

Frequency Scanned Interferometry for ILC Tracker Alignment

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In this paper, we report high-precision absolute distance and vibration measurements performed with frequency scanned interferometry using a pair of single-mode optical fibers. Absolute distance was determined by counting the interference fringes produced while scanning the laser frequency. A high-finesse Fabry-Perot interferometer was used to determine frequency changes during scanning. Two multiple-distance-measurement analysis techniques were developed to improve distance precision and to extract the amplitude and frequency of vibrations. Under laboratory conditions, measurement precision of ~ 50 nm was achieved for absolute distances ranging from 0.1 meters to 0.7 meters by using the first multiple-distance-measurement technique. The second analysis technique has the capability to measure vibration frequencies ranging from 0.1 Hz to 100 Hz with amplitude as small as a few nanometers, without *a priori* knowledge. A possible optical alignment system for a silicon tracker is also presented.

1. INTRODUCTION

The motivation for this project is to design a novel optical system for quasi-real time alignment of tracker detector elements used in High Energy Physics (HEP) experiments. A.F. Fox-Murphy *et.al.* from Oxford University reported their design of a frequency scanned interferometer (FSI) for precise alignment of the ATLAS Inner Detector [1, 2]. Given the demonstrated need for improvements in detector performance, we plan to design an enhanced FSI system to be used for the alignment of tracker elements in the next generation of electron positron Linear Collider detectors. Current plans for future detectors require a spatial resolution for signals from a tracker detector, such as a silicon microstrip or silicon drift detector, to be approximately 7-10 μm [3]. To achieve this required spatial resolution, the measurement precision of absolute distance changes of tracker elements in one dimension should be on the order of 1 μm . Simultaneous measurements from hundreds of interferometers will be used to determine the 3-dimensional positions of the tracker elements.

The University of Michigan group constructed two demonstration Frequency Scanned Interferometer (FSI) systems with laser beams transported by air or single-mode optical fiber in the laboratory for initial feasibility studies. Absolute distance was determined by counting the interference fringes produced while scanning the laser frequency[4]. The main goal of the demonstration systems was to determine the potential accuracy of absolute distance measurements that could be achieved under controlled conditions. Secondary goals included estimating the effects of vibrations and studying error sources crucial to the absolute distance accuracy. The main contents of this proceedings article come from our published paper[5]. However, new material in this paper includes a description of a dual-laser system and a possible optical alignment for a silicon tracker detector.

2. PRINCIPLES

The intensity I of any two-beam interferometer can be expressed as

$$I = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos(\phi_1 - \phi_2) \quad (1)$$

where I_1 and I_2 are the intensities of the two combined beams, and ϕ_1 and ϕ_2 are the phases. Assuming the optical path lengths of the two beams are L_1 and L_2 , the phase difference in Eq. (1) is $\Phi = \phi_1 - \phi_2 = 2\pi|L_1 - L_2|(\nu/c)$, where ν is the optical frequency of the laser beam, and c is the speed of light.

For a fixed path interferometer, as the frequency of the laser is continuously scanned, the optical beams will constructively and destructively interfere, causing “fringes”. The number of fringes ΔN is

$$\Delta N = |L_1 - L_2|(\Delta\nu/c) = L\Delta\nu/c \quad (2)$$

where L is the optical path difference between the two beams, and $\Delta\nu$ is the scanned frequency range. The optical path difference (OPD for absolute distance between beamsplitter and retroreflector) can be determined by counting interference fringes while scanning the laser frequency.

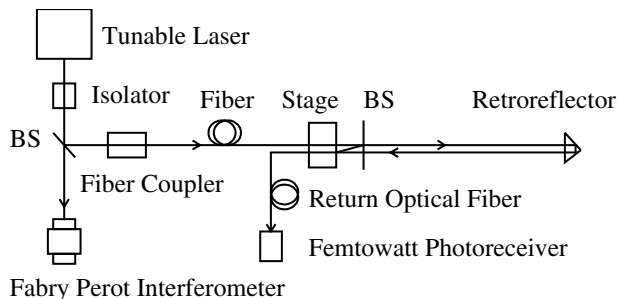


Figure 1: Schematic of an optical fiber FSI system.

3. DEMONSTRATION SYSTEM OF FSI

A schematic of the FSI system with a pair of optical fibers is shown in Fig.1. The light source is a New Focus Velocity 6308 tunable laser ($665.1 \text{ nm} < \lambda < 675.2 \text{ nm}$). A high-finesse (> 200) Thorlabs SA200 F-P is used to measure the frequency range scanned by the laser. The free spectral range (FSR) of two adjacent F-P peaks is 1.5 GHz, which corresponds to 0.002 nm. A Faraday Isolator was used to reject light reflected back into the lasing cavity. The laser beam was coupled into a single-mode optical fiber with a fiber coupler. Data acquisition is based on a National Instruments DAQ card capable of simultaneously sampling 4 channels at a rate of 5 MS/s/ch with a precision of 12-bits. Omega thermistors with a tolerance of 0.02 K and a precision of 0.01 mK are used to monitor temperature. The apparatus is supported on a damped Newport optical table.

In order to reduce air flow and temperature fluctuations, a transparent plastic box was constructed on top of the optical table. PVC pipes were installed to shield the volume of air surrounding the laser beam. Inside the PVC pipes, the typical standard deviation of 20 temperature measurements was about 0.5 mK . Temperature fluctuations were suppressed by a factor of approximately 100 by employing the plastic box and PVC pipes.

