





Gamma-ray Large Area Space Telescope



GLAST Large Area Telescope:

AntiCoincidence Detector (ACD) Pre-Ship Review

ACD Team NASA Goddard Space Flight Center







SECTION	PRESENTOR	TIME		
Introduction	T. Johnson	8:00-8:10		
ACD Overview	D. Thompson	8:10-8:20		
Requirements, Segway into Environmental Testing	M. Amato	8:20-8:30		
Environmental Testing Overview	C. Coltharp	8:30-8:35		
Electrical Testing	M. Amato	8:35-8:45		
Mechanical Testing Results	K. Segal	8:45-9:30		
Thermal Testing Results	C. Peters	9:30-10:00		
Break		10:00-10:10		
CPT and Performance Testing Results	D. Thompson	10:10-10:50		
Verification and Resource Margins	M. Amato	10:50-11:35		
Product Assurance (PR/PFR Status)	J. Lohr	11:35-12:00		
Lunch (pizza party)		12:00-1:30		

ACD PSR	Agenda (Afternoon)		8 August 20	05
SECTION		PRESENTOR	TIME	
Risk Management		T. Johnson	1:30-1:45	
Project Review Activity		T. Johnson	1:45-1:50	
ADP and Deliverables		C. Coltharp	1:50-2:05	
Transportation		K. Harris	2:05-2:20	
Safety		D. Kofeldt	2:20-2:30	
PSR Summary		T. Johnson	2:30-2:35	
Closeout		Review Team	2:35-3:00	







Installing the MMS



Integrated ACD with MMS

Integrated the MMS

-Challenging job was performed flawlessly, one day before a temporary stand down of critical lifts at Goddard.





- Completed ACD functional and performance testing.
 - This required that the ACD be rotated on its side to orientate the side Tile Detector Assemblies perpendicular to the flux of Cosmic Ray Muons.



ACD being rotated on its side (cover in place to provide protection from Helium exposure) for performance testing







Fully integrated ACD on the C220 shaker in Building 7

Successfully completed vibration and acoustic testing!



The ACD in the acoustics chamber







Lowering the ACD over the Tracker thermal simulator (required to drive the temperature of the ACD)

Prepared for the ACD Pre-Ship Review on August 8.

Successfully completed Thermal Vacuum testing



Installed in Facility 225







 Successfully completed Mass
 Property testing

Installed on the Mass Property Measurement Facility

Prepared for today's Pre-Ship Review!







ACD OVERVIEW

Dave Thompson

ACD Instrument Scientist



INSTRUMENT OVERVIEW

ACD PSR



The Anticoincidence Detector (ACD) is a subassembly of the GLAST Large Area Telescope (LAT)

- Precision Si-strip Tracker (TKR) 18 XY tracking planes. Single-sided silicon strip detectors (228 µm pitch) Measure the photon direction; gamma ID.
- Hodoscopic CsI Calorimeter(CAL) Array of 1536 CsI(TI) crystals in 8 layers. Measure the photon energy; image the shower.
- Segmented Anticoincidence Detector (ACD) 89 plastic scintillator tiles. Reject background of charged cosmic rays; segmentation removes self-veto effects at high energy.
- Electronics System Includes flexible. robust hardware trigger and software filters.



Systems work together to identify and measure the flux of cosmic gamma rays with energy 20 MeV - >300 GeV.



Level III Key Requirements Summary



ACD PSR Reference: LAT-SS-00016 **Parameter** Requirement **Expected Performance** Verification Method **Detection of Charged** \geq 0.9997 average detection efficiency over entire >0.9997 Test and **Particles** area of ACD (less for bottom row of tiles) Analysis ≥0.99 (bottom tiles) Fast VETO signal Logic signal 200-1600 nsec after passage of charged 200-1600 nsec Demonstrate particle PHA signal For each phototube, pulse height measurement for each Trigger Acknowledge (TACK) Test and Below 10 MIP, precision of <0.02 MIP or 5% Analysis < 0.02 MIP or 5% (whichever larger) Above 10 MIP, precision of < 1 MIP or 2% (whichever < 1 MIP or 2% larger) False VETO rate -< 20% false VETO's due to calorimeter backsplash < 20% Test and backsplash at 300 GeV **Analysis** False VETO rate - noise < 1% < 1% gamma-ray rejection from false VETO's due to Analysis electrical noise Yes High Threshold (Heavy Detection of highly-ionized particles (C-N-O or heavier) Analysis Nuclei) Detection for calorimeter calibration. Size <1800 x1800 x 1025 at Outside: 1820 x1820 x 1050 mm Demonstrate hardpoints 1827 x 1827 for lowest 310mm ~1820 x 1820 x 1050 at Inside Grid: 1574 x 1574 x 204.7 mm softpoints Inside TKR: 1515.5 x 1515.5 x 650 mm 1574 x 1574 x 204.7 >1515.5 x 1515.5 x 650 < 295 kg 278 kg Demonstrate Mass < 11.5 Watts (conditioned) <11.5 Watts Demonstrate Power Instrument Lifetime Minimum 5 yrs > 5 yr. Analysis



INSTRUMENT OVERVIEW ACD





Interface to LAT

TILE SHELL ASSEMBLY

- 89 Plastic scintillator tiles
- Waveshifting fiber light collection (with clear fiber light guides for long runs)
- Two sets of fibers interleaved for each tile
- Tiles overlap in one dimension
- 8 scintillating fiber ribbons cover gaps in other dimension (not shown)
- Supported on self-standing composite shell
- Covered by thermal blanket + micrometeoroid shield (not shown)

BASE ELECTRONICS ASSEMBLY

- 194 photomultiplier tube sensors (2/tile)
- 12 electronics boards (two sets of 6), each handling up to 18 phototubes. Two High Voltage Bias Supplies on each board.







INSTRUMENT OVERVIEW





Completed ACD, with all detectors and electronics

ACD with Micrometeoroid Shield and Multi-Layer Insulation (except for Germanium/Kapton outer layer)



System Test Planning Test Overview



REQUIREMENTS

Michael Amato

ACD Systems Engineer



Level III Key Requirements Summary



ACD PSR Reference: LAT-SS-00016 Verification **Parameter** Requirement **Expected Performance** Method Detection of Charged Test and \geq 0.9997 average detection efficiency over entire >0.9997 **Particles** Analysis area of ACD (less for bottom row of tiles) ≥0.99 (bottom tiles) 200-1600 nsec Demonstrate Fast VETO signal Logic signal 200-1600 nsec after passage of charged particle PHA signal For each phototube, pulse height measurement for each Trigger Acknowledge (TACK) Test and Below 10 MIP, precision of <0.02 MIP or 5% Analysis < 0.02 MIP or 5% (whichever larger) Above 10 MIP, precision of < 1 MIP or 2% (whichever < 1 MIP or 2% larger) False VETO rate -< 20% false VETO's due to calorimeter backsplash < 20% Test and backsplash at 300 GeV Analysis < 1% False VETO rate - noise < 1% gamma-ray rejection from false VETO's due to Analysis electrical noise High Threshold (Heavy Detection of highly-ionized particles (C-N-O or heavier) Yes Analysis Nuclei) Detection for calorimeter calibration. Size Outside: 1820 x1820 x 1050 mm <1800 x1800 x 1025 at Demonstrate hardpoints 1827 x 1827 for lowest 310mm ~1820 x 1820 x 1050 at Inside Grid: 1574 x 1574 x 204.7 mm softpoints Inside TKR: 1515.5 x 1515.5 x 650 mm 1574 x 1574 x 204.7 >1515.5 x 1515.5 x 650 < 295 kg 278 ka Demonstrate Mass <11.5 Watts < 11.5 Watts (conditioned) Demonstrate Power Minimum 5 yrs Instrument Lifetime > 5 yr. Analysis

秦 Key Level III Requirement Changes Since CDR 🥸



ACD PSR

Reference: LAT-SS-00016

8 August 2005

Parameter	Requirement at CDR	Current Requirement				
Detection of Charged Particles	\geq 0.9997 average detection efficiency over entire area of ACD (less for bottom row of tiles)	No change since CDR				
Fast VETO signal	Logic signal 200-1600 nsec after passage of charged particle	No change since CDR				
PHA signal	For each phototube, pulse height measurement for each Trigger Acknowledge (TACK)	No change since CDR				
	Below 10 MIP, precision of <0.02 MIP or 5% (whichever larger)					
	Above 10 MIP, precision of < 1 MIP or 2% (whichever larger)					
False VETO rate - backsplash	< 20% false VETO's due to calorimeter backsplash at 300 GeV	No change since CDR				
False VETO rate - noise	< 1% gamma-ray rejection from false VETO's due to electrical noise	No change since CDR				
High Threshold (Heavy Nuclei) Detection	Detection of highly-ionized particles (C-N-O or heavier) for calorimeter calibration.	No change since CDR				
Size	Outside: 1796 x1796 x 1050 mm	Outside: 1820 x1820 x 1050 mm				
	1806 x 1806 for lowest 310mm	1827 x 1827 for lowest 310mm				
	Inside Grid: 1574 x 1574 x 204.7 mm	Inside Grid: 1574 x 1574 x 204.7 mm				
	Inside TKR: 1515.5 x 1515.5 x 650 mm	Inside TKR: 1515.5 x 1515.5 x 650 mm				
Mass	< 280 kg	< 295 kg				
Power	< 31 Watts (conditioned)	< 11.5 Watts (conditioned)				
Instrument Lifetime	Minimum 5 yrs	No change since CDR				









ACD Requirements Database



• ACD uses our Requirements Database in DOORS to Track Requirements

ID	LAT ACD Subsystem Level III Requirements, LAT-SS-00016	Parent reg Link Comments	Link Action Items	ACD Le			
ACD2 14	other sources from which they derive are listed in the Requirements I able below.						
ACD2-1	5.2 Detection of Charged Particles	2		Require			
MUD-10 Ine AUD shall detect energy deposits with energies of above an adjustable threshold nominally at 0.3 MIP (minimum ionizing particle) (see 5.3 below) and produce VETO signals.							
ACD3-17	5.3 Adjustable Threshold on Detecting Charged Particle			<u>Dunious</u>			
ACD3-18	18 The threshold for VETO detection of charged particles shall be adjustable from 0.1 to 2.0 MIP, with a size of ≤0.05 MIP. (0.1 to 0.6 MIP would have been range if no degradation was expected)	step		(DOORS			
ACD3-19	9 5.4 Detection Efficiency						
ACD3-20	20 The average detection efficiency for minimum ionizing particles shall be at least 0.9997 over the entire area of the ACD (except for the bottom tiles on each side, for which the efficiency shall be at least .99 simulation confirmation of this number is desired at some point).	,	Latest GAP analysis h been sent to Alex for e simulation update	Active betwee			
ACD3-21	21 5.5 Instrument Coverage			Require			
ACD3-22	22 The ACD shall cover the top and sides of the LAT tracker down to the top of the Csl. The top of all sides of the ACD scintillator shall be extended upward so as to be at least as high as the highest point	4 ► tin					
	Active Links between Requirements			ACD-LAT			
	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352	In-links at depth 1	Req Action item Req	ACD-LAT DOOR			
LAT A -89 5.1 -90 Each (freq	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 10.5 HVBS Input Power h HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz.	 In-links at depth 1 ACD ICD LAT-SS-00363 ACDICD-45 	Req Action item Req	ACD-LAT DOOR Databa			
LAT A -89 5.1 -90 Each (freq -91 5.1	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 10.5 HVBS Input Power h HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz.	In-links at depth 1	Req Action item Req	ACD-LAT DOOR Databa			
LAT A -89 5.1 -90 Each (freq -91 5.1 -92 The)	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 10.5 HVBS Input Power In HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz. 10.6 HVBS Line and Load Regulation HVBS output voltage shall be regulated to ±0.5% for all combinations of input voltage and load	 In-links at depth 1 ACD ICD LAT-SS-00363 ACDICD-45 ACD Level III Requireme 	Req Action item Req	ACD-LAT DOOR Databa			
LAT A -89 5.1 -90 Each (freq -91 5.1 -92 The J curre	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 10.5 HVBS Input Power In HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz. 10.6 HVBS Line and Load Regulation HVBS output voltage shall be regulated to ±0.5% for all combinations of input voltage and load rent. (This produces ~5% change in PMT gain).	 In-links at depth 1 ACD ICD LAT-SS-00363 ACDICD-45 ACD Level III Requireme LAT-SS-00016 ACD3-18 	Req Action item Req	ACD-LAT DOOR Databa			
LAT A -89 5.1 -90 Each (freq -91 5.1 -92 The J curre	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 ID.5 HVBS Input Power In HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz. ID.6 HVBS Line and Load Regulation HVBS output voltage shall be regulated to ±0.5% for all combinations of input voltage and load tent. (This produces ~5% change in PMT gain).	 In-links at depth 1 ACD ICD LAT-SS-00363 ACDICD-45 ACD Level III Requireme LAT-SS-00016 ACD3-18 ACD Level III Requireme LAT-SS-00016 ACD3-20 	Req Action item Req nts	ACD-LAT DOOR Databa <u>ACD Leve</u> Requirem Database			
LAT A -89 5.1 -90 Each (freq -91 5.1 -92 The 1 curre	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 ID.5 HVBS Input Power In HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz. ID.6 HVBS Line and Load Regulation HVBS output voltage shall be regulated to ±0.5% for all combinations of input voltage and load ent. (This produces ~5% change in PMT gain).	 In-links at depth 1 ACD ICD LAT-SS-00363 ACDICD-45 ACD Level III Requireme LAT-SS-00016 ACD3-18 ACD Level III Requireme LAT-SS-00016 ACD3-20 	Req Action item Req nts	ACD-LAT DOOR Databa <u>ACD Lev</u> <u>Requirem</u> <u>Database</u> (DOORS)			
LAT A -89 5.1 -90 Each (freq -91 5.1 -92 The l curre	Active Links between Requirements ACD Subsystem Level IV Requirements and Verification Table, LAT-SS-00352 D.5 HVBS Input Power In HVBS shall operate from a supply voltage of 28V ± 1V, with possible input ripple of 10 mV quency range 50 Hz to 50 MHz). The noise shall be less than 100 mV RMS from DC to 1.0 MHz. D.6 HVBS Line and Load Regulation HVBS output voltage shall be regulated to ±0.5% for all combinations of input voltage and load ent. (This produces ~5% change in PMT gain). D.7 HVBS Output Ripple HVBS output voltage ripple shall be compatible with the ACD ASIC design. The HVBS output	 In-links at depth 1 ACD ICD LAT-SS-00363 ACDICD-45 ACD Level III Requireme LAT-SS-00016 ACD3-18 ACD Level III Requireme LAT-SS-00016 ACD3-20 ACD Level III Requireme 	Req Action item Req nts nts	ACD-LAT DOOR Databa <u>ACD Leve</u> <u>Requireme</u> <u>Database</u> (DOORS)			



