

1

at Stanford Linear Accelerator Center

<u>An Overview of</u> <u>Ground Motion and Vibration</u> <u>Studies</u>



Acknowledgements

- SLAC Accelerator Physics: Andrei Seryi, Fredric Le Pimpec
- SLAC Conventional Facility:

Clay Corvin, Javier Sevilla, Jerry Aarons

• Colin Gordon & Associates:

Hal Amick, Tao Xu, Nat Wongrasert

• DMJM & Harris:

Sven Svendsen

• Parsons/Geovision team:

Bruce Shelton, Paul MacCalden Robert Nigbor, Rod Merrill, Brent Lawrence

• Seismic I solation Engineering (SIE inc.):

Fred Tajirian, Mansour Tabatabaie









at Stanford Linear Accelerator Center

Representative LC Site- Logan Ridge, California



1. View South

A typical sandstone outcrop at the site is shown below. The near surface rock is soft, competent and well blocked. High tunnel boring machine advance rates are obtainable in sandstone. It is an ideal rock for the LC.



View West & Vibration Station



Surface measurements of vibration are plotted below and are comparable with those in the LEP tunnel. They exceed the goals for X-band stability and they can be found in a variety of locations worldwide.



International Linear Collider

at Stanford Linear Accelerator Center <u>Representative LC Site- Dekalb, Illinois</u>



The measurements plotted above are taken in NUMI tunnel at shallow depth and in Aurora mine. Despite the surface being populated and moderately urbanized, the underground locations are relatively quiet.





The Galena-Platteville Dolomite is shown above in outcrop. Beneath the DeKalb LC site at a depth of ~300 ft these two units make up a 300+ ft thick, near horizontal, uniform, carbonate unit which has excellent rock mass characteristics that make it an ideal rock for the LC. International Linear Collider











at Stanford Linear Accelerator Center

Characterization of Vibration Sources in the Support Tunnel



Average integrated displacement at the base of the modulator and near its support. Modulator pulsed noise @ 60 Hz:

- < 30nm on the modulator < 12 nm on the floor
- (within acceptable limit)



16GPM water and Chiller ON **Chiller Vibration** -----Inside chiller - spring Inside chiller - Boltec at foot of the chiller - Bolted foot of the chiller - spring 10-7 Jispl **Floor Vibration** 10-9 10⁰ 10^{2} 103 10 Freq : Hz

The chiller (~700 lb) shown here vibrates by 2-3micron at 59Hz. If mounted rigidly, it transmits ~30nm to the floor near the support. Same chiller mounted on soft spring transmits considerably less vibration to the floor (<nm).



International Linear Collider

Experimentally

determined the

two construction

vibration

tunneling

at Stanford Linear Accelerator Center



Vibration transmissibility was measured at two locations:

•At SLAC along Sector 9 and 10 for Cut-&-Cover construction method

-Eocene sandstone and claystone (shear velocity of ~720 m/se

•At the Los Angeles County Metropolitan Transportation Authority (MTA) Red Line tunnels near the Universal City Station for shallow tunneling construction method

-Miocene sandstone and shale (shear velocity of ~950 m/sec) Fred Asiri



•At SLAC along Sector 9 and 10 for Cut-&-Cover construction method

ILC- Snowmass 2005- WG 4





at Stan	ford L	inear A	lccele	erator	Center
---------	--------	---------	--------	--------	--------

Source	Receiver	Distance, ft	Attenuation at Given Frequency			
			10 Hz	20 Hz	30 Hz	60 Hz
S1	R1	130	0.014	0.0084	0.012	0.005
	R2	134	0.012	0.012	0.014	0.004
	R3	162	0.011	0.0084	0.006	0.001
	R4	233	0.010	0.004	0.002	0.001
	R5	289	0.005	0.002	0.0009	0.0003

The figures in the above table represent the attenuation Factor for a vibration with its source near S1 propagating along the same path.

Example 1: Suppose a pump is installed at S1, and it produces a vibration at 60 Hz with an amplitude of X. The amplitude at 60 Hz that we measure at R5 would be the greater of either ambient or 0.0003X.

