# Performance Simulation of the LiCAS-RTRS Survey Train

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The proposed LiCAS<sup>1</sup> metrology system is a novel instrument dedicated to align and monitor the mechanical stability of a future linear high energy  $e^+e^-$  collider. LiCAS uses Laser Straightness Monitors (LSM) and Frequency Scanning Interferometry (FSI) [1, 2] for straightness and absolute distance measurements, respectively. This paper presents detailed simulations of a LiCAS system operating inside a Rapid Tunnel Reference Surveyor (RTRS train). With the proposed design it is feasible to achieve the required vertical accuracy of the order of  $\mathcal{O}(200) \,\mu m$  over 600 m tunnel sections meeting the specification for the TESLA collider [3].

# **1. PRINCIPLE OF THE LICAS-RTRS TRAIN OPERATION**

Technical details of the LiCAS-RTRS train were introduced in separate presentations [4, 5]. In figure 1 the schematic view of the LiCAS train operating in the accelerator tunnel is presented. The train is composed of 6 cars, the distance between the centres of neighbouring cars is ~ 4.5 m. Each car is equipped with 4 CCD cameras and two beam splitters (BS) constituting the straightness monitor. The straightness monitor measures the transverse translation  $(T_x, T_y)$  and transverse rotation  $(R_x, R_y)$  with respect to a z axis defined by the laser beam passing through all cars in a vacuum pipe. The laser beam is reflected back using the retro-reflector (RR) located in the last car, illuminating the upper CCD cameras of the straightness monitors. 6 FSI lines placed in the same vacuum pipe between each pair of cars are responsible for the distance measurement along the z axis  $(T_z)$ . In addition a clinometer located on each car provides a measurement of rotation around the z axis  $(R_z)$ . When the train stops in front of the wall markers it firstly measures the relative position and rotation of all cars with respect to the first car. This defines the local reference frame of the train in which the location of the wall mounted reference markers are measured next. This procedure is repeated for each train stop. Each marker is measured up to 6 times. Finally the coordinates of each marker, expressed in the local train frames are transformed to the frame of the first train (the global frame) by fitting them to each other under the constraint that wall markers have not moved during the entire measurement.

## 2. OPTO-GEOMETRICAL MODEL OF THE LICAS-RTRS TRAIN

In order to study the expected precision on the position reconstruction of the tunnel reference markers a simulation of the LiCAS survey train was performed. To describe the sensing parts of the train the SIMULGEO [6] package was used which allows for modelling of the opto-geometrical systems. This software is also capable of performing the full error propagation including correlations between various sub-components linked via common mechanical supports.

<sup>&</sup>lt;sup>1</sup>Linear Collider Alignment and Survey: R&D group at the University of Oxford.



Figure 1: Principle of the LiCAS train operation. Top view of the two train stops along the accelerator tunnel are presented. For detailed description see text.

## 2.1. Results of the train simulations

Presented results were obtained assuming the intrinsic resolution of the CCD cameras and FSI lines equal to  $\sigma_{CCD} = \sigma_{FSI} = 1 \,\mu m$ . The assumed precision of the clinometer was  $\sigma_{tilt} = 1 \,\mu rad$ . The simulation was performed under the assumption that all calibration constants (positions and rotations of CCD cameras, beam splitters, FSI light sources and retro-reflectors) are known to the accuracy of  $\sigma_{pos} = 1 \,\mu m$  for positions and  $\sigma_{ang} = 1 \,\mu rad$  for angles.

The long-distance operation of the train inside the accelerator tunnel was simulated by a set of many identical trains displaced by 4.5 m (distance between stops), each pair of them coupled via 5 overlapping wall markers. SIMULGEO calculations provide very precise results (taking into account correlations between subcomponents of the system) based on the exact opto-geometrical model of the survey procedure. However, from the numerical point of view, such an approach, manipulating large matrices, is very time and memory consuming. The 20 train stop results (90 m tunnel section) were obtained after 34 hours of CPU time using 1 GB RAM memory on a 2 GHz machine (the rank of the used matrix was of the order of 10 000). The numerical complexity of these calculations scale like  $N^2$ , where N is the number of involved coordinates. The simulation of the full 600 m tunnel section would require more then 7 weeks of CPU time.

#### 2.2. Random walk model

To overcome the above mentioned limitations a simplified analytical formula inspired by a random walk model was derived to extrapolate the SIMULGEO predictions over long tunnel sections:

$$\sigma_{xy,n} = \sqrt{l^2 \sigma_\alpha^2 \frac{n(n+1)(2n+1)}{6} + \sigma_{xy}^2 \frac{n(n+1)}{2}}, \quad \sigma_{z,n} = \sqrt{\sigma_z^2 \frac{n(n+1)}{2}}$$
(1)

where n is the wall marker number, l is the effective length of the ruler (here: distance between cars), and the corresponding errors are the parameters of the random walk:  $\sigma_{\alpha}$  is the angular error,  $\sigma_{xy}$  are the transverse errors and  $\sigma_z$  is the longitudinal error. In this approach the procedure of accelerator alignment resembles the construction of a long straight line using short ruler. The overall error is a convolution of the precision of the ruler and the precision



Figure 2: LiCAS train simulation (left plot): insertion contains the results of the exact simulation obtained with the SIMULGEO, extrapolated on the main plot to the 600 m tunnel section using the formula from the random walk model. Examples of the random walk trajectories (upper middle plot) and straight line fit to selected trajectory (lower middle plot). RMS of the residua distribution from the straight line fit to the random walk trajectories: horizontal (upper right plot) and vertical direction (lower right plot).

of the placement of the ruler with respect to the previous measurement. The asymptotic behaviour of the formulae from equation no. 1 is:  $\sigma_{xy,n} \sim n^{\frac{3}{2}}$ , and  $\sigma_{z,n} \sim n$ . This fast growth of errors (especially for transverse directions) is a consequence of the fact that the errors are highly correlated and the precision of the  $n^{th}$  element depends on the precision of all previous points. Formulae 1 were fitted to the SIMULGEO points determining  $\sigma_{\alpha}$ ,  $\sigma_{xy}$ ,  $\sigma_z$  and then extrapolated over a 600 m tunnel section (fig. 2 left plot). The obtained predictions refer to the precision of the placement of the  $n^{th}$  accelerator component with respect to the first one. However this is not the ultimate measure of the quality of the accelerator alignment. The relevant parameter is the mean deviation of each component from the ideal straight line which can be expected from the above procedure. To obtain the final prediction on the deviation of the SIMULGEO points (fig. 2 middle column). A straight line was fitted to each trajectory and the corresponding residua were calculated. The extracted RMS values of the residua distributions for each marker along 600 m provide the measure of the accuracy of the whole procedure. Because of high correlation between errors for n and n + 1marker the generated trajectories exhibit much smaller oscillations that would be expected from completely random process. Figure 2 (right column) summarises the results obtained in this analysis demonstrating that the vertical precision of the order of  $\mathcal{O}(100 \, \mu m)$  over 600 m is feasible.

### References

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