



SiD Solenoid at Snowmass

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- What is the SiD Solenoid?
- Add Dipole in Detector to SiD model
- "Publish" fieldmaps: "beamline" from 2D model; Inner Detector from 3D model
- Normalize Cost SiD magnet cost model to CMS "as built" data...





High Field, Large Size create many challenges

- Look for Proof of Principle...
 - Only "High Field" Operating Solenoids at <u>2T</u>: DØ, Atlas; at <u>3T</u>: AMY (cryostable,
 - heavy/expensive pressure vessel)
- Closest is (may be?) CMS: 4 T,
 2.7 GJ, Ø = 6m, L = 13 m
- Develop Preconceptual Design "Along Lines of" CMS
 - Expedites Approach to Credible Conductor/Winding Designs
 - Credible Engineering Approach for Industrial Fabrication
 - Credible Cost Estimates





Follow CMS Conductor, Winding Designs





- First Cut: Same conductor as CMS
- Winding Design: CMS (4 layer)→ SiD (6 layer)
- CMS 5 modules 2.5 m long → Sid 2 modules 2.6 m long
- Choose 6 layers (tradeoffs), "derate" CMS conductor to 5.8 T peak field (vs. 4.6 for CMS). I (CMS) = 19500; I (SiD) = 18000.
 - Critical current Ic(4.2K, Bpeak) derates 46900/59000 ~ 0.79
 - Iop derates ~ 0.92
 - <u>Stability expectations require modeling</u>; <u>32 CMS strands => 34</u> <u>for SiD</u>



2D, 3D ANSYS Models









(AVG)

UΧ

RSYS=0

PowerGraphics EFACET=1





solenoid axis

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"Barrel"

shape from

energization



Von Mises Stress in Winding Pack, Cold & Energized





Quantity	SiD	CMS
Von Mises Stress in High- Purity Al	22.4 MPa	22 MPa
Von Mises Stress in Structural Al	165 Mp a	145 MPa
Von Mises Stress in Rutherford Cable	132 MPa	128 MPa
Maximum Radial Displacement	5.9mm	~5mm
Maximum Axial Displacement	2.9mm	~3.5mm
Maximum Shear Stress in Insulation	22.6 MPa	21 MPa

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Compare with CMS



Quantity	SiD	CMS
Radial Decentering	38 kN/mm	38 kN/mm
Axial Decentering	230 kN/mm	85 kN/mm
Stored Energy	1.4 GJ	2.8 GJ

• Conclude cryostat approach can be like CMS:

Requirements

- Cold mass support 130 Mt
- React decentering forces, seismic, cooldown, steady-state operation

CMS Concept

- Thin metallic rods preloaded in tension
- Axial rods for axial loads
- Vertical rods for dead weight
- Additional tangential rods (in preloaded pairs) for radial loads





Iron Yoke Issues





Endplate gussets support barrel Layers, allow insertion of muon chambers

> Maximum deflections (loaded with calorimeters, solenoid) ~0.3 in

Barrel (and End Caps): Steel plates 10 cm thick, 5 cm gaps



NODAL SOLUTION STEP=1 SUB =1 TIME=1 UY (AVG) RSYS=0 **PowerGraphics** EFACET=1 AVRES=Mat DMX =.300153 SMN =-.299074 SMX =.019215 -.299074-.263709 -.228343-.192978-.157612-.122247-.086881 -.051516 -.01615.019215

Vertical Deflections for Staggered Barrel Iron Connections (units = inches)

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Calculation for single winding layer highlights nonuniformity of conductor







Layers aligned to maximize nonuniformity of conductor







• Near-axis field out to Z=20 m



• Central Field - uniformity, etc



Dipole-Integrated-Detector facilitates Crossing Angle





"Saddle-coil" dipole wrapped onto outer support cylinder of solenoid



Forces on Dipole Burdensome, May be Manageable





- Fx = 400K lbs (radial, summed)
- Fz = 1754K lbs (axial, summed)



DID Field on SiD Axis





• DID (zeroes IP vertical angle, SR vertical beamsize growth) compatible with Antisolenoids used for beam-size compensation from solenoid fringe





- Need iterations with Detector/Physics Groups to select "most probable" performance parameters
 - How to "Open" detector ?
 - Must Detector Roll "off beamline" ?
 - Anti-solenoids in forward region
 - EndCap steel support details
 - Muon steel plate/gap thicknesses
- Field Homogeneity not specified (Must we?)
- Radiation Transparency not specified (OK?)
- "Fallback" field (below which physics is compromised not specified (SiD should specify)
- Develop Cost Model based on CMS actuals