Example2: If we want to place a pump at S1 and not to exceed ambient at R5 (0.6μ in/sec), then we need to impose a limit on the resulting vibration at S1 of 0.6/0.0003=0.002 in /sec.



Ambient Vibration at Receiver Location R5



Log Mean Transmission From Drive Point S!





The LCC-0122 and LCC-0123 have been revised and the revisions are posted:



Fred Asiri

39,



International Linear Collider

at Stanford Linear Accelerator Center

Support to Beam tunnel transmission measured in LA metro tunnels and verified with 3D modeling computer program (SASSI). At 60Hz the mobility across tunnels is ~1 nm/100 Newton's permitting moderate vibration in Support tunnel. If required, vibration due to rotating equipment can be eliminated with standard inexpensive means, e.g. 3Hz springs.













Comparison of Calculated and Measured Mobilities



Comparison of Maximum Calculated and Measured Velocities in Tunnel B, Lower Bound and Upper Bound Soil

The results of the 3-D computer simulation program "SASSI" and the measured vibration data from the MTA tunnel tests are correlated.

> The SASSI simulation computer program can be used to predict the attenuations of vibration emanating sources in the support tunnel to the vibration sensitive equipment in the beam tunnel.





Science Vibration and Stability Needs for Warm LC

-Assumptions:

The total beam jitter at the IP is 50% of the beam size, with the following uncorrelated contributions:

30% from the main linac, 30% from the beam delivery, 25% from the final doublet, and with 15% injection jitter, RSS is ~ 50%

Assuming the above jitter budget:

The vertical vibration of the linac quadrupoles needs to be less than 12 nm above several Hz

–Ground stability:

Considering that the normal operations include a 9 month run cycle, followed by a 3 month period for maintenance & alignment,

An annual relative drift rate at the beam pedestal support floor should be less than +/- 2 mm over a distance of 200 meters.

What are the Science Vibration and Stability

Needs for the Cold LC?



Beam Housing Foundation Vibration Criteria-Warm

Vibration Criteria at the invert of Beam Housing

The RMS value of the imported (i.e. added) broadband vibration integrated above 3 Hz should be less than a factor of two (2) times the preexisting ground vibration amplitude, excluding the resonant "spike" vibrations synchronous with collider repetition rate.

With the resonant spikes included, the RMS amplitude above 3 Hz should be less than a factor of three (3) times the pre-existing ground vibration amplitude.

m²/Hz

Its assumed that the preexisting RMS value of the vertical component of ground vibration amplitude is less than two nanometers integrated above 3 Hz.



at Stanford Linear Accelerator Center

International Linear Collider

DRAFTED FROM WARM

Beam Housing Foundation Vibration Criteria-Cold Vibration Criteria at the invert of Beam Housing

m²/Hz

The RMS value of the imported (i.e. added) broadband vibration integrated above 3 Hz should be less than a factor of two (2) times the preexisting ground vibration amplitude, excluding the resonant "spike" vibrations synchronous with collider repetition rate.

With the resonant spikes included, the RMS amplitude above 3 Hz should be less than a factor of three (3) times the pre-existing ground vibration amplitude.

Its assumed that the pre-existing RMS value of the vertical component of ground vibration amplitude is less than 5 nanometers integrated above 3 Hz. and less than 20 nanometers integrated above 0.5 Hz.





at Stanford Linear Accelerator Center

What should be done next?

• To measure ambient ground noise (natural, far-field) for the ILC Sample Illinois sites at or near the Interaction Point

> We are planning to conduct this task

• To identify and to characterize the major vibration sources (cultural, near-field) for the cold machine sub systems

Cryogenics systems (Compressors), LCW cooling system, rotating mechanical and electrical equipment (L-Band Modulator)

• To adopt the vibration criteria (goals) and to determined the stability parameters for the cold machine (similar to the one for the warm machine)

>Vibration budget for the cold machine is higher, but so the imported noises

• To utilized 3-D computer modeling and to modify the parameters for the ILC Sample site

>SASSI models can be used to parametric predict transmissibility functions

> Mitigate vibration effects by trying different options, tradeoff

> This can lead to better optimization of design requirements, as well as to better manage the ILC vibration budget