



Cryomodule Plans at KEK

KEK

Norihito Ohuchi and Kiyosumi Tsuchiya



1) Target of the cryostat R&D in KEK

- Gaining the experience of the long cryostat for the S.C. cavity.
- R&D of a high performance and low cost ILC cryostat.
- Cooling two types of the cavities of 35 MV/m and 45 MV/m down to 2 K in STF, and performing high power and beam tests.

2) Strategy of the cryostat R&D

- Starting point of the STF cryostat design: **TESLA design**
- R&D and study items for the STF cryostat
 - Understanding the TESLA design from the cryogenic hydrodynamic point of view.
 - Heat transfer of the superfluid helium, pressure drop, and temperature distribution in the system.
 - R&D component
 - SUS-Ti joint between the helium vessel and cryogenic lines.
 - Magnetic shield
 - Measurement of the remanent field in the shield and the magnetic characteristics of the shield material.
 - Low cost vacuum system for the STF cryostat
 - Survey of the low cost quadrupole magnet system



3) Status of the cryostat R&D in KEK

- FY2005
 - Finalizing the conceptual design of the cryostat for the STF in KEK.
 - The design of the overall assembly has been completed.
 - Making a contract with a company for the construction of the cryostat.
 - The company will be decided at the 24th of August.
- FY2006
 - Design and construction of the tools for assembling the cavities into the cryostat.

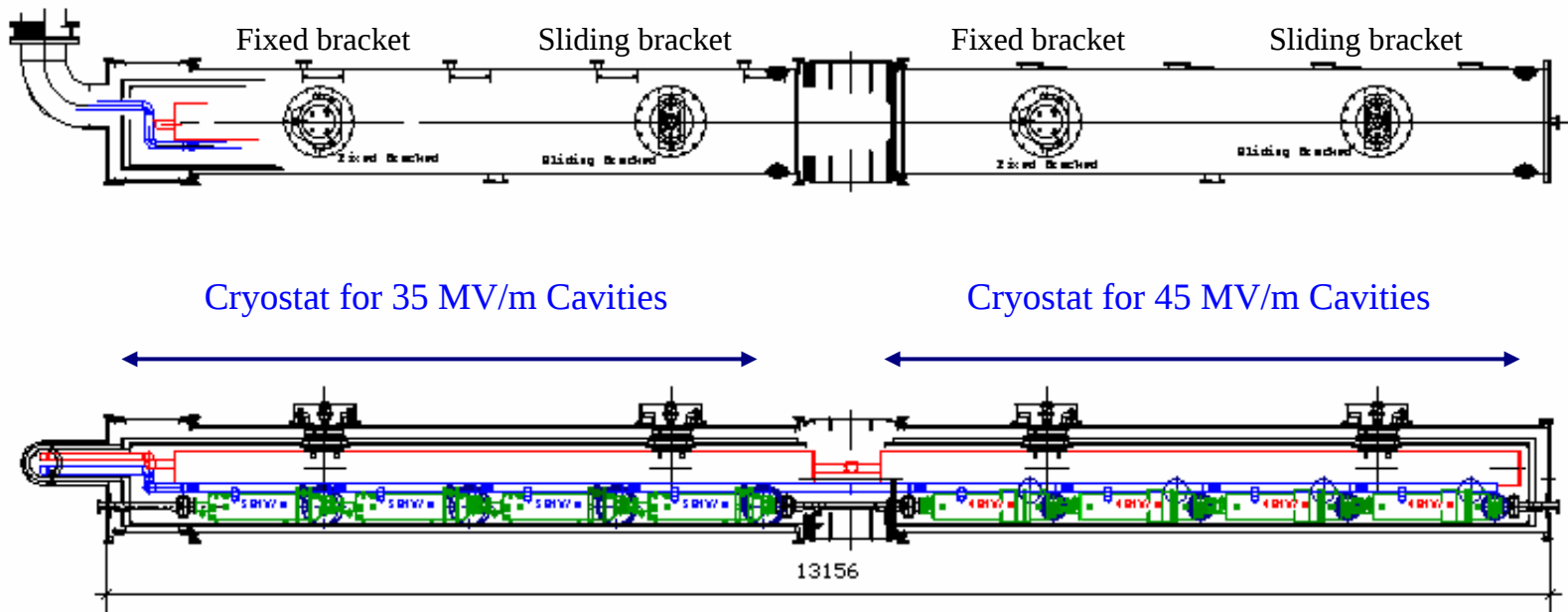
4) Technical issues in the STF phase-1 cryostat