ACD Requirements





• Some important requirements flow through a science simulation

ACD Simulation Input Parameters







$\boldsymbol{\cdot}$ CHANGES IN THE LAT ICD

CHANGE REQUEST	DESCRIPTION	REASON
LAT-XR-842-03	1. Updated CG requirement	1. Correct known errors
(Pre-LAT CDR)	2. Connector specifications	2. Clarification and
	3. Flight and test instrumentation (thermal and	finalization of requirements.
	vibration) specifications	3. Finalize requirements
	4. Clarification on optical survey	4. Finalize requirements
	and measurement	5. Required for PMTs
	5. Added helium mitigation plan	
LAT-XR-774-02	1. Dead Time Requirement	1. Clarification
	2. Adjustable High Threshold	2. Adjusted slightly
	 Low Threshold signal and adjustment 	3. Deleted. Replaced by zero suppression
	4. Mass allocation	4. Increase required
	5. Micrometeoroid protection	5. Relaxed requirement due to new reliability assessment





CHANGES IN THE LAT ICD

CHANGE REQUEST	DESCRIPTION	REASON
LAT-XR-02469-01	 Power allocation reduced Z-axis CG lowered 	<i>1. Reduced from 31W to 10.5W average nominal</i>
	3. Detector coverage of Trackers	2. Reduced from 393mm to 330mm
		3. Clarified position of detectors with respect to the LAT
LAT-XR-03019-01	Helium limitation requirement	Helium exposure limit increased
LAT-XR-04774-01	BEA survival temperature	Increased from -40C to -30C due to concern about PMT glass failure
LAT-XR-03304-01	 Connector locations Added external triggers 	1. Changed location of some connectors
	3. MLI interface	2. Required to test ACD
	4. Vent path	3. Clarified
		4. Clarified





CHANGES IN THE LAT ICD

CHANGE REQUEST	DESCRIPTION	REASON
LAT-XR-04696-01	1. ACD mass	1. Increase required
	2. Bottom Tile Detector Assembly location	2. Better definition required.
	3. Connector location	3. Detail added
	4. GARC Reset	4. Solution for GARC reset
	5. LVDS termination resistor	issue implemented
	tolerance	5. Tolerance was not
	6. Cable impedance	previously specified
	7. Power supply voltage range	6. Requirement added
	8. 28V and 3.3 V power supply current limiting and	 Changed requirement from 27-29 V to 24-29 V
	<i>monitoring requirements added</i>	8. Required for safety and monitoring of ACD
	9. Grid surface	9. Changed from alodine to black anodize





$\boldsymbol{\cdot}$ CHANGES IN THE LAT ICD

CHANGE REQUEST	DESCRIPTION	REASON
LAT-XR-05240-01-01	 ACD mass Z-axis CG 	 Increase required Increased from 330mm to 340mm
LAT-XR-06717-01	 Interface cable design Grounding Maximum power MLI grounding 	 Updated to reflect current design Updated FREE board to chassis ground details Updated maximum power dissipation Added detail

CHANGES IN LAT IDD -

- More defined stay clears, connector locations, hardware
- Change in location of blanket interface moved up from bottom of ACD
- Addition of ACD blanket ground plate and probable harness run paths
- Insert call out change





TESTING OVERVIEW

Test Verification Matrix



Note : Many tests needed by items are done at a higher subassembly, so also look up in higher assemblies for a test. Green rows – hight, yellow - eng model, white - spares or development

--Not done at P.E.R., Complete now --Descoped

Note : Electronics board components and other small part qualification and testing (i.e Garc, GAFE, HVBS cpacitors, Mech fastners etc..) is captured in the ACD parts program plan

	Green rows - Flight component rows Yellow rows - Engineering Model rows Item - major subassemblies in bold	evel of Assembly	nit Type	up pil er	est Levels	est Status	lodal Survey (tow level sine rvey)	tatic Loads	ine Burst	ine Vibration	an dom Vibration	lechanical Function/	ptical Performance Testing	coustics	lass Properties	iterface Verif.	V C/EMI	SD Compat (Grounding?)	lag netics	creening Process	liveness (A) / Functional (F) Comprehensive (C)	f 12 cyc for qual, 4 for ccpt)	hermal Cycle	bermal Balance	IMPORTANT NOTES
	FULLY INTEGRATED ACD	s	F	GSFC	Prtoflt		x		*	x			x	x	x	,	*	x	T		с	4		x	Protoflight Levels - qualification levels at reduced durations, possibly lotched. Acoustic to qual files, i.e. "sine burst and EMI descoped at this level ending walver, need to determine exactly which props measured in mass prop
	Tile Shell Assembly	24	F	CSEC	Acot										Y I										
[Tile Shell Assembly - partial	SA	D	GSFC	Qual		х	х	х	х	х	х			х							6			All qual units need total of 12 cycles, TDA already has seen 6, making exception for some purely mech subsystems
[ACD Mechanical Subsystem (no	S	F	GSFC	Qual		X-e		Х-е	X-e		Х		Х	Х										ACD Structure wimass sims, no elect or det, LAT mass simulator needed ?
[Shell	С	F	TBD	N/A										Х										Do thermal vac because you have to bake out anyway
[Shell - partial	Ρ	D	GSFC	Qual			X-b																	
[Tile Detector Assembly	SA	F	Fermilab	Acpt								Х		Х						A, F				89 Fit TDAs one fit unit may see therm vac before assemb to shell
1	Tile Detector Assembly	SA	S	Fermilab	Acpt				Х	Х			Х	Х	х							12			24 spares
	Tile Detector Assembly	SA	ЕМ	Fermilab	Qual				х	х	X-m		х		х						F	6			20 TDAs. The 6 them vac cycles should have been 12, we may need to do 6 more to qual
[Tile Detector Assembly	SA	D	Fermilab	Qual								Х									12			Functional testing code660
	TDA Tiedown (Flexure)	Р	F	GSFC	Prtofit																				Test bonded joint
	TDA Tledown (Flexure)	Р	EM	GSFC	Qual			Χ?	Х	Х	X-m	Х			Х										Test bonded joint
	TDA Tiedown (Flexure)	P	D	GSFC	Qual			X-b																	Characterize flexures
I	WSF/Clear Fiber Connector	С	F	GSFC	Acpt								Х		х						A, F				
_ I	WSF/Clear Fiber Connector	С	EM	GSFC	Qual			Х	Х	Х	X-m	Х	Х		х						F				
L	WSF/Clear Fiber Connector	С	D	GSFC	Qual								Х								A		8		Several development models
	Base Frame	С	F	GSFC	Qual			х				х			х	х									Lift interface at this level, could also be done at ACD mech subsystem level
	Partial BFA & Electronics Chassis	SA	ЕМ	GSFC	Qual				Х?	X?	X?-m					х	х	х			F				Corner or one side BFA, BEA assemb. T.V.deleted. All other testing in the base frame may be eliminated except for EMI
	Base Frame - partial	С	D	GSFC	Qual														_						No env tests planned at this time
	Shleid & Thermal Blanket	С	F	GSFC											х								X*		Similarity to dev. Model, " therm cyccle is really bakeout
	Shield & Thermal Blanket -see rema	С	EM	GSFC										_	Х										May not build Eng Model, Similarity to dev. model
	Shleid & Thermal Blanket	С	D	JSC, GSF	Qual									_	_	\rightarrow	\rightarrow	_	_	_					Characterize thermal perf., particle impact
	Clear fiber cable assembly	SA	F	GSFC	Qual								Х	_	_	\rightarrow	\rightarrow	_	_	_	A				
	PMT/Fiber Connector	С	F	GSFC									Х	_	_						A				any spares not in a TDA will need to see testing
	PMT/Fiber Connector	С	EM	GSFC	Qual					Х	X	Х	Х	_	_	_	_		_	_	F	6			
	PMT/Fiber Connector	C	D	GSFC	Qual	-							Х	_			_	_	-	_	F		8		Several development models
	Base Electronics Assembly	S	F	GSFC	Acpt	-								-	X	X	-	_	-	-	F				
	Electronics Chassis	SA	F	GSFC	Acpt		X			X	X-M			_	х	X	_	_	_	-	F	4			(FREE, HVBS, PMT)
	Electronics Chassis	SA	s	GSFC	Qual		х		х	х	X-m				х	х					F	12			(PREE, PVDS, PMT), Same lessing as ingrit units but quarrequires 12 1.V. cycles, this is the first flight chassis we build, used as qual
	Electronics Chassis	SA	ЕМ	GSFC	Qual		x		x	x	X-m				x	x					F	4			(FREE, HVBS, PMT). All qual units usually need total of 12 cycles, the thinking is that this is not flight like enough to use for qual so spare (first flight chassis built) is qual unit, may go to 12 cycles anyway. HOWEVER first flight chassis built (probably the spare) will go through same qual tests specified for EM unit
1	Electronics Chassis	SA	D	GSFC	N/A											х					F				(FREE, HVBS, PMT), thermal vac wont be done here if EM is almost ready



Performance Test

Tile Flexure NDI

Mass Properties

Sine Survey

SA

Static Test of Tile Flexures

Partial Shell Assy + TDA

Top Level Environmental Test Flow (from matrix UPDATE)



Now successfully completed! Subsyste Low Level Sine Mass Properties oSine Vibe **Remaining Tests** Thermal Vac (4 cycles) o Opt. Performance Acoustic Vibe 5 MMS/ Blanket Analysis Mass Properties BEA o MMS Ballistic Test (eng unit) Interface Verification o Thermal Vacuum Performance Test Α Α Modal Survey o Electronics Chassis Mass Prop. 0 0 Sine Vibe 0 Interface Ver. 0 Random Vibe Shell & BFA w/Mass Simulation Functional Test <u></u> 0 EMI/EMC Mechanical Subsystem Models А Low Level 0 Mechanical Partial BFA +Chasis lectronics Sine Strength Test hassis Modal Survey o 0 Mass Prop. Sine Burst Acoustics 0 0 Sine Burst Interface Ver. 0 0 Sine Vibe Mass Properties Sine Vibe Functional Test 0 0 Q Random Vibe EMI/EMC O 0





Testing Descopes



 EMI tests on the full ACD were moved to LAT level. Tests on all chassis were done but tests on the full ACD with the noisy GASU EGSE were not likely to be useful and they were expensive

Waivers approved

- EMI at ACD system level waiver (reasons covered in PER)
- Thermal Balance waiver (covered in PER, the result is that a few ICD thermal interface requirements are only verified via analysis and only indirectly from thermal vacuum results, LAT not very sensitive to ACD thermal interface number variances)







Environmental Test Flow And Functional Testing Results

Craig Coltharp Integration and Test Manager, Code 568





Test Facilities Used



- Vibration Facility
 - GSFC's MB C-220 Exciters (4,082Kg)
 - performed ACD TSA structural verification
- Acoustics Facility
 - GSFC's Acoustic Facility
- Thermal Vacuum Facility
 - Chamber 225
 - 9' dia X 14' long
 - -310F to 302F
- Mass Properties
 - GSFC's MPMF (4,536Kg)



PLANS



GLAST LAT ACD Subsystem Verification Plan ACD-PLAN-000050 **ACD Configuration Management Plan** ACD-PLAN-000107 **ACD Helium Monitor and Control Plan** ACD-PLAN-000152 **ACD Integration and Test Plan** ACD-PLAN-000350 **ACD-On-Ground Science Performance Calibration and Monitoring** ACD-PLAN-000332 ACD Flight Instrument Protoflight Vibration Test Plan ACD-PLAN-000334 ACD Flight Instrument Protoflight Acoustic Test Plan ACD Flight Thermal Vacuum Test Plan ACD-PLAN-000347 **GLAST ACD Instrument and GSE Packaging, Handling,** and Transportation Plan



Procedures



- ACD Mechanical Handling Procedure
- GLAST ACD Light Tight Test Procedure
- Comprehensive Performance Test Procedure
- ACD Redline Procedure for Engineering Documentation
- GASU #8 Safe to Mate Procedure
- ACD GN2 Purge Structure Removal Procedure
- ACD-Monitor Operational Test Procedure
- Aronson Table Operation Procedure

ACD-PROC-000195 ACD-PROC-000252 ACD-PROC-000270 ACD-PROC-000284 ACD-PROC-000333 ACD-PROC-000336 ACD-PROC-000346 ACD-PROC-000349





- Prior to environmental testing during functional & performance testing
 - approx 300 hours
- Hours accumulated during environmental test flow
 - Prior to TVAC 24 hours
 - TVAC 131 hours
 - Post TVAC 8 hours


ACD - Post Delivery Flow (as of 8/5)

5) 8 August 2005



*- Based on ship date of August 12, could ship as early as August 10.





