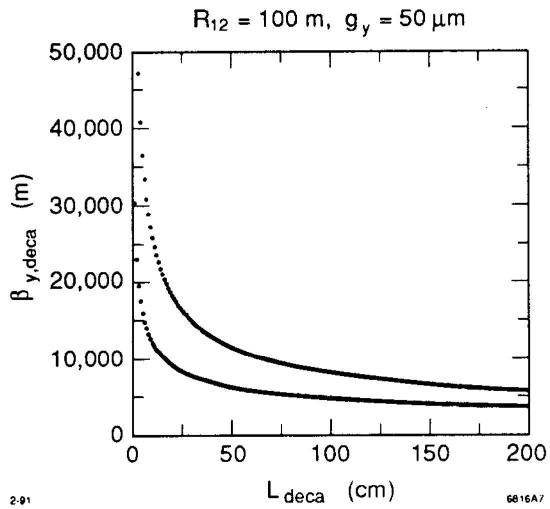

Figure 7: Parameter space for nonlinear collimation with decapoles.

for the vertical. This design succeeds in satisfying all of the requirements imposed on collimation systems, including effective collimation of transverse and energy tails, control of wakefield effects, protection of scrapers, and control of geometric and chromatic aberrations. The stability tolerances at the scrapers and sextupoles are similar to those occurring in the NLC Final Focus system; given the precision of the beam position monitors envisioned for an NLC, these tolerances should not rule out nonlinear collimation as a candidate for beam scraping in a future linear collider.

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