- Connection of pipes
 - Applying automatic welding as much as possible.
- Material of the cryostat components
 - Vacuum vessel Carbon Steel
 - Pipes for cryogenics SUS304L or 316L (Ti for the 35 MV/m cavity)
 - Thermal radiation shield Al 1050
 - Vacuum seal at room temp. O-ring
 - MLI (super-insulation) Polyester film
- Tuning resolution of cavity alignment $< 50 \text{ } \mu\text{m}$



STF cryostat

Overall design



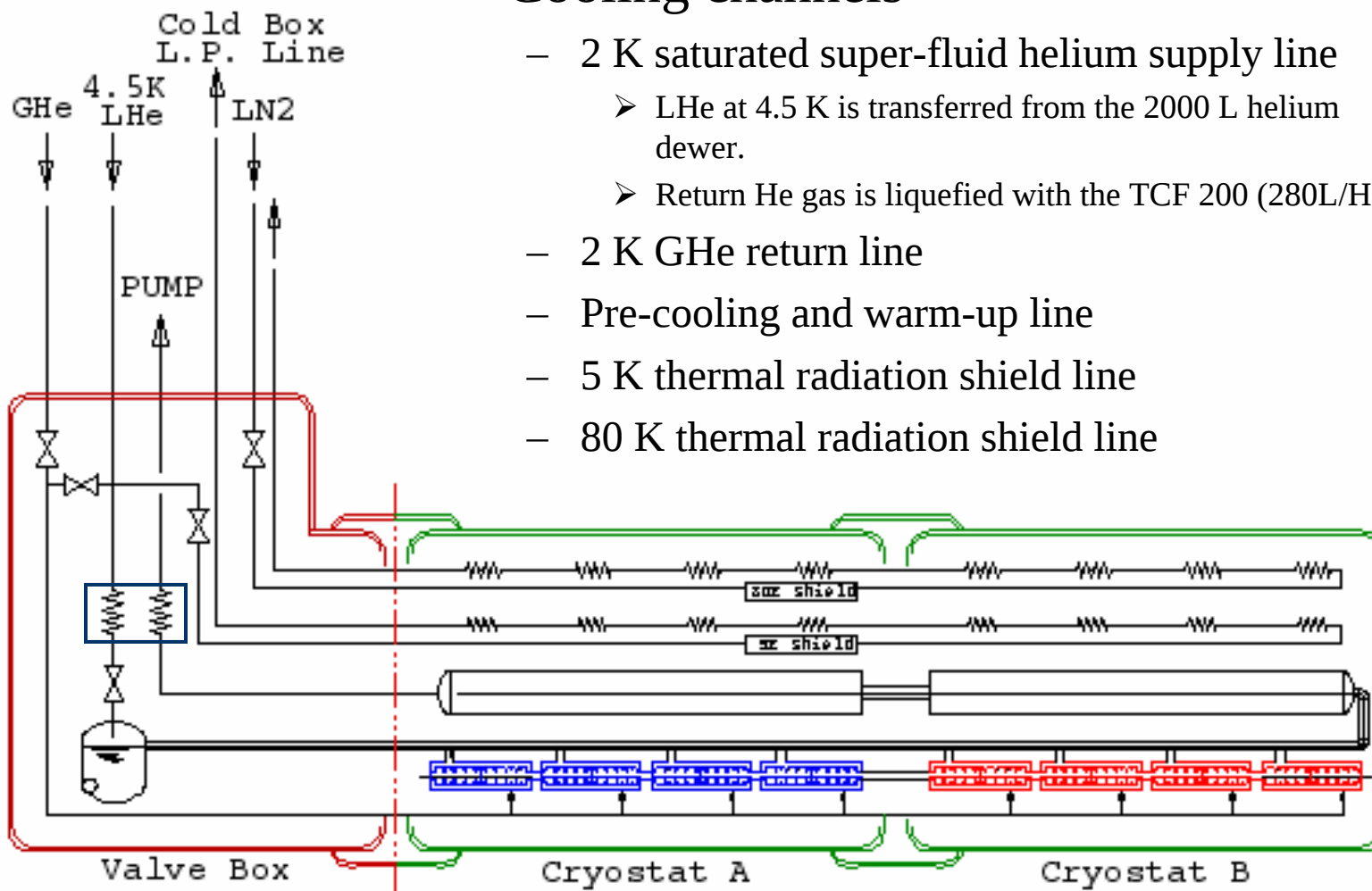
- Total weight of cryostat = around 5.6 ton.
- The lengths of the vacuum vessels for 35MV/m cavities and 45 MV/m cavities are 5545 mm and 5907 mm, respectively .
- The lengths of the 2K Gas return pipes for two cryostats are identical, 5830 mm.
- The most up-stream cavity-jacket is fixed for each cryostat by the support near the fixed bracket for each cryostat, and the other supports are free in the axial direction.
- The position of the jacket with respect to the input coupler is kept at almost constant with a Invar rod during cool-down.