TESTING -ELECTRICAL



Electrical Interface







Electrical Testing Summary



- Please recall that all electrical testing on individual chassis was complete and covered at P.E.R. There is no interdependency or connections between chassis. All that was left was to test all of then at once with the EGSE GASU instead of one at a time and to get overall performance data.
- Partial Summary of the tests done -
 - ASIC part life, thermal cycle, burn in, and radiation testing
 - PMT and PMT subassembly performance, qualification and acceptance testing
 - FREE board performance, qualification and acceptance testing
 - HVBS board performance, qualification and acceptance testing
 - Complete Electronic Chassis performance, qualification and acceptance testing





ACD Mechanical Pre-Ship Review

Aug 2005

ACD Mechanical Team

Ken Segal / Code 543, ACD Lead Mechanical Engineer

Ryan Simmons / Code 542, ACD Lead Mechanical Analyst



ACD Mechanical PER Presentation Outline



- ACD Mechanical Verification Testing
 - Test Levels
 - Sine Vibration and Acoustic Test Configurations
 - Sine Vibration Test
 - Acoustic Test
 - Dimensional Survey
 - Mass Properties Tests
- Conclusions



Test Levels



Swept sine and acoustic protoflight levels

- Sine testing will be limited to structural qualification test responses if required
 - X and Y-axes = 3.5g on the TSA
 - Z-axis = 4.0g on the TSA

X & Y Axes Sine Sweep Protoflight Level			
Frequency	Level	Sweep Rate	
(Hz)	(g, 0-pk)	(oct/min)	
5-15	2.5	4.0	
15-25	0.9	4.0	
25-35	0.9	1.5	
35-40	0.9	4.0	
40-50	1.9	4.0	

Z Axis Sine Sweep Protoflight Level			
Frequency (Hz)	Level	Sweep Rate	
5-15	0.4	4.0	
15-25	1.2	4.0	
25-35	2.7	1.5	
35-50	0.7	4.0	

Acoustic Protoflight Level		
1/3 Octave Center	Protoflight	
Frequency	Test Levels	
(Hz)	(dB)	
31.5	127.4	
40	130.3	
50	134.2	
63	135.1	
80	137.4	
100	134.9	
125	133.6	
160	131.6	
200	132.4	
250	129.6	
315	126.4	
400	122.9	
500	122.1	
630	119.6	
800	120.5	
1000	120.2	
1250	121.4	
1600	122.0	
2000	120.0	
2500	120.3	
3150	118.6	
4000	116.0	
5000	111.9	
6300	107.9	
8000	104.8	
10000	102.8	
Overall Sound Pressure	143.8	
Level (OASPL)		
Duration	60 sec.	



Test Configuration Sine Vibration and Acoustic Tests



- BFA and TSA shown on the vibration fixture
 - 2" plate
 - Eight mounting posts representing LAT I/F
- Not Shown
 - Additional 3" plate for thrust axis vibration
- Tested Configuration
 - Full ACD assembly minus GeKapton outer layer 0.83Kg (1.84lbs), MLI Velcro 0.3Kg
 - Removable accelerometer locations (accels located on inside of TSA)
 Fly-away accelerometers







Test Configuration Sine Vibration and Acoustic Tests



- Tested Configuration (Cont)
 - MMS Post Configuration
 - One cracked MMS post in place on +X side as shown
 - Passed test without catastrophic failure
 - Will replace with acceptance tested post
 - Drawing Configuration could not be met with hardware delivered
 - EO produced to reflect what we tested and what will fly







ACD Sine Vibration- Test Configuration

ACD PSR



- ACD Shown in Z- Axis Test Configuration on the vibration fixture
 - 2" plate and additional 3" plate for thrust axis vibration (z-axis only)
 - Eight mounting posts representing LAT I/F





ACD Sine Vibration Testing



 Lateral Axis Test and Test Configuration Shown





2.5

Acceleration (g)

0.5

ACD Sine Vibration Test Results



8X TSA - Post Sig. Sweep
 24X BFA - Pre Sig. Sweep

- Signature Sine Sweep:
 0.1g from 5-150 Hz
- Natural Frequencies
 - X = 70.77 Hz
 - Y = 71.0 Hz
 - **Z** = 69.25

irst frequency = 71.0 Hz

Responses from Accel. 9Y

Y-Axis

All first modes are on the TSA



esponses from Accel. 8)



ACD Sine Vibration Test Results









- ACD Passed Sine Vibration Tests No Problems Detected
 - Structurally OK
 - Pre and Post Performance Assessment Good
 - Documented in test report ACD-RPT-000363



ACD Acoustic Test Configuration

8 August 2005

• Test configuration

- Structure on the ACD dolly
- TSA cavity closed out at the vibe fixture (see next slide)
- Internal microphones installed (see next slide)
- Accelerometers same as in vibration tests
 - Accel #9 on the TSA +Y face detached prior to testing
- MMS and MLI installed
 - Again outer MLI layer of Germanium Kapton was not installed
 - Velcro for the LAT interface (along the bottom edge of the blankets) has not been installed.
- MMS Posts as described previously





ACD Acoustic Test Configuration



- Two internal microphones where placed inside the ACD cavity
- Sandbags were used to close out the cavity to simulate the presence of LAT









- Acoustic input was within protoflight specification
 - Input spec 143.8 dB
 - Shaped chamber at 143.7 dB (prior to bringing ACD in)
 - Final level 143.3 dB, well within the ±3dB limits





ACD Acoustic Test Results

0.000001 +



- ACD acoustic tests were nominal
- All responses were as expected
 - Prior component random vibration testing was to GEVS minimum workmanship level of 6.8 Grms (shown on plots)
 - Acoustic results show that minimum workmanship levels were conservative
- Chris Fransen, the GLAST acoustic analyst, is satisfied with the test results
- One post-test issue found (see next slide)



100

Frequency (Hz)

10000





• One Issues to Report

- PR 02324-001

- A Nut Plate like those used to secure tiles to tile flexure was found on floor in ACD +X, -Y corner after testing was completed.
- Assessment
 - The Nut plate is believed to have been on ACD dolly before testing started. The nut plate in question had debonded from the angled shim it was mounted to during TDA installation and was inadvertently left behind. During acoustic tests it shook free. If this came off the flight assembly, analyses show that a tile mounted with 3 fasteners shows positive margin of safety.



Where do nutplates reside? Where did this one come from?

Is it a structural or performance issue?

Where do nutplates reside? In Tile flexures at 508 locations on ACD to hold 89 tiles to the structure.





PR 02324-001

- A Nut Plate like those used to secure tiles to tile flexure was found on floor in ACD +X, -Y corner after testing was completed.
- Where did this nutplate come from? An angled shim used on 2nd and 3rd row side tiles (40).



Evidence-

The epoxy on the nutplate found has the impressions common to Angled Tile shims machining marks.

These are found in 160 places on the ACD.





PR 02324-001

- Assessment
 - A Nut Plate like those used to secure tiles to tile flexure was found on floor in ACD +X, -Y corner after testing was completed.
- Where did this nutplate come from? The nut plate is not from the ACD flight structure.
- Evidence:
 - Nut plates have a locking feature that requires 0.5 in-lbs to overcome the locking feature. The locking feature is not likely to be overcome through vibration or acoustic loadings.
 - One is being passed around for you to feel the locking grip.





PR 02324-001

- Assessment
 - A Nut Plate like those used to secure tiles to tile flexure was found on floor in ACD +X, -Y corner after testing was completed.
- Where did this nutplate come from? The nut plate is not from the ACD flight structure.

Evidence:

Nut plate is captured within a flexure by tape that surrounds each flexure to provide light tight seal. Light tight seal is validated through light tight testing.

Meaning: It is unlikely that a loose nutplate would get 'free'

Example of a taped

Flexures are Shown







PR 02324-001

- Assessment
 - A Nut Plate like those used to secure tiles to tile flexure was found on floor in ACD +X, -Y corner after testing was completed.
- Where did this nutplate come from? The nut plate is not from the ACD flight structure.

– Evidence

- The ACD had closeouts between the ACD and the 2" plate and covering the hole in the 2 inch plate
- Picture shows inside the ACD for the Acoustic test.
 - Notice: the wooden plywood used to closeout the 2" plate and the closeouts in place between the ACD and the 2" plate







PR 02324-001

Assessment

 A Nut Plate like those used to secure tiles to tile flexure was found on floor in ACD +X, -Y corner after testing was completed.

– Where did this nutplate come from?

 The Nut plate is believed to been on ACD dolly before testing started. The nut plate (one of 6) debonded from the angled shim it was mounted to during TDA installation.

- Evidence:

- Post Acoustic Test Inspection result:
- nutplate installation tool found in the +x,
 -y corner of the ACD dolly

- Meaning

 A nutplate replacement is likely to have occurred in this location and the nutplate may have been in this location and it was missed during cleanup.







• PR 02324-001

- Assessment
 - If the nutplate came off the flight structure.....Is it a structural or performance issue?
 - Analyses has been done for a tile mounted with 3 fasteners
 - Results show positive margin of safety for
 - -Fasteners
 - -Flexures
 - -Tiles

PR 02324-001 Conclusion

 The flight structure most probably did not shed any parts, and if one fastener is loose it does not pose a performance problem: therefore, proceed with ACD shipping.





- All mechanical test levels achieved.
- One post-test issue nutplate found on floor
- ACD Passed All Tests
 - Structurally Pre- and post-test signature sine sweeps agree excellently for swept sine testing
 - No indication of damage following acoustic testing (see previous slide)
 - Pre and Post performance assessment Good
 - Results documented in test report ACD-RPT-000363



ACD Mass Properties Results



ACD Mass

- Mass Requirement < 295Kg</p>
- Mass Measured = 283.2Kg (Margin of 11.8Kg)
- Mass Liens
 - SUBTRACT Thermal testing instrumentation, connector caps, Llumalloy cover.
 - ADDITIONAL Ge Kapton
 - ~0.83Kg spread over outer area
 - ADDITIONAL Velcro interface to MLI (for LAT MLI to ACD MLI interface)
 - ~ 0.3 Kg is below CG

• ACD CG

- Requirement is
 - X and Y < 6mm</p>
 - Z<340mm where Z=0 is the LAT Frame of Reference
- Configuration
 - ACD Secured to Vibration Test Setup and 3" plate
- Measured CG
 - X= +0.3mm
 - Y= -1.3mm
 - -Z = +310.2mm



ACD Dimensional Survey



- Dimensional Survey Is To Be Completed
- Requirements:
 - Bottom Edge of ACD Bottom Tile Detector = 158.17 ± 0.50mm (6.227 ± 0.020) in the +Z direction from the ACD-LAT interface plane.
 - Stay-clear Volumes IAW LAT-DS-00309, ACD-LAT Interface Definition Drawing
- Bottom Edge of ACD Bottom Tile Detector Verified to be 6.187"
 - Out of Requirement Tile is too low by 0.020"
 - Based on measurements:
 - 6.045 Channel Max Allowable Height
 - 0.125 Installation Measurement Tile Wrapping to Channel
 - 0.017 Tile Wrapping Measurement
 - ACD Team Believes the minus tolerance is in error (should be infinite)
 - WAIVER TO BE GENERATED



ACD Dimensional Verifications Interior Stay Clear Volume Violations



- Interior Stay Clear Volume Measurement Complete
 - Two violations established issues being addressed
 - Interior Wire on Tile Shell Assembly (TSA) inside Surface
 - Base Frame Assembly (BFA) Inside Surface



- An Interior Wire violates Interior Stay Clear by as much as 0.022"
 - A waiver has been written, sent to LAT, and waiver is in the signature cycle.