Detectors for HEP experiments must usually be operated remotely for safety reasons because of intensive radiation, high voltage or strong magnetic fields. In addition, precise tracking elements are typically surrounded by other detector components, making access difficult. For practical HEP application of FSI, optical fibers for light delivery and return are therefore necessary.

The beam intensity coupled into the return optical fiber is very weak, requiring ultra-sensitive photodetectors for detection. Considering the limited laser beam intensity and the need to split into many beams to serve a set of interferometers, it is vital to increase the geometrical efficiency. To this end, a collimator is built by placing an optical fiber in a ferrule (1mm diameter) and gluing one end of the optical fiber to a GRIN lens. The GRIN lens is a 0.25 pitch lens with 0.46 numerical aperture, 1 mm diameter and 2.58 mm length which is optimized for a wavelength of 630nm. The density of the outgoing beam from the optical fiber is increased by a factor of approximately 1000 by using a GRIN lens. The return beams are received by another optical fiber and amplified by a Si femtowatt photoreceiver with a gain of $2 \times 10^{10} V/A$.

4. MULTIPLE-DISTANCE-MEASUREMENT TECHNIQUES

For a FSI system, drifts and vibrations occurring along the optical path during the scan will be magnified by a factor of $\Omega = \nu/\Delta\nu$, where ν is the average optical frequency of the laser beam and $\Delta\nu$ is the scanned frequency range. For the full scan of our laser, $\Omega \sim 67$. Small vibrations and drift errors that have negligible effects for many optical applications may have a significant impact on a FSI system. A single-frequency vibration may be expressed as $x_{vib}(t) = a_{vib} \cos(2\pi f_{vib}t + \phi_{vib})$, where a_{vib} , f_{vib} and ϕ_{vib} are the amplitude, frequency and phase of the vibration, respectively. If t_0 is the start time of the scan, Eq. (2) can be re-written as

$$\Delta N = L\Delta\nu/c + 2[x_{vib}(t)\nu(t) - x_{vib}(t_0)\nu(t_0)]/c \quad (3)$$

If we approximate $\nu(t) \sim \nu(t_0) = \nu$, the measured optical path difference L_{meas} may be expressed as

$$L_{meas} = L_{true} - 4a_{vib}\Omega \sin[\pi f_{vib}(t - t_0)] \times \sin[\pi f_{vib}(t + t_0) + \phi_{vib}] \quad (4)$$

where L_{true} is the true optical path difference in the absence of vibrations. If the path-averaged refractive index of ambient air \bar{n}_g is known, the measured distance is $R_{meas} = L_{meas}/(2\bar{n}_g)$.

If the measurement window size ($t-t_0$) is fixed and the window used to measure a set of R_{meas} is sequentially shifted, the effects of the vibration will be evident. We use a set of distance measurements in one scan by successively shifting the fixed-length measurement window one F-P peak forward each time. The arithmetic average of all measured R_{meas} values in one scan is taken to be the measured distance of the scan (although more sophisticated fitting methods can be used to extract the central value). For a large number of distance measurements N_{meas} , the vibration effects can be greatly suppressed. Of course, statistical uncertainties from fringe and frequency determination, dominant in our current system, can also be reduced with multiple scans. Averaging multiple measurements in one scan, however, provides similar precision improvement to averaging distance measurements from independent scans, and is faster, more efficient, and less susceptible to systematic errors from drift. In this way, we can improve the distance accuracy dramatically if there are no significant drift errors during one scan, caused, for example, by temperature variation. This multiple-distance-measurement technique is called 'slip measurement window with fixed size', shown in Fig.2. However, there is a trade off in that the thermal drift error is increased with the increase of N_{meas} because of the larger magnification factor Ω for a smaller measurement window size.

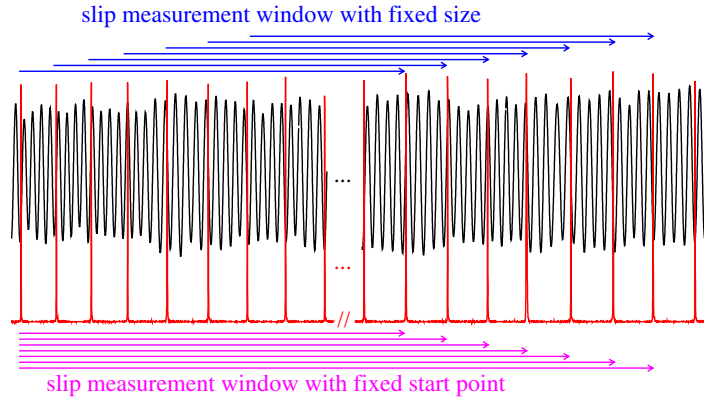


Figure 2: The schematic of two multiple-distance-measurement techniques. The interference fringes from the femtowatt photoreceiver and the scanning frequency peaks from the Fabry-Perot interferometer(F-P) for the optical fiber FSI system recorded simultaneously by DAQ card are shown in black and red, respectively. The free spectral range(FSR) of two adjacent F-P peaks (1.5 GHz) provides a calibration of the scanned frequency range.

In order to extract the amplitude and frequency of the vibration, another multiple-distance-measurement technique called 'slip measurement window with fixed start point' is used, as shown in Fig.2. In Eq. (3), if t_0 is fixed, the

measurement window size is enlarged one F-P peak for each shift, an oscillation of a set of measured R_{meas} values indicates the amplitude and frequency of vibration. This technique is not suitable for distance measurement because there always exists an initial bias term, from t_0 , which cannot