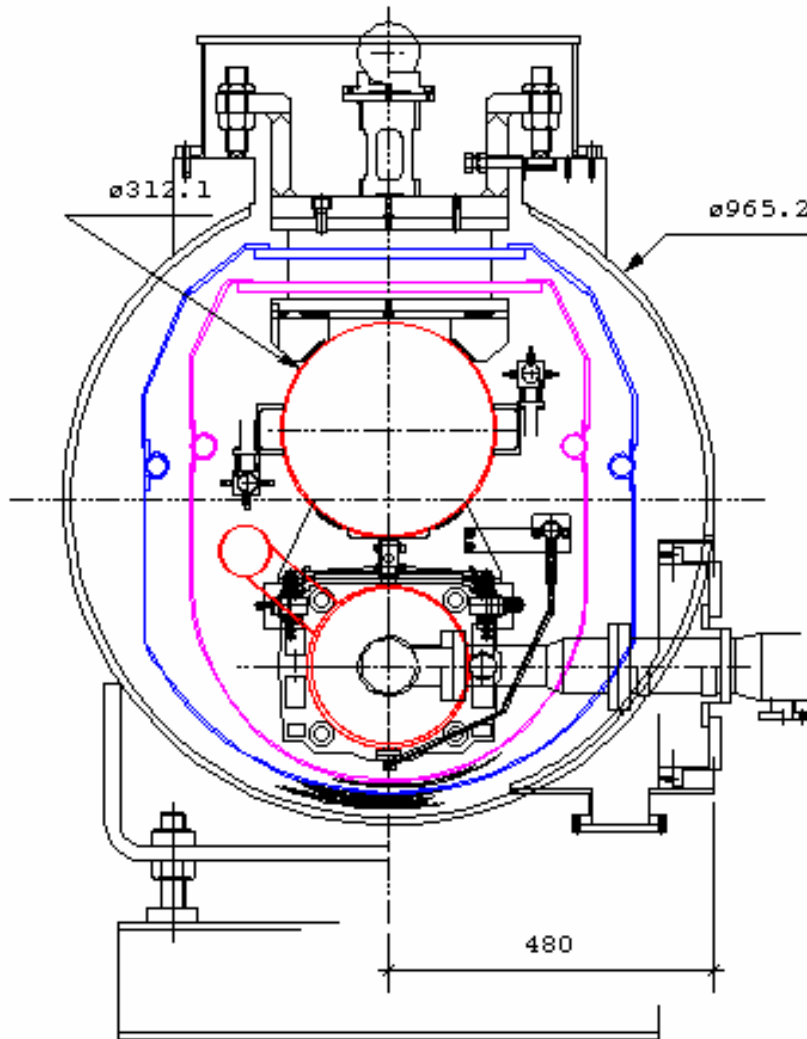
Cooling circuits

- Cooling channels

- 2 K saturated super-fluid helium supply line
 - LHe at 4.5 K is transferred from the 2000 L helium dewer.
 - Return He gas is liquefied with the TCF 200 (280L/H).
- 2 K GHe return line
- Pre-cooling and warm-up line
- 5 K thermal radiation shield line
- 80 K thermal radiation shield line