ACD Dimensional Verifications Interior Stay Clear Volume Violation-BFA August 2005





Survey To Be Completed



Conclusions



- VIBRATION ENVIRONMENTAL TESTS
 - ACD Passed All Tests
 - All test levels achieved.
 - Results documented in test report ACD-RPT-000363.
 - One post-test issue detected and addressed
- OPEN ISSUES
 - Complete CG Testing
 - Complete Dimensional Survey
 - Write and Get Dimensional Violation Waivers Signed





System Test Planning Thermal Test Overview

ACD Thermal Subsystem Carlton V. Peters ACD Thermal Engineer GSFC, Code 545



ACD Design Configuration

ACD PSR



- Anticoincidence Detector covers all five external sides of the LAT
- External MLI Blanket has 3 mil Germanium Black Kapton outer layer and is composed of 14 blanket layers
- Blanket will be attached using a combination of standard blanket attachments such as double sided tape and blanket buttons.
- Micrometeoroid shield includes approximately 3 cm of Solomide foam, Kevlar and Nextel layers
- Thin composite, low conductivity shell provides ACD structural support
- High emittance tracker exterior surfaces provide radiative path between tracker and ACD Shell interior
- Electronics Boards mounted to BEA Rail
- No dedicated radiator
- BEA mounted to grid at the 4 corners via corner fittings and at the center of each side by mid-span connectors





Thermal Design Approach



Tile Detector Assembly

- Passive thermal design approach
- The following ACD characteristics argue for a thermal design approach based on local thermal environment considerations for any of the five sides:
 - LAT Point anywhere anytime viewing requirements
 - TDA's located on all five ACD exterior sides
 - Poor lateral thermal conduction characteristics through the ACD TDA structural support (low conductivity composite shell)
 - No dedicated radiator

Electronics Board Interface

- Passive thermal design approach without survival heaters
- Electronics board interface temperatures are driven by the grid cold sink boundary temperature since heat transfer from the board interface to the grid is through a radiative heat transfer path and a series conduction heat transfer path.






System Test Planning Thermal Test Overview



Thermal Vacuum test levels

– Qualification

- TDA: -40 °C to +45 °C
- PMT: -30 °C to +40 °C
- Free Board: -30 °C to +40 °C
- HVBS: -30 °C to +40 °C
- Electronic Chassis: -30 °C to +40 °C
- ACD: -25 °C to +40 °C (Per LAT-SS-00778-02 LAT Environmental Specification)

- Acceptance

- TDA: -30 °C to +35 °C
- PMT: -20 °C to +35 °C
- Free Board: -20 °C to +35 °C
- HVBS: -20 °C to +35 °C
- Electronic Chassis: -20 °C to +35 °C
- ACD: -20 °C to +35 °C (Per LAT-SS-00778-02 LAT Environmental Specification)



System Test Planning Thermal Test Overview



- Discussed at PER
 - PMT Assembly Thermal Vacuum Tested
 - Engineering units and Flight units: 2.5 cycles from -30 °C to +40 °C
 - FREE and HVBS Thermal Cycle Tested
 - Engineering models: -30 °C to +60 °C
 - Flight Models: -20 °C to +50 °C
 - Tested under vacuum with Electronic Chassis
 - Electronic Chassis Thermal Vacuum Tested
 - Engineering Model: 12 cycles from -30 °C to +40 °C
 - Flight units: 4 cycles from -20 °C to +35 °C
 - Tile Detector Assembly Thermal Vacuum Tested
 - Engineering model: 5.5 cycles from -60 °C to +45 °C
- PSR Discussion
 - ACD Flight Unit
 - PER: 5 cycles, 4 without MMS/MLI, 1 cycle with MMS/MLI
 - Thermal Vacuum Tested, 4.5 cycles from -30 °C to +40 °C



System Test Planning Thermal Test Overview (PER)



- ACD Flight unit (Thermal Vacuum)
 - ACD Flight TV Test Plan (ACD-Plan-000347)
 - ACD Thermal Vacuum test will be performed in Facility 290 in building 10 in June of 2005
 - Backup is facility 225 located in building 7
 - The ACD will be in it's flight configuration without the Micrometeoroid shield and Multi-Layered insulation for part of the test and will be in it's flight configuration with the MMS but without the MLI for part of the test
 - Test Flow
 - For the first four cycles of the ACD TV test, the ACD without the MMS and MLI, will be cycled to qualification temperatures
 - First cold and first hot cycles will be to survival limits
 - After 4th TV cycle there will be a chamber break to install MMS and MLI on ACD
 - Fifth and final cycle will be to temperature extremes to fully mechanically stress ACD MMS and MLI mechanical support attachments



System Test Planning

ACD PSR Thermal Test Overview (Actual Test Program)

- ACD Flight unit (Thermal Vacuum)
 - ACD Flight TV Test Plan (ACD-Plan-000347)
 - ACD Thermal Vacuum test was performed in Facility 225 in building 7 from July 21st through August 5th of 2005
 - The ACD was in it's flight configuration with the Micrometeoroid shield and Multi-Layered insulation (without the GBK outer layer) for the entire test
 - Test Flow
 - First hot transition to contamination Bakeout
 - Chamber break to fix suspected leak
 - Transition to Hot Bakeout and Hot non-operational (survival) soak
 - Transition to Ambient soak
 - Transition to Cold non-operational (survival) soak
 - 4 total hot and cold operational soaks, one Nominal soak prior to final hot operational soak
 - Ambient soak prior to Repressurization









Summary



- ACD subsystem tested to the specified levels
- No RFA's out of PER to address
- Required 4 cycles hot and cold completed
 - Temperatures monitored via 100+ thermocouples located on the ACD instrument and GSE
 - Less than 10% of test telemetry failed during test
 - No critical thermocouples failed
 - 1 Flight sensor anomaly
 - Non-critical, redundant sensor exists and functioning correctly
 - Read out temperature correctly a few days after failure and for remainder of test
 - Sensor will be examined post test
 - Flight Telemetry data correlated with test telemetry data within 2 °C during soak periods





Contamination Control

Chris Lorentson

ACD Contamination Engineer





- ACD external structure and MMS were cleaned prior to integration (closeout) for environmental testing
- ACD internal structure will be cleaned following thermal vacuum testing
- ACD system will be cleaned and double bagged prior to shipping to SLAC
- ACD system was baked out during the system level thermal vacuum test
- Two TQCMs, a cold finger and a scavenger plate were used to monitor the test in chamber 225 at GSFC
 - TQCM #1 was a 15 MHz TQCM located outside the ACD structure
 - Outgassing certification requirement was 610 Hz/hr
 - Outgassing certification measurement at acceptance was 42Hz/hr



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- TQCM #2 was a 10 MHz TQCM located within the ACD structure
 - Outgassing certification requirement was 270 Hz/hr
 - Outgassing certification measurement at acceptance was not possible due to extremely high deposition rates.
 - The enclosure around this TQCM was more tightly sealed than anticipated. This causes the contaminants to be trapped within the enclosure and falsely raise the TQCM deposition rate

-Requirements development for the test assume free flow of molecular species

- The low deposition rate on the external TQCM indicated that these contaminants were not reaching the external structure
- ACD internal outgassing is vented out the aft of the observatory, not in the direction of contamination sensitive hardware
- External structure outgassing is the primary concern for contamination of sensitive surfaces
- Results of this TQCM were not considered in test acceptance for the above reasons
- Cold finger and scavenger plate analysis will be available upon completion





CPT and Performance Testing Results



Completed Verification Results Summary - Comprehensive Performance Test



- A successful Comprehensive Performance Test of the fully integrated flight system has been performed before and after vibration/acoustics and at four temperatures: +35 C, +23 C, 0 C, and -25 C.
- Document numbers are ACD-PROC-000270 (functional/performance) and ACD-PROC-000352 (margin).
- The test covers all aspects of the ACD functional areas such as
 - Voltages, currents, temperatures
 - Electronics performance (discriminators, PHA, timing)
 - Detector operation and performance
 - Commanding
 - Margin testing (varying electronics voltages and clock frequencies)
- Almost all of our electrical requirements verification at system level is done by this test.



Open Issues from Testing



- In the course of numerous functional tests, some anomalies have been seen for which we have not been able to find good explanations.
- Although none of these appear to affect the basic performance of the ACD, they represent residual risks, primarily in the area of reliability.
- The status of these anomalies, the testing we have done, and the possible impacts are described on the following pages.





- The calibration test script for the ACD High Level Discriminator produces repeatable errors on one of the 12 FREE cards when the test is performed on the whole ACD simultaneously.
- The test always works when only two FREE cards (including the one that produced errors in the full run) are tested.
- We have been unable to trace this problem to any software changes, although it did appear between software updates.
- Troubleshooting included swapping cables. The problem did <u>not</u> move with the ACD cable, but remained with the input port of the LAT interface electronics box (GASU), which is not part of the ACD. We plan to re-check this at the LAT level with the flight GASU.
- Because we have an adequate workaround, and because this test involves only a calibration of a secondary aspect of the ACD, we have not pursued additional troubleshooting.
- Our solution for now is "use as is."





- During each of the cold cycles during the thermal vacuum test, we observed 2-4 excess counts on one electronics channel of the ACD during a test.
- The test was done using charge injection and was a test of a high VETO threshold (5 strobes; should have recorded no counts).
- Either the VETO threshold was not set properly, or the test charge was larger than expected.
- The excess counts appeared on the last GAFE of the last GARC, suggesting a possible end-of-test-cycle clearing error, possibly due to timing, but we have no way to confirm this suspicion.
- It is also possible that we have a channel with an instability, because this same error was seen on this channel in chassis cold tests.
- The operational performance of this channel is excellent at all temperatures.
- If we found excess VETO rate in orbit, we could re-set the threshold. It has very wide dynamic range.





- During two of the four transitions from hot to cold during the thermal vacuum test, we observed high rates (up to 5 KHz) on one tile detector of the ACD. Temperature was between 10 C and –15 C.
- The high rate in both cases settled down to a normal rate (< 100 Hz) by the time temperature stability was achieved.
- The test script that was running collected only rate data, so we have no other information about the output from that tile. We do not even know which of the two phototube signals might have given the high rate, because the hardware counters sum the signals.
- This channel (both phototubes) produces good data in every functional test we have done, including a run at 0 C.
- Because it is a transient problem, not even seen in every transition, we have been unable to diagnose this problem. Generally noise decreases with lower temperature. It was not seen in chassis tests.
- If a high rate on a channel appeared in orbit, we have the option of disabling a phototube signal. Loss of one signal would be acceptable for ACD performance.





TDA Light Yield determination – *results of ACD Performance Test*

Approach is given in ACD-PLAN-000332 "ACD On-Ground Science Performance Calibration and Monitoring"

The idea is based on determining the light yield (L.Y.) for 3 arbitrarily selected TDA's (012, 021, and 022) by carefully measuring their efficiency and deriving L.Y. from obtained efficiency value. From these measurements we determined the ADC sensitivity A_{fl} ,

$$A_{fl} = \frac{1}{6} \times \sum_{i=1}^{6} \frac{P_i}{LY_i \times G_{i,fl}}$$

and after that determined L.Y. for all remaining TDA channels as

$$LY = \frac{P}{A_{fl} \times G_{fl}}$$

where P is the MIP peak position obtained in performed tests, G is the given PMT gain (taken from PMT data sheets)





Sample - Light Yield, determined in this test



Tile	Cable #	Pedestal	Pedestal	Pedestal	Mean	via Landau	using	via	reference,	coeff.	position	previous	PMT Gain	Flight PMT	L.Y. with	L.Y.,
Number	[PMT #]	@ 700	@ 750	@ 800	Pedestal	fit	Landau fit	polynomia	TOP	Applied	for	but	at 1250V	Q.E.	reference	inferred
020	0-020	445.5	445.5	445.5	445.5	1169.39	723.89	1101.68	660.07	0.92	607	607	15.7	22.1	16	26.9
	1-020	214.5	213.5	213.5	213.8	1209.48	995.68	1132.26	916.4	0.92	843	739	20.7	20.3	16.3	24.9
021	0-021	265.5	265.5	265.5	265.5	1036.91	771.41	972.228	707.976	0.82	579	579	18	20	16	22.4
	1-021	512.5	512.5	512.5	512.5	1465.25	952.75	1426.67	910.17	0.82	746	654	19.5	20	16.7	23.4
022	0-022	520.5	520.5	520.5	520.5	1369.83	849.33	1343.74	790.61	0.73	577	577	18.5	18.7	16.3	21.7
	1-022	496.5	496.5	496.5	496.5	1365.8	869.3	1333.81	826.49	0.73	603	529	14.9	18.6	16.5	24.7
023	0-023	204.5	204.5	204.5	204.5	756.982	552.482	705.823	499.8	0.82	410	283	8.1	21.8	17.3	24.3
	1-023	153.5	150.5	150.5	151.5	798.43	646.93	762.939	614.1	0.82	503	406	10	21.4	17	28.3
024	0-024	120.5	120.5	120.5	120.5	668.028	547.528	622.373	499.51	0.92	460	317	9	20.3	17.3	24.6
	1-024	109.5	109.5	109.5	109.5	901.267	791.767	839.302	729.4	0.92	671	541	11.8	19.9	14.5	32
010	0-010	189.5	189.5	189.5	189.5	704.501	515.001	664.391	472.3	0.92	434	434	19	20.1	14	15.9
	1-010	728.5	728.5	728.5	728.5	1333.15	604.65	1313.11	581.83	0.92	535	469	14.4	23.7	13.8	22.7
011	0-011	140.5	141.5	141.5	141.5	709.57	568.07	679.382	533.5	0.82	437	437	15.6	18.8	15.2	20.4
	1-011	219.5	219.5	219.5	219.5	729.833	510.333	692.2	471.8	0.82	386	339	14.5	18.2	14.4	16.3
012	0-012	173.5	174.5	176.5	174.8	1008.07	833.27	926.294	745	0.82	611	647	18.3	22.2	15.8	24.6
	1-012	372.5	372.5	372.5	372.5	1222.07	849.57	1166.74	790.87	0.82	649	497	14.9	21.4	16.4	23.2
013	0-013	196.5	197.5	197.5	197.2	771.264	574.064	732.644	534.9	0.82	439	465	15.2	21.5	17.5	21.3
	1-013	172.5	172.5	171.5	172.2	905.555	733.355	847.513	669.2	0.82	548	420	13.6	21.3	15.8	21.5
014	0-014	501.5	501.5	502.5	501.8	1150.17	648.37	1099.3	597.2	0.92	549	582	16.3	22.2	14.6	24.9
	1-014	396.5	395.5	395.5	395.8	1293.7	897.9	1244.37	846.3	0.92	778	596	17.8	21.1	16.4	23.3
030	0-030	174.5	176.5	176.5	175.8	894.538	718.738	866.488	687	0.92	632	415	15	18.7	14.4	19.2
	1-030	134.5	134.5	134.5	134.5	841.562	707.062	801.26	664.67	0.92	612	469	14.6	21.6	14.1	22.3
031	0-031	599.5	599.5	599.5	599.5	1290.09	690.59	1221.78	615.84	0.82	505	331	11.3	21.6	14.1	20.3
	1-031	162.5	162.5	162.5	162.5	699.638	537.138	651.966	489.2	0.82	401	307	14.9	20.1	14.9	14.4
032	0-032	195.5	195.5	195.5	195.5	981.309	785.809	916.545	715.3	0.82	586	384	10.5	21.7	16.5	25.5
	1-032	684.5	683.5	683.5	683.8	1555.4	871.6	1494.17	806.8	0.82	662	507	13.3	21.4	16.6	26.6
033	0-033	150.5	150.5	151.5	150.8	715.075	564.275	665.606	513	0.82	421	290	9.4	21.2	18.2	21.5
	1-033	210.5	211.5	211.5	211.2	761.241	550.041	704.267	495.6	0.82	407	328	14.2	18.1	17	16.1





- by design the ribbon performance is lower than that of the tiles.
- ACD would never achieve required performance without proper functioning ribbons
- required L.Y. from the ribbons is 3 p.e. from the ribbon center (average for both ends) and 6 p.e. at the crown tile level
- Approach to the measurement was similar to that used for the TDA's. Triggering hodoscope was installed such a way to cover the ribbon and both adjacent TDA's



Each of 8 ribbons was tested in 2 points to confirm light attenuation along the ribbon



Ribbons Light Yield



Ribbon	PMT	End (level of crown tiles)	Center	End (level of crown	Attenuation coefficient
				tiles)	
500	0	11.1		2.0	0.18
	1	2.7		12.0	0.23
501	0	10.7		1.7	0.16
	1	2.2		11.4	0.19
502	0	1.3 ?		8.5	0.15
	1	11.9		1.1	0.09
503	0	2.3		10.0	0.23
	1	11.4		1.8	0.16
600	0	10.1	2.8		0.28
	1	1.6	4.1		0.39
601	0	1.6	4.1		0.39
	1	8.5	2.4		0.29
602	0	8.9	2.7		0.30
	1	1.7	3.8		0.45
603	0	1.5	3.8		0.39
	1	12.9	3.3		0.26

Ribbons Performance test data demonstrates that all they meet L.Y. requirements. Obtained data put in ACD Performance Simulation model





All gaps and clearances between TDA's and ribbons were carefully measured on the flight unit

- The gap requirements at room temperature were as follows:
 - tile butt joints 2 mm
 - tile vertical gaps 3 mm
 - tile to ribbon gaps 2 mm except bending and corner areas
 - corner gaps 4 mm
- All gaps measured at room temperature were corrected to -20C, lowest operating temperature expected.
- Measured gap values (increased for the lower temperature) were put in ACD Performance Simulation model.
- Measured gaps are found to be better than required (on average)



Simulation Model









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Full ACD Efficiency



Simulations were performed for the following cases:

all determined L.Y. values;
ribbon L.Y. 4 p.e. from the
ribbon center – line 1

 1 FREE board failed; 17 tiles operate with only 1
PMT (including 8 tiles on the top) – line 3

 L.Y. from every detector is reduced by 15%; L.Y. from the ribbon center is 3 p.e. – line 2



ACD does meet particle detection efficiency requirement with margins (ACD-RPT-000372)



ACD Science Requirements Verification - Backsplash



- A set of tiles and calorimeter emulators was taken to CERN in 2002.
- Measurements were made of the energy, angle, and material dependence of the backsplash.
- These measurements were compared to a simulation of the same geometry.
- The same simulation was used for the ACD geometry
- The calculated backsplash at 300 GeV is 7%, well below the 20% requirement.
- Even at a threshold of 0.12 MIP, ACD would meet its requirement.







Efficiency

 ACD meets its efficiency requirement with margin, including loss of light or even loss of up to 17 phototubes (or one FREE card).

Backsplash

 The ACD is substantially less susceptible to backsplash than required. The operating threshold could be lowered if needed to gain additional efficiency.





VERIFICATION



ACD Science Requirements Verification Summary- 1



• Some important requirements flow through a science simulation, because direct measurement is impractical (no calibrated source of cosmic rays).

ACD Simulation Measured Input Parameters





ACD Science Requirements Verification Summary- 2



• Some important requirements flow through a science simulation, because direct measurement is impractical (no calibrated source of cosmic rays).

ACD Simulation Measured Input Parameters





Completed Verification Results Summary-Important System performance results 8 August 2005



Important system performance analysis

- Efficiency requirement 0.9997
 - Verified Simulation using as-measured inputs shown above. While the _ inputs have been verified the overall efficiency cannot be fully measured on the ground. The simulation has been reviewed and is in CM. The repeated performance tests confirm input to the simulation.

False veto rate – requirement <20% backsplash, <1% noise

 Verified – backsplash <10% was measured in runs at CERN, using ACD- type detectors and LAT-like calorimeter, plus simulation of detailed ACD geometry. Noise was measured during CPT.

Fast veto signal – requirement – discriminator pulses, variable width

- Verified CPT verified logic pulses, bench tests verified widths
- PHA signal requirement Minimum Ionizing Pulses (MIP), CNO pulses
 - Verified CPT verified PHA for MIP; Test Charge Injection verified CNO



Completed Verification Results Summary-Test-to-Test Variation



Temperature Dependence

 As expected from component and chassis tests, some electronics parameters such as pedestal and some performance parameters such as light throughput have a temperature dependence (more light at lower temperatures, which is where the ACD will operate). These variations have been tabulated for use in on-orbit adjustment of ACD parameters.

• Other Observed Changes

The light throughput on a few of the 194 channels shows some test-to-test variation, up to about 10%, with both positive and negative changes, but no trend. Part of this is likely to be fitting of data with limited statistics, but part may be to vibration and CTE causing small position shifts of the light-transmitting fiber runs and at the faces of the phototubes. Changes at this level have no measurable impact on the overall ACD performance.



Completed Verification Results Summary-Verification Status



- Requirement verification tests complete
- 135 Level 4 requirements and 95 ICD areas
- Any LAT Environmental Specification and LAT Verification Plan requirements are captured and referred to by level 4 and ICD requirements
- Performance characterization, pre and post environmental functional and performance tests now complete.
- Verification sections of delivery data package being prepared as well as test result data packages.
- The ACD system also lent itself to a great deal of subsystem verification. Most requirements also verified prior to final tests.
- Since CDR the full set of ACD requirements has been repeatedly reviewed internally (science team, leads, systems, etc..) for testing weaknesses and any other issues.




MECHANICAL SUMMARY

- Most of the mechanical requirements are verified at the subsystem level via subsystem engineering and flight unit vibration, thermal and strength tests. (see environmental test flow for subsystem flight and engineering units)
- Mechanical requirements not yet verified at PER;
 - Final mass properties, Mass and Center of Gravity Mass OK, C.G. see mechanical testing section
 - Fully assembled ACD system level Sine Vibration, Acoustic and thermal vacuum tests tested successfully
 - Final stay clear survey Minor (0.5mm) inside violation, PFR ACD-021 written and forwarded to LAT. Informal approval by LAT Mechanical Systems Engineer (M. Nordby) through email. Formal change request (LAT-XR- 07058-01) out for approval. All external hard points, including thermal blanket attachment points have been measured and fall well within stay clear. "Soft point" (ie. Thermal blanket) stay clear being measured today, August 8.
 - MGSE MMS lift sling verification test completed
 - Thermal Performance of MLI blanket low risk and sensitivity. There is a waiver (LAT-XR-06769-01 CR) for thermal balance test that would have been of low value but high cost.
 - All mechanical requirements now verified except C.G., external stay clear measurement and MMS/MLI final density measurements. (procedures and WOAs used for actual verification recorded in table)
 - See requirements section for small list of waivers and Margins section for verified margins





ELECTRICAL SUMMARY

- Full subsystem verification successfully completed.
 - The electronic chassis operate completely independently and have been fully tested and exercised in their flight assembled configuration, as has each Tile Detector Assembly.
 - They function the same on the assembled ACD; in fact the functional test is basically the same. There is no interdependency between channels.
- Full ACD Pre and post-environmental functional and performance tests completed.
 - The system level tests allow for optimization of settings, determining the ability to meet the efficiency requirement and exercising the GASU side of the interface for multiple chassis. Almost all requirements and performance verified by CPT (ACD-PROC-000270) and associated margin test. Refer back to CPT testing section for EGSE software scripts issues.





ELECTRICAL SUMMARY

Electrical requirements not yet verified at PER;

- Overall Efficiency Our most important requirement, refer to earlier slides.
 Functional and performance tests results have been analyzed and inserted into science simulation runs
 - Light through-put performance of channels between the scintillating detectors and PMTs in their as-assembled condition. This is one of many inputs into the above efficiency requirement.
 - Meets requirements. <u>Estimated efficiency is greater than</u> <u>0.9997</u>

-See CPT and efficiency slides

 <u>All electrical requirements now verified</u> (procedures and WOAs used for actual verification recorded in table)

-See system level EMI testing waiver (earlier) and non conformance slide (to come)





ELECTRICAL SUMMARY

• Electrical requirements that were not yet verified at PER;

- ICD interfaces have been verified at the chassis level, and the full ACD has been run with the EGSE GASU#8. All tests successful
- Some minor anomalies associated with electrical testing are long running issues with the EGSE system remain – see CPT and PR sections





• Important verification subtables

•<u>Table of requirements to</u> <u>be re-verified at system</u> <u>level.</u>

• These are all verified at chassis level, and there is no difference in function after assembled and in the basic functional test itself. Hard copy of complete table available

•ACD verifies at level 4 requirement level. Any level 3 requirements that did not decompose to level 4 where carried down as is to facilitate complete verification at one level. <u>All level 4 requirements</u> <u>have been successfully</u> <u>verified.</u>

Regt ID	LAT ACD Level IV Requirement	Verificatio n Method	ACD System Verification Procedure	Planned Test
ACD4-25	5.1 Charged Particle Detection			
ACD4-26	The ACD shall produce both fast and logic (hitmap) VETO signals in response to PMT signals resulting from charged particles traversing the ACD tiles and ribbons.	Test	ACD Comprehensive Performance Test (CPT) (ACD-PROC-000270)	Efficiency test & T/V
ACD4-27	5.2 Adjustable Threshold on VETO Detection of Charged Particles			
ACD4-28	The threshold for detecting charged particles shall be adjustable from 0.064 to 1.28 pC (0.1 to 2 MIP), with a step size of <0.032 pC (0.05 MIP).	Test	ACD Comprehensive Performance Test (CPT) (ACD-PROC-000270 Chassis Full Functional Test	Efficiency test & T/\
ACD4-29	5.3 False VETO due to Electrical Noise			
ACD4-30	The total ACD false VETO trigger rate due to noise shall be less than 10 kHz (~46Hz per channel) at 0.096 pC (0.15 MIP) threshold (assuming 1 us VETO pulses).	Analysis Test Simulation	ACD Comprehensive Performance Test (CPT) (ACD-PROC-000270)	Efficiency test & T/\
ACD4-31	5.4 High Threshold Detection			
ACD4-32	ionizing particles (carbon nitrogen oxygen or heavier nuclei), which produce signals from 31.2 - 200 MIP (20 pC to 128 pC) with a goal of 1000 MIP (640 pC). The ACD is required to detect, via the High Level Discriminator (HLD), all signals above the High-Level threshold (nominally 25 MIP's); it is required to digitize (PHA) signals up to 200 MIP's (128 pC). The current design actually allows for digitization of signals up to 1000 MIP's (640 pC). Each ACD electronics board shall OR up to 18 HLD outputs (selected via command) to generate a single HLD_OR signal for transmission to the AEM.	Simulation	Performance Test (CPT) (ACD-PROC-000270) up to ~200 MIP	test & TA
ACD4-34	5.5 Adjustable High-Threshold			
ACD4-35	The High Level Threshold shall be adjustable for PMT signals from 12.8 to 40.96 pC (20 to 64 MIP) in steps of 0.64 pC (1 MIP) _20%. HOWEVER As of Oct 2003 the GAFE 56 and GAFE 7, one of which should be our flight chip, do not quite meet this requirement as stated. On those chips The High Level Discriminator is adjustable from 0 - 130 MIP in steps less than 1.6 MIP/step. This adjustability still allows us to meet all of our related requirements. So this is likely to be our flight performance. See related NCR	lest	ACU Comprehensive Performance Test (CPT) (ACD-PROC-000270)	Efficiency test & T/\
ACD4-37	The ACD electronics shall accent from the GEM a	Test	ACD Comprehensive	





Important verification sub-tables

•Table of requirements only verified at the subsystem level.