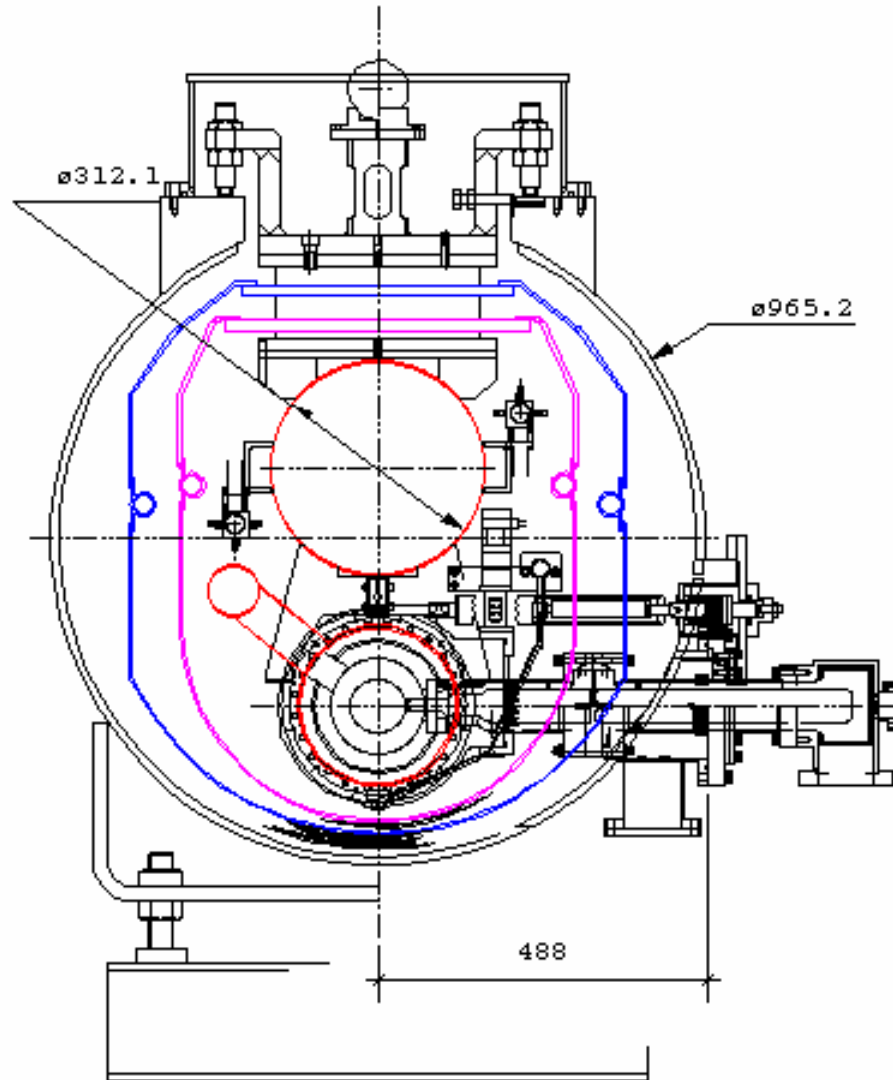


Cross section of the 35 MV/m cryostat



- Outer diameter of the vacuum vessel is same as the diameter of the TESLA cryostat.
- Support system of the cavity is slightly different from the TESLA system.
- The distance between the vacuum vessel and the input coupler is around 10 mm.
- The thermal radiation shields have the cooling pipes in the left and right symmetry.

Cross section of the 45 MV/m cryostat



- Support system of the cavity is same as the TESLA system.
- The distance between the vacuum vessel and the input coupler is around 10 mm.



Thermal contraction

Cooling pipe (SUS: $L/L = -0.265\%$)

	Pipe end @valve box	GHe pipe end @up-stream	Fixed support bracket	Sliding support bracket	GHe pipe end @down-stream
Position (mm)	2571	1376	0	-3153	-4454
L (mm)	-6.8	-3.7	0	-8.4	-11.8

Thermal radiation shield (Al: $L/L = -0.33\%$ @80K, $L/L = -0.368\%$ @5K)

	Shield end	Fixed support bracket	Sliding support bracket	Shield end
Position (mm)	1858	0	-3153	-4454
L for 80 K shield (mm)	-6.1	0	-10.4	-14.7
L for 5 K shield (mm)	-6.8	0	-11.6	-16.4

Components

	Support post 300-4K $L/L = -0.338\%$	Cavity (Nb) 300-4K $L/L = -0.129\%$	Ti jacket 300-4K $L/L = -0.134\%$	SUS jacket 300-4K $L/L = -0.265\%$	Invar rod 300-20K $L/L = -0.034\%$
L (mm)	140 (in vertical)	1260	1260	1260	5000
L (mm)	-0.47	-1.63	-1.69	-3.34	-1.7



Cryostat pipe size

	STF-phase1	TESLA	Material
Vacuum vessel	965.2, t 12	965.2 , t 9.52	carbon steel
2 K He Gas return	318.5, t 6.5	312 , t 6	SUS
2 K two-phase supply	76.3 , t 2.1	76 , t 2.0 (60 , t 1.5)	Ti or SUS
Cool down/warm up	27.2 , t 1.65	42.2 , t 1.65	SUS
5 K shield supply	30 , t 4	60.3 , t 2.76	SUS
5 K shield return	30 , t 4	60.0 , t 5	SUS
80 K shield supply	30 , t 4	60.3 , t 2.76	SUS
80 K shield return	30 , t 4	60 , t 5	SUS



Construction schedule of the STF cryostat

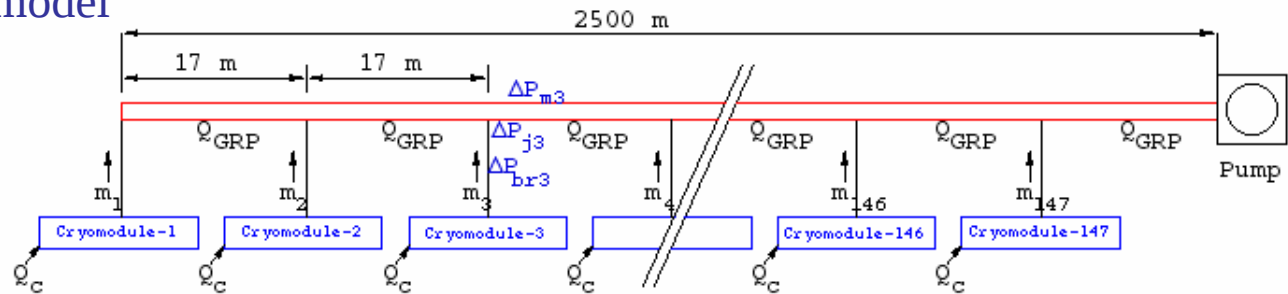
	2005				2006			
	Jan~Mar	Apr~Jun	Jul~Sep	Oct~Dec	Jan~Mar	Apr~Jun	Jul~Sep	Oct~Dec
Conceptual design	←→							
Safety code survey	←→							
Detailed design			←→					
Fabrication			←→					
Assembling						←→		
Installation into STF							←→	
Cool down test								←→



Hydrodynamic study

ILC model (Pressure and temperature profile along the GRP of 300)

Calculation model



Q_c : 10 W or 30 W

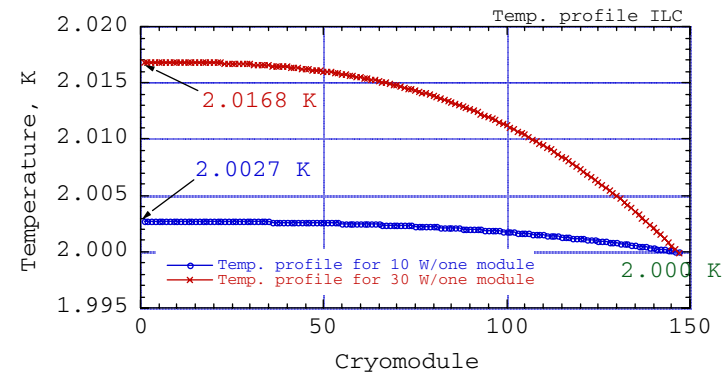
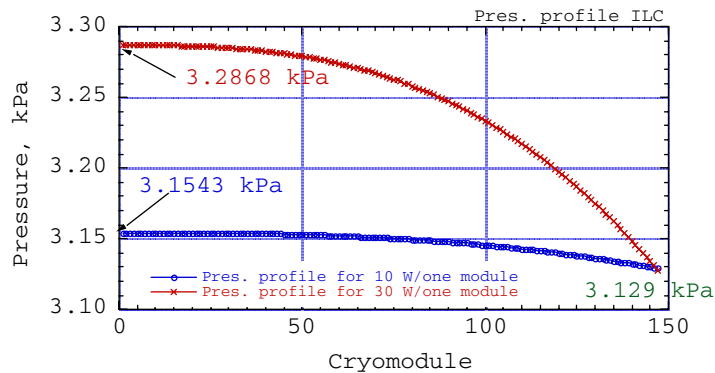
Q_{GRP} : 1 W

m_n : evaporated helium gas at n-th module

P_{mn} : P by mass flow along n-th section

P_{jn} : P by confluence at n-th section

P_{bn} : P along n-th branch pipe



- Pressure drop along the 2.5 km GRP = 25 Pa for 10 W, 158 Pa for 30W
- Temperature difference along the 2.5 km GRP = 3 mK for 10 W, 17 mK for 30W



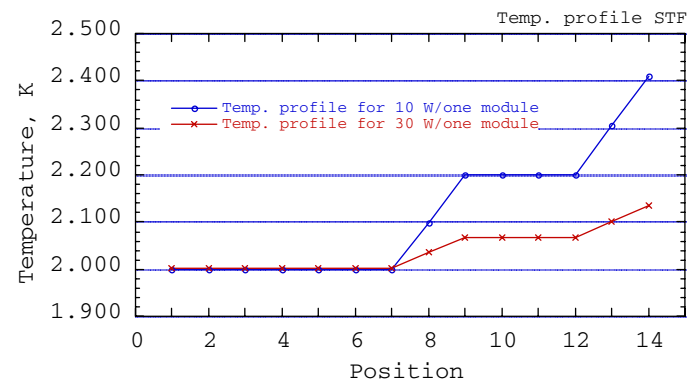
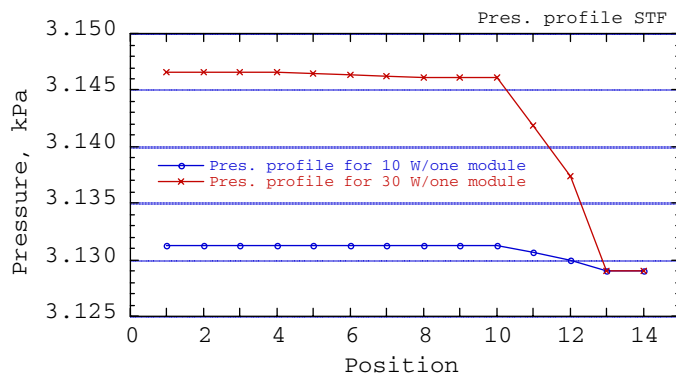
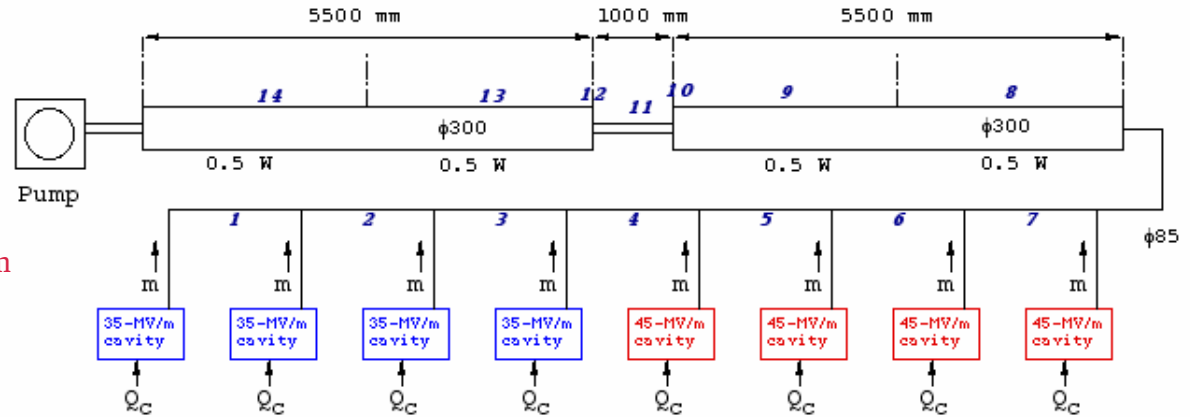
STF phase-1 model

Calculation model

Q_c : 10/8 W or 30/8 W

m: evaporated helium gas

Pipe diameter of section 11 : 30 mm



- Pressure drop along the system = 2.27 Pa for 10 W, 17.59 Pa for 30W
- Temperature at each cavity = 2.000 K for 10/8 W, 2.002 K for 30/8 W

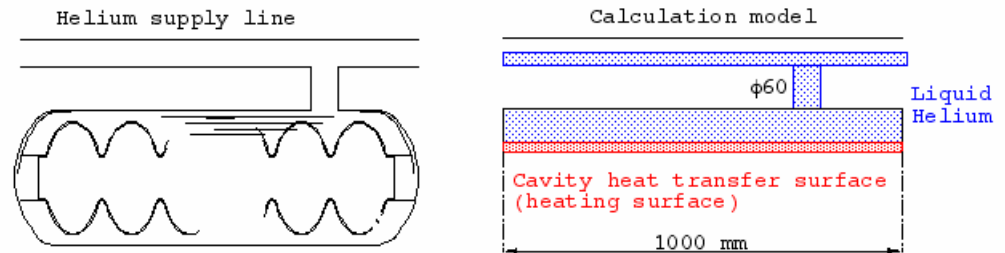


Temperature profile in the helium jacket

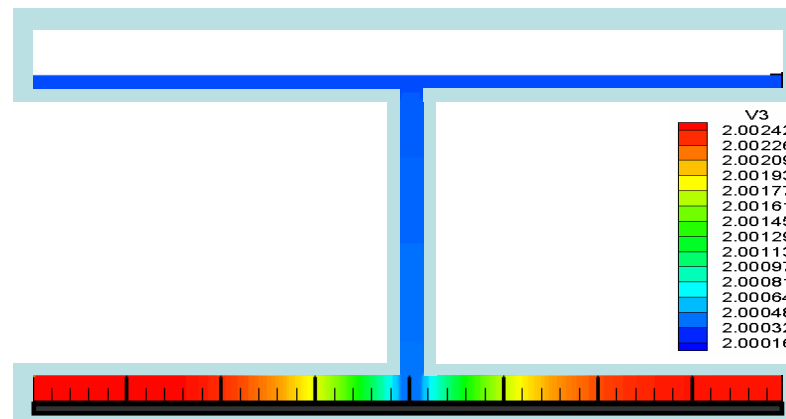
(calculation of temperature profile in LHe to confirm the maximum temperature less than Lambda temperature)

Calculation model

- Pipe diameter between LHe supply line and cavity jacket = 60 mm
- Cavity jacket length = 1000 mm
- Distance between cavity heating surface and jacket inner surface = 6 mm
- Heat load = 30.0 / 4 W



Temperature profile after 4.6 seconds



- The diameter of 60 mm for the pipe between the LHe supply line and the cavity jacket is enough to keep the LHe temperature below the Lambda temperature.



SUS-Ti joint R&D

- **Joining by HIP (Hot Isostatic Pressing)**
 - Important concern : diffusion of Fe, Cr and Ni into Ti
--> degradation of strength at low temperature
 - Manufacturing samples with the insert materials
 - V on the surface of Ti and Cu on the SUS
 - The following tests will be performed in this year.
 - ☐ Tensile tests at room temperature and liquid nitrogen temperature.
 - ☐ Charpy V-notch impact tests at room temperature and liquid nitrogen temperature.
 - ☐ Helium leak tests at 2 K.
- **Friction pressure welding**
 - Diffusion rates of Fe, Cr and Ni into Ti are less than the rates by HIP.
 - Need to measure the strength of the joint.
 - The manufacturing method of the samples is under investigation.



Magnetic shield

- Remanent field in the vacuum vessel
 - Survey of the measuring system for weak magnetic field
 - Calculation of the distribution of remanent magnetic field in the cryostat
 - Study of the magnetization in the manufacturing process of the cryostat
- Measurement of the magnetic characteristics of the shield material
 - Temperature dependence
 - Effect of machining process
 - Effect of heating process

Cryogenic sensors and heat load measurement

- Cryogenic sensors
 - Selection of cryogenic temperature sensors; Cernox, CGR and TVO
 - Liquid helium sensor; behavior of the sensor around the Lambda point
- Heat load measurement of the cryomodule
 - Measurement of the heat load from each component in the module
 - Separation between the static and dynamic heat loads



Quadrupole magnet

- **TESLA design**
 - The magnet is cooled by super-fluid helium in the jacket.
 - Ceramic insulators are required for the current leads.
 - In case of applying the HTC current leads, the insulators are installed on the metal jacket.
 - Magnet assembly in the cryostat is complicated

- **Study of the alternative magnet system**
 - The possibility of the magnet system cooled by conduction
 - Optimization of the operation temperature
 - Simulation of the cool-down process after magnet quench (cool-down time)
 - System configuration



Summary

- The design of the cryomodule for the STF phase-1 is based on the TESLA design.
- This cryomodule will have been manufactured in 2006, and in October of 2006, we will start various tests of the cryostat and the RF system in the STF.
- R&D items for the cryomodule
 - Study of thermal and hydrodynamic behavior of the R&D cryostat
 - SUS-Ti junction
 - Magnetic shield
 - Vacuum system
 - Survey of the quadrupole magnet system cooled by thermal conduction