• These are not directly verifiable at system level, only indirectly. Hard copy of complete table available. <u>All have been successfully verified</u>.

The following table is a list of requirements that must be verified at a lower level of assembly than Electronic Chassis.

No	DOORS ID	LAT-SS-00352 ID	Verified	ACD WOA	Rationale
1	ACD4-39,40	5.7.1 Fast VETO Signal Latency	FREE Comprehensive Performance Test, ACD-PROC-000051, Section 11.4	ACD-WOA-00021 through ACD-WOA- 00036	This test requires an oscilloscope on the GAFE output to make a direct measurement.
2	ACD4-41,42	5.7.2 Fast VETO Signal Width	FREE Comprehensive Performance Test, ACD-PROC-000051, Section 11.5	ACD-WOA-00021 through ACD-WOA- 00036	This test requires an oscilloscope on the GAFE output to make a direct measurement.
3	ACD4-43,44	5.7.3 Fast VETO Retriggering	GARC Comprehensive Performance Test, ACD-PROC-000051, Section 11.4, Discriminator Input Minimum Width Test	ACD-WOA-00021 through ACD-WOA- 00036	This test requires an oscilloscope on the GAFE output to make a direct measurement.
4	ACD4-66,67	5.8.4 Pulse Height Measurement Latency	GLAST LAT ACD Interface Digital Timing Measurements, ACD-RPT- 000274	Not applicable to this report.	This test requires an oscilloscope on the GAFE output to make a direct measurement.
5	ACD4-70,71	5.8.6 Differential Non-Linearity	FREE Comprehensive Performance Test, ACD-PROC-000051, Section 11.20	ACD-WOA-00021 through ACD-WOA- 00036	This test requires the use of an external pulse generator.
6	ACD4-85,86	5.9.3 HVBS Limiting Output Current	HVBS Functional Test, ACD-PROC- 000064, Sect. 4.5, Tables 3, 4, 5	ACD-WOA-00321 through ACD-WOA- 00353	This test requires application of a non- flight load in the lab for verification.
7	ACD4-87,88	5.9.4 HVBS Output Voltage Adjustment	HVBS Functional Test, ACD-PROC- 000064, Sect. 4.5, Tables 3, 4, 5	ACD-WOA-00321 through ACD-WOA- 00353	Verification for this section requires both an oscilloscope and the application of a non- flight load.

Completed Verification Results Summary

- Non conformances, hard to verify tests August 2005

Summary of Non-conformances

ACD PSR

- Minor stay clear violations mentioned earlier (ACD4-215) Change Request (LAT-XR- 07058-01) is in the approval process.
- ACD4-92, 90, 100 HVBS line and load regulation % target, temperature stability, output ripple, not a major issue, could contribute to temperature performance changes. Tracking down more detailed test results to confirm – Non-conformance will be written if needed.
- For a few requirements, we have not yet confirmed the correct system level verification test.
 - Some ICD items in section 9 (command and data handling) were not included in the 'only verifiable at the subsystem level' category, but may fall into that category because they are only indirectly tested at the system level. Reviewing tests to update verification table.

Completed Verification Results Summary

borderline areas

ACD PSR



- Summary of requirements where conformance is border line
 - ACD4-220 Distance from lower tile to ACD interface plane distance tolerance not met. The important distance is covered in level 4 requirement and can only be verified at LAT. The requirement as written should not have had a negative tolerance. We beat the science intent of the requirement which is coverage relative to tracker and calorimeter – lower is better!
 - ACD4-73 Temperature performance stability. On average we meet the requirement but some channels don't. Requirement written for average and overall there is no science concern as long as behavior is known.
 - ACD4-224 The ACD shall cause interaction of less than 6% of the incident gamma radiation within the LAT field of view.
 - This is a difficult requirement to verify by analysis. A variety of analyses have been completed with results varying from 5.8 to 6.4%. This requirement was more of a design guideline and the overall science impact due to small variabilities in this number is minimal (note the significant digits of the requirement). The LAT science team has been informed of this potential non-conformance.
 - ACD4-226 The thermal blanket/micrometeoroid shield shall have a mass per unit area of ~<0.32 g/cm² which should minimize secondary gamma-ray production by undetected cosmic ray interactions.
 - This requirement is difficult to determine with high accuracy, however it is estimated that the "as-built" thermal blanket/micrometeoroid shield has an overall average density of ~3.6 g/cm² (12.5% higher than goal of ~<0.32 g/cm²). This variance is due to the additional layers of Kevlar added to the MMS, which was required by an update to ORDEM2000 (Orbital Debris Environment Model), so that the more important requirement of having a Probability No Penetration (PNP) >.95. A change request will be submitted to the LAT Instrument Project Office.





- All of our subsystem testing verification is complete and all major anomalies addressed.
- System level verification is complete.
- Final analysis and optimization of system settings and final channel performance inputs complete.
- Post environmental functional tests and performance tests completed. Tests also successful with few problems or non conformances.





RESOURCE MARGINS



ACD Technical Budget Summary



ACD PSR

Technical Resources –

<u>ACD Mass</u>

- Allocation 295 kg
- ACD measured mass
 282 kg
- ACD mass margin 14 kg

<u>ACD Power</u>

- Can not accurately measure the full power of ACD in its assembled state due to limitations in the EGSE. Power measurements performed on each flight electronics chassis and the High Voltage Bias Supplies provides a nominal power of:
 - Measured 11.9 W
 - Allocation 12.5 W
 - Margin 0.6 W
- ACD meets power specifications and requirements when operated nominally at specified limits. By using relative power measurements taken during thermal vacuum testing, it is estimated that the ACD will use 0.1 W less power at hot operating temperature and 0.4 W more power at cold operating temperature.



ACD PSR

ACD Technical Budget Summary



Technical Resources –

<u>Thermal Interface</u> (max dissipation across ACD-LAT interface)

- Dissipation Allocation
 16 W
- Dissipation Analysis <14 W
 - Not directly measurable with requested de-scope of thermal balance, however analysis is very complete and simple with no significant uncertainties
 - LAT is not sensitive to small errors in this number

FREQUENCY MARGIN

 All analysis and tests of all subsystems exceed 50 Hz min requirement. Lowest frequency result from tests is ~70 Hz for TSA and ~100 Hz for the electronic chassis.







Mission Assurance

James Lohr GLAST SAM





ACD-2336- 003 07/27/2005 18:10	A cracked –9 EO #4 post (1) was used in the left middle position marked "E" as per MMS Installation Assembly, GE2054591on the +X Side of the MMS. This was instead of a -7EO#4 post.	 The fabrication shortage and test schedule drove decision to substitute existing posts for the redesigned posts, some of which arrived with cracks and were rejected. However, the best of the cracked –9 EO #4 posts (1) was used in the left middle position marked "E" as per MMS Installation Assembly, GE2054591on the +X Side of the MMS. This decision was strictly for test and the post is planned for replacement with a flight tested post after Environmental testing is complete. Environmental qualification tests on replacement posts completed.
ACD- 02334-016 08/05/2005 08:14	During two of the four transitions from hot to cold during the ACD thermal vacuum test, we observed high count rates in the ACDMonitor script. In each case, these rates exceeded 1000 Hz. The temperature range was approximately - 10 C to -15 C. Because hardware counters were used, we only know that it was one of the data channels from phototubes attached to tile 320 - i.e. GARC 6, GAFE 16 or GARC 7, GAFE 17. By the time the temperature had stabilized at -25 C, the rates had returned to their normal values of less than 100 Hz. No problems have been seen with either phototube signal in any functional test at any temperature.	 The test script that was running collected only rate data, so we have no other information about the output of that channel. We do not even know which of the two phototube signals might have given the high rate, because the hardware counters sum the signals. This channel (both phototubes) produces good data in every functional test we have done. Because it is a transient problem, not even seen in every transition, we have been unable to diagnose this problem. Generally noise decreases with lower temperature. If a high rate on a channel appeared in orbit, we have the option of disabling a phototube signal. Loss of one signal would be acceptable for ACD performance.





ACD- 02334-009 07/26/2005 15:45	D- 34-009 26/2005 45 AcdVetoHitmapPha failed: Garc 11 Gafe 17: High TCI level channel received unexpected HW Count of 2 (expected 0)	 During each of the cold cycles during the thermal vacuum test, we observed 2-4 excess counts on one electronics channel of the ACD during a test. The test was done using charge injection and was a test of a high VETO threshold (should have recorded no counts).
		 Either the VETO threshold was not set properly, or the test charge was larger than expected.
		• The excess counts appeared on the last GAFE of the last GARC, suggesting a possible end-of-test-cycle clearing error, possibly due to timing, but we have no way to confirm this suspicion.
		 If we found excess VETO rate in orbit, we could re-set the threshold. It has very wide dynamic range.





ACD-ACD-INT-02324- 001 07/22/2005 14:54	During a visual inspection of the ACD after the completion of the Acoustic test, it was noticed that a nutplate with adhesive, like the the parts used to capture the screws that mount the TDAs to the ACD structure, was found on the floor of the test cell under the ACD Dolly. The location where the nutplate was found was under the +X, -Y corner.	 The Nut plate is believed to have been on ACD dolly before testing started. The nut plate in question had debonded from the angled shim it was mounted to during TDA installation and was inadvertently left behind. During acoustic tests it shook free. Nut plates have a locking feature that requires 0.5 in-lbs to overcome the locking feature. The locking feature is not likely to be overcome through vibration or acoustic loadings. Nut plate is captured within a flexure by tape that surrounds each flexure to provide light tight seal. Light tight seal is validated through light tight testing. The ACD had closeouts between the ACD and the 2" plate and covering the hole in the 2 inch plate. Post Acoustic Test Inspection revealed nutplate installation tool found in the +x, -y corner of the ACD dolly. If this came off the flight assembly, analyses show that a tile mounted with 3 fasteners shows positive margin of safety.
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ACD- 02334- 004 07/21/200 5 17:55	While running the Thermal Monitoring system, the readout for Yp_Inshell_S was reading around 23 degrees at startup and started flunctuating between 5 degrees to a negative 50.	 Will perform visual inspection after removal from chamber to assess condition. No impact if it does not work.
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ACD-ACD-INT-02322- 001 07/20/2005 14:16	 HldCal output for GARC5 is faulty when this test in run for all GARCs simultaneously. Extra triggers are being seen on all GAFE channels on GARC5, and the script resets the counter during the run. The calibration function, which should be a straight line, shows a peak. Troubleshooting on this problem: 1. This problem was not seen during the full functional test on 6/13/05. 2. This problem has been seen on all full functional tests since 6/17/05. 3. Running with only GARC2 and GARC5 enabled produces good results (consistent with the 6/13 run. 4. Running with only GARC4/GARC5 or GARCs 2, 3, 4, 5, 6, 7 also produces good results. 5. Running with all GARCs except GARC5 enabled produces similar nonlinear performance in GARCs 1,2,3,4, but not GARC 0 or GARCs 6-11. 6. If the cables for GARC5 and GARC2 are swapped, the nonlinear behavior still appears in the data labeled GARC5 (which came from GARC2 in this case). 7. Changing back to the HldCal software used on 6/13 does not solve the problem. 8. Changing back to the gGEM software used on 6/13 does not solve the problem. 8. Changing back to the gGEM software used on 6/13 does not solve the problem. 8. Changing back to the gGEM software used on 6/13 does not solve the problem. 8. Changing back to the gGEM software used on 6/13 does not solve the problem. This PR now consolidates the following PRs, all of which describe the identical problem: ACD-02334-001, ACD-02322-005, ACD-02322-001. These other PRs will be edited to reference this one, so that they can be closed. This PR should be left open for now, so that it can be carried to the next level of assembly. 	•	 The problem does not appear to be in the ACD hardware, since it shows up on the same data channels when cables are swapped. This is a problem of calibration or operating conditions, not a problem of performance, as best we can tell. We have found no adequate explanation of how the data are being garbled, but software seems to be a likely candidate. We have an adequate workaround to obtain this calibration, by a run using just two GARCs. The whole topic of calibrating the High Level Discriminator is a secondary issue for the ACD, since the only goal of the HLD is to send trigger signals for possible high-Z cosmic rays. We are proceeding with this as an open issue.
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OPEN PFR (Green)



ACD-021 07/05/200 5 19:49	Measurements show that one thermistor wire installed onto the interior surface of the TSA violates the ACD stay-clear volume.	 Stay clear violation is very minimal and does not cause an interference between the LAT and ACD. Waiver LAT-XR- 07058-01 submitted to LAT. It is in the approval process. Preliminary approval received via email.
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Risk Management

Tom Johnson Instrument Manager, Code 556







- If failures occur the ACD is designed to fail 'gracefully'. Major failures result in incremental steps in performance. Other than a major micrometeoroid hit, it takes multiple failures to fail a detector channel. Complete detector channel failures leave holes in coverage.
- Micrometeoroid shield penetration is the only in orbit single point failure risk. ACD fails to meet the efficiency requirement with one tile destroyed by micrometeoroid penetration. The only other way to lose a entire detector channel is for multiple failures of other components.
- A GARC failure results in loss of up to 17 PMTs leaving 17 detector tiles operating on one PMT. The ACD meets the efficiency requirement in this scenerio.
- Each Tile Detector Assembly and Ribbon Detector has fibers leading to two separate PMTs on separate electronic chassis. PMTs are powered by separate HVBSs.
- Each electronic chassis has redundant HVBSs.
- High Voltage for the PMTs can be adjusted in orbit to counteract PMT gain degradation over time.





Risk



- As part of the reliability/risk mitigation program, the following activities have been performed:
 - Failure Modes and Effect Analysis and Critical Items List ACD-RPT-000042 (LAT-TD-00913)
 - Limited-Life Item Analysis (LAT-TD-00523)
 - *Reliability Assessments and Worse Case Analysis (ACD-RPT-000071)*
 - Fault Tree (ACD-RPT-000072)
 - Parts Stress and De-rating Analysis
 - Continuous Risk Management Plan (LAT-MD-000067)





ACD RISK ASSESSMENT





Rank	Approach	Risk Title
1	M,R	Damage and/or light leak to Tile Detector Assembly
2	M,R	Electronics component failure (incl PMT subassembly)
3	М	EEE Part Failure
4	М	EGSE failure or malfunction
5	R,M	Facility problem.
6	M	Corona around high voltage during vacuum testing
7	M	Secondary structural failure during environmental testing
8	M	Damage to ACD during handling or test set up operations (including ESD)
9	M,A	ACD EMI/EMC Test Descope
10	R,A	ACD Thermal Balance test descope

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ACD RISK ASSESSMENT – AT PSR





Number /Trend	Approac h	Risk Title
1 ↓	M,R	Damage and/or light leak to Tile Detector Assembly
² ↓	M,R	Electronics component failure (incl PMT subassembly)
3	М	EEE Part Failure
4	М	EGSE failure or malfunction/LAT interface issue.
5	R,M	Facility problem. (RETIRED)
6 ↓	М	Corona around high voltage during vacuum testing
7 ↓	М	Secondary structural failure during environmental testing
⁸ ↓	М	Damage to ACD during handling or test set up operations (including ESD)
9 ↓	M,A	ACD EMI/EMC Test Descope (RETIRED)
10 📕	R,A	ACD Thermal Balance test descope (RETIRED)





Project Review Activities

Tom Johnson Instrument Manager, Code 556



Monthly Reviews



- AETD Champion Team Review Representatives from all applicable divisions within AETD review our status on the first Monday of every month. They also serve as our "champion" within their respective division and help us to resolve issues.
- Goddard Monthly Status Review (MSR) Issues, risks, schedule, milestones, cost, reserves, and accomplishments presented to the Goddard Program Management Council monthly.
- GLAST/LAT Monthly Cost and Schedule Review Technical issues, accomplishments, and cost and schedule variances and corrective actions presented to the LAT and GLAST Project Offices monthly





ACD PSR

- Past Reviews: All Action Items closed
 - LAT Internal Review of the ACD January, 1999
 - Pre-PDR/Baseline Review February, 2001
 - LAT System Requirement Review (SRR)- May 2001
 - ACD Peer Review July, 2001
 - 62 RFA's All closed out
 - LAT PDR/Baseline Review January, 2002
 - 12 RFA's All closed out
 - LAT Internal Stanford Linear Accelerator Center Review April, 2002
 - LAT Delta PDR/Baseline Review July, 2002
 - 3 RFA's All closed out
 - ACD Critical Design Review January 7 & 8, 2003
 - 19 RFA's All closed out
 - LAT Critical Design Review (CDR) May 12 16 2003
 - 2 RFA's All closed out (both ASIC related)
 - DOE/NASA Independent Review March, 2004
 - PMT Mounting Design Peer Review August 30, 2004
 - 18 RFA's All closed out, zero PMT glass enclosures have failed using new mounting design
 - ISO Audit November, 2004
 - 2 Observations, no findings or RFA's



Request for Action - PER



ACD	PSR	8 Aug	just 2005
RFA	Action/Question	Response	Status
1	a) Successful completion of ACD full functional/performance testing.	The ACD full functional is currently 90% complete. It will be completed when one test is re-run with an updated test script. ACD vibration testing will begin following the successful completion of the final test. Vibration testing is scheduled to begin on Tuesday, July 12.	CLOSED
	 b) Complete review of TV test configuration given that new plan (back to baseline) require disintegration of MMS prior to TV (reflected on chart 88) with ACD Champion team. 	Due to facility and hardware availability constraints, the ACD had planned to deviate from the original baseline and perform thermal vacuum testing prior to vibration testing. The four cycle thermal vacuum test was to be performed without the Micrometeoroid Shield (MMS)/Thermal Blanket (TB) and then the MMS/TB would be installed and one thermal cycle would be performed to verify the structural integrity of the MMS/TB mechanical attachment points. Hours prior to the ACD PER, it was realized that the ACD would not have to deviate from the original baseline. Therefore, the ACD will perform all testing with the MMS/TB installed. Vibration testing will be performed first followed by thermal vacuum testing. No de-integration of the MMS/TB will be performed during the environmental testing flow. One slight deviation is that the Germanium Kapton outer layer will not be installed during ACD mechanical and thermal leads and is an acceptable and/or preferable deviation due to the fragile nature of the material. It will be installed prior to LAT level thermal vacuum testing.	CLOSED
	c) Ensure hat a reliable EGSE SW/LATTE SW baseline version is frozen to ensure consistent performance testing evaluation throughout the environmental test program.	Will do. Several updates have been made to LATTE since the ACD PER. These updates were required to successfully run the ACD functional and performance tests.	CLOSED



Request for Action - PER



RFA #	Action/Question	Response	Status
2	Get a fiber optics expert's opinion on the integrity of the fiber optic bundle that had the broken fiber on it (Detector Assembly 230). Could there be any residual stress that could predispose other fibers in the bundle to fail?	Status and visual inspection result. It was found that in TDA 230 (long tile on –Y side) one green fiber (wave-length shifting fiber) is broken just at the entry point into the fiber bushing. The first impression after careful visual inspection is that due to some reason this single fiber was not bonded to all other fibers (20 in total) to create a strong bundle in the entering point into the bushing to the black tubing, and during tubing taping to the bushing some rotation of the tubing caused the fiber to break. All other fibers (20 in total) are bonded together at the length of approximately 0.5" from the bushing and create a solid bundle. Careful visual inspection did not show any visible damage to any of other fibers. Normally damaged fibers are easily seen by presence of bright rings, which were not found in this fiber bundle. Also the inspection of both fiber bundles of this TDA was performed according to "Clear Fiber Cable Post-Installation Test Procedure" ACD-PROC-000294 and did not reveal any damages to the fibers. Mitigation: Special tests were performed (at the time of ACD design) to measure the TDA performance dependence on the number of broken fibers, and it was found that up to 4 broken fibers are allowed in the TDA to still meet the performance requirement. This test was for the TDA's which are required to have 0.9997 efficiency, but the long tile has an efficiency requirement of only 0.999. So, a single broken fiber has no effect on the operation of this TDA was already said above, visual inspection (reference, chassis qualification chassis vibration testing). This can result in a 470psi stress on the fiber subside and with the stress on a single fiber, however, under vibration environments the fiber bundle can experience a 60 ga cceleration (reference, chassis qualification chassis vibration testing). This can result in a 470psi stress on the fiber bundle and this stress is low compared to bulk scintillator material. Therefore, fibers are not likely to fail during environmental testing. Finall	OPEN – Waiting on approval from orininator. The performance of the TDA's has remained constant throughout environmental testing of the ACD, which indicates that the plastic fibers did not break during testing.





#	Recommendation	Response	Status
	During ACD TV Testing, run the GASU baseplate temperature at a level that will give equivalent ambient boundary point temperatures. GASU #8 has not been tested in vacuum at temperature and may experience some temperature sensitivity during TV testing that may affect ACD testing. This problem was experienced during Tracker TV testing using a TEM box had not been tested in vacuum @temperatur	It has always been the plan to maintain the GASU at ambient temperature during thermal vacuum testing. A thermal control plate has already been provided for the GASU and it will be blanketed for the test. Both the thermal control plate and GASU will be instrumented with thermocouples and will be controlled using a Temperature Conditioning Unit (TCU) provided by the Environmental Testing Group (Code 549). Additionally, since GASU #8 has not been tested in vacuum, a thorough review has been performed by the ACD and LAT teams and it was concluded that it was a very low risk to perform testing on the ACD using a GASU that has not been tested under vacuum conditions. A report documenting this issue has been written and submitted in the ACD configuration management library (ACD-RPT-000359). Code 560 has reviewed this issue as well and came to the conclusion that the risk of failure was very low and therefore vacuum testing on GASU #8 is not required (email confirmation from C. Coltharp on June 21, 2005).	CLOSED – GASU was held at ambient temperature during TVAC testing.





# Recommendation		Response	Status
2 While the PMT h supplies have bee people command spacecraft will be consider impleme software lockout turning high volta down, launch, or outgassing. Coro voltage breakdow pump down, laun completing outga breakdown might transients that cou or spacecraft bus hardware or softw voltage might pre command that mi spacecraft if it we time.	igh voltage power n well designed and ing the instrument or careful, please enting a hardware or that would prevent age on during pump prior to completing na or Passion high or might occur during ch, or prior to ssing. Such a produce EMI or ald damage instrument electronics. A vare lockout of high vent an accidental ght damage the ere sent at a critical	The ACD currently implements a hardware lockout that requires three commands to apply a voltage to the PMTs. This works in the following way: Any time the GARC ASIC is reset (for example, at power-up or by command), the high voltage enable bits are reset to the inactive state, the bias level DAC is commanded to a zero level, and the high voltage level registers are cleared. To apply voltage to the PMTs, three commands are needed: (a) enable the high voltage supply (this is an active high bit) (b) supply a value for the high voltage level to be used (c) direct the GARC to send this level to the DAC. The enable commands each consist of three bits with a best two-of-three voting logic for the bit status. This triple modular redundancy provides additional protection against single event upsets. Additionally, there is an additional failure mode that has been covered related to power supply sequencing. The GARC ASIC requires +3.3V power to actively control the state of the high voltage bias supplies. In the absence of +3.3V power while +28V is applied to the ACD (a non-standard mode), there is a pull- down resistor on the FREE board to passively inhibit the operation of the supplies. While it is true that proper care should be exercised by both test conductors and software	OPEN – Waiting on response from originator





#	Recommendation	Response
3	For historical reason, the PMT high voltage power supplies are capable of being commanded to an output of 1150 Vdc even though it has been determine that the maximum required output is 950 Vdc. Further, no system level testing is planned above 950 Vdc. Please consider implementing a hardware or software lockout that would prevent accidental commanding of the high voltage to a voltage level above which was tested at the spacecraft/instrument level for both I&T and on-orbit operations. Increased voltage may produce corona or H. V. breakdown that could damage T/M or components. Never allow orbital ops that have not been tested on the ground.	This addresses the issue of the original design of the ACD system having a specification of 1300 V, but having a recent desire to limit the voltage to 1150 V. Since all of the flight electronics had been built, tested, and qualified prior to this change, it remains capable of 1300 V operation. (In fact, the great majority of the phototubes in the flight ACD system have already been tested and characterized at 1300 V). Any maximum level lockout would have to be accomplished in software at this point. This is most simply done using the command sequence detailed in section (2). After writing the high voltage level to be used in step (b), this value is read back from the GARC. If the value read back corresponds to a value greater than 1150V, then step (c) is not initiated. If the software performs this check, a voltage higher than 1150 V could not be commanded without an explicit operator override.





#	Recommendation	Response
3	For historical reason, the PMT high voltage power supplies are capable of being commanded to an output of 1150 Vdc even though it has been determine that the maximum required output is 950 Vdc. Further, no system level testing is planned above 950 Vdc. Please consider implementing a hardware or software lockout that would prevent accidental commanding of the high voltage to a voltage level above which was tested at the spacecraft/instrument level for both I&T and on-orbit operations. Increased voltage may produce corona or H. V. breakdown that could damage T/M or components. Never allow orbital ops that have not been tested on the ground.	This addresses the issue of the original design of the ACD system having a specification of 1300 V, but having a recent desire to limit the voltage to 1150 V. Since all of the flight electronics had been built, tested, and qualified prior to this change, it remains capable of 1300 V operation. (In fact, the great majority of the phototubes in the flight ACD system have already been tested and characterized at 1300 V). Any maximum level lockout would have to be accomplished in software at this point. This is most simply done using the command sequence detailed in section (2). After writing the high voltage level to be used in step (b), this value is read back from the GARC. If the value read back corresponds to a value greater than 1150V, then step (c) is not initiated. If the software performs this check, a voltage higher than 1150 V could not be commanded without an explicit operator override.





#	Recommendation	Response	Status
4	Consider GSFC personnel escort for cross country road trip of ACD to SLAC. There was talk of an active purge system being used. There should be shock and temperature sensors. A knowledgeable technician along for the ride could be beneficial. Commercial truck drivers should be more conservative with an escort.	Providing a cross country escort for the transportation of the ACD from the GSFC to SLAC was not included in the baseline plan due to cost constraints. The baseline plan is to transport the ACD in an environmentally controlled air ride tractor trailer using dual drivers. The ACD will be mounted on a shipping dolly that is vibration isolated and it will be instrumented and monitored for shock and temperature. It will be bagged and purged to provide additional humidity and contamination control. The ACD is not particularly sensitive to temperature or contamination. The temperature limits are +40C on the high side and the low side is constrained primarily by condensation, which is mitigated by the environmental control system with redundant control provided by the purge. Contamination will be controlled by double bagging with the purge providing additional backup capability. As noted in the recommendation, the primary benefit of an escort would be to ensure that the truck operators drive responsibly and conservatively. With all of that said, the ACD Team does agree that there would be some benefit to escorting the ACD from Goddard to SLAC. Therefore, we will submit a request to the LAT project requesting the additional funding (estimated to be \$30K) required to support a cross country escort for the ACD	CLOSED – Transportation plan and contingencies are in place to transport the ACD to SLAC without an escort.



Reviews – Future



- Future Reviews:
 - ACD Pre-Ship Review (PSR) TODAY, August 8, 2005
 - LAT Pre-Environmental Review (PER) January 2006
 - LAT Pre-ship Review (PSR) May 2006




Deliverables **Flight Hardware**



- Anti Coincidence Detector (ACD) GE2054500
- 1/4" bolts (quantity 12)
- 3/8" bolts, (quantity 8)



Deliverables



As defined by ACD-LAT ICD- (LAT-SS-00363-07):

• Lifting Harness, etc:

ACD Lift Brackets: GE2057546 Machining, Lift Sling GLAST GSE

- ACD Lift Sling: GE2068104 Lift sling assembly BEA configuration
- Handling Dolly:

ACD Dolly: GE2057516 BEA Handling Dolly

• Drill Templates:

none

MMS/Thermal Blanket removal tools:

Will not be delivered

• ACD multi purpose test fixture:

2" Plate Assembly: GE2068109 Universal Fixture, Assembly GLAST GSE

• Hydraset if needed:

Not enough hook height

• Helium Monitoring equipment:

(Loan) Inficon model: 12206 Protec



Deliverables



ACD Subsystem to LAT I&T Deliverables MOU (LAT-TD-04542-01):

- 3.1.1 Users Manual: ACD Comprehensive Performance Test Procedure (ACD-PROC-000270) and GLAST ACD G3 EGSE Script Summary (ACD-LIST-000282)
- 3.1.2 Test Scripts: All have been put into CVS repository at SLAC
- 3.1.3 Algorithms: GLAST ACD G3 EGSE Script Summary (ACD-LIST-000282)
- 3.1.4 SVAC Plan: To Be Provided
- 3.1.5 MGSE:
 - Drawings, Inspections, Proof Tests, Certifications: Will be provided on CDs and/or DVDs from ACD CM Library.
- ♦ 3.1.6 EGSE:
 - None







ACD Acceptance Test Data Package Contents Requirements (LAT-TD-04349-01):

• We are working on completing the ATDP by 15 Sep 2005.





ACD TRANPORTATION Preship Review

Aug 2005

ACD Mechanical Team

Kenny Harris / Code 543, ACD Mechanical Engineer





- Instrument Transportation
 - Requirements
 - Documentation
 - Transporter Personnel
 - Roles
 - System Description
 - Analysis Results
 - Certification Tests
 - Contingencies
 - GLAS vs GLAST Comparison



REQUIREMENTS



- Transport the ACD Instrument from GSFC to SLAC
- Maintain temperature of 70±10°F
- Maintain Relative Humidity of < 60%</p>
- Supply Continuous Purge to ACD at 10 CFH
- Record Shock and vibration data during trip.
- Mechanical Load Environment Not to Exceed Tested Values for All Components



Documentation



- ACD Instrument and Ground Support Equipment Packaging, Handling, and Transportation Plan ACD-PLAN -369
- ACD Instrumentation Plan ACD -000-371
- Shipping Configuration Drawing
- WOA for transport to SLAC is pending



Transportation Personnel



AI Strojny Steve West Ryan Simmons William Chambers Kenny Harris AI Lacks Andrew Kolfeldt Bill Hensley Steve Harper Paul Haney Mike Lenz Mike Taylor Walt Carel Steve White Rick Eichen Ken Segal Craig Colthorp

TRAX Mechanical Engineer Instrumentation ACD Lead Analyst Analyst ACD Mechanical Engineer **Quality Assurance** Safety Logistics Technician Technician Technician Logistics Packaging Designer Traffic Manager Mechanical Lead ACD I&T Manager



Roles



- GSFC is responsible for shipment to SLAC
- SLAC will be responsible for providing operator assistance for cranes and forklifts in removing ACD from truck
- GSFC will perform functional test at SLAC before buyoff
- GSFC is responsible for packaging and shipping return items back to GSFC from SLAC
- Code 230 will be stay in contact with the truck drivers and update the project with a status every 12 hours and 4 hours before arrival to SLAC







TRANSPORTATION DESIGN LOADS



These Design Loads Were Used to Analyze All Structural Components in the Transportation Assembly.

Air Ride Transportation loading:

Longitudinal (g's)	Lateral (g's)	Vertical (g's)
+1.5 G's Forward (along direction of travel)	<u>+</u> 0.5 G's Lateral	+2.5/-1.5 G's Vertical (positive towards the ground)



Structural Analysis Results



Component	Material	Loading	Stress (psi)	F.S.y	Page
2" vib plate attch ¹ / ₂ "-13	Unbrako	combined	42758	3.9	7
¹ / ₂ " plate attch 5/16"-18	Unbrako	combined	42603	3.9	8
$\frac{1}{2}$ " plate attch 5/16"-18nut	140ksi ult	Thrd shr	18373	3.1	8
Isolator I beam buckling	Alum	buckling	Sig crit=17ksi	13.9	10
Isolator plates	Alum	bending	362	96.7	11
Isolator/plate I/f 3/8"-unf	unbrako	combined	44220	3.8	13
Tie down straps	na	na	Pmax = 4.5 kips	na	16
WF8x5 I beams (fork loads)	Alum	bending	1575	22.2	18



ACD PSR

TRANSPORTATION ANALYSIS RESULTS



<u>Finite Element Model Factor of Safety Summary</u> <u>Need picture of model or delete</u>						
Item	Load Case	Stress (psi)	F.S.yield	Page		
Pallet Plate Stresses v.m.	1	383	91.4	Al		
Pallet Beam End A max comb.	1	368	95.1	A2		
Pallet Beam End A min comb.	1	-445	78.7	A3		
Pallet Beam End B max comb.	1	402	87.1	A4		
Pallet Beam End B min comb.	1	-391	89.5	A5		
Pallet Plate Stresses v.m.	2	383	91.4	A6		
Pallet Beam End A max comb.	2	382	91.6	A7		
Pallet Beam End A min comb.	2	-373	93.8	A8		
Pallet Beam End B max comb.	2	394	88.8	A9		
Pallet Beam End B min comb.	2	-463	75.6	A10		
Pallet Plate Stresses v.m.	3	342	102.3	A11		
Pallet Beam End A max comb.	3	413	84.7	A12		
Pallet Beam End A min comb.	3	-383	91.4	A13		
Pallet Beam End B max comb.	3	359	97.5	A14		
Pallet Beam End B min comb.	3	-453	77.3	A15		
Pallet Plate Stresses v.m	4	383	91.4	A16		
Pallet Beam End A max comb.	4	359	97.5	A17		
Pallet Beam End A min comb.	4	-370	94.6	A18		
Pallet Beam End B max comb.	4	376	93.1	A19		
Pallet Beam End B min comb.	4	-389	90.0	A20		



CERTIFICATION TESTS



- Shipping Dolly Static Load Test to 1.25g
- Shipping Dolly Fork-Lift Test to 1.25g
- Trailer Maintenance
- Route Survey Two Weeks Prior to Ship
- Road test waived due to similarities to GLAS shipment





CONTINGENCIES



<u>EVENT</u>

- Severe Weather during transport
- Severe Weather at SLAC upon arrival
- Flat Tire
- Tractor Mechanical Problems
- Sick Driver
- Climate Control Unit Fails
- Isolator Coil Fails
- Low Purge Supply
- Emergency Road Closure

<u>ACTION</u>

- Use driver's discretion
- Wait to unload
- Repair
- Repair/Replace
- **Dual Drivers**
- Redundant
- Multi-Redundant Coils Per Isolator
- Minimal Impact On Isolation
- 100% margin during trip; Bottles coupled with manifold
- Contact State Transportation Authorities/ or Local Police





No Road Test Justification

	GLAS	GLAST	
# of coil isolators	6	8*	
Isolation frequency	13 Hz	13 Hz	
Center of gravity	77" from rear	64.02" from rear	
Weight	3000 lbs	3466 lbs	

Modifications performed for GLAST shipment

- •Added 2 plates to support ACD
- •Added 2 channels to support forklift

•*Added 2 isolators to reach desired stiffness







Safety

Jim Anderson/Andrew Kofeldt Systems Safety Engineer SRS Technologies/Code 302



Safety ACD PSR HAZARDS



- Transportation

- ACD will be shipped single bagged with the Purge Tent as a cover
 - -Purge is dry air, no asphyxiation hazard
 - -Protect unit from objects falling against or on cover
- Transportation is in an enclosed vehicle
- ACD transportation dolly has been proof tested and certified for use
- SLAC Operations
 - GSFC has had regular contact with SLAC Safety through periodic phone calls and face-to-face meetings
 - SLAC aware of all ACD safety issues through contacts and preparation of the overall LAT Preliminary Hazard Analysis



Safety ACD PSR HAZARDS



- SLAC lifting & handling procedures will be reviewed by GSFC Safety
 - The initial lift of the ACD at SLAC will be witnessed by GSFC Safety as well as SLAC
 - Initial removal from Transport Vehicle uses Forklift
 - -ACD personnel/SLAC vehicle operator and Procedure
 - -First crane lift is from Shipping fixture onto ACD Dolly
 - -ACD personnel and Procedure/SLAC crane operator
 - Lifting hardware has gone through all required analysis and certification and is inspected for possible damage before each use
 - All lifting operations are supported by safety and are conducted in accordance with a safety-approved hazardous operations procedure



Safety Applicable Documents



- GLAST ACD Instrument and Ground Support Packaging, Handling and Transportation Plan, GLAST ACD Plan-001
 - Reviewed and Approved
- NASA-STD-8719.9 NASA Standard Lifting Standard
 - All hazardous operations procedures and work order authorizations are reviewed and approved by project safety prior to use







SUMMARY

Tom Johnson ACD Instrument Manager Code 556

SUMMARY





- The ACD successfully passed all environmental and performance testing!
- The ACD demonstrated it meets its performance requirements, with significant margin!
- The few anomalies seen during testing do not significantly impact the performance of the ACD and will be addressed at LAT level testing using new interface hardware and software.
- All open liens/non-conformances have been identified and a close out plan has been developed for each one.
- Following final stay clear measurements, thermal blanket removal, and cleaning, the ACD will be ready for installation on its shipping dolly.
- The Team is fully prepared to ship the ACD to the Stanford Linear Accelerator Center!

Let's get ACD on the road to SLAC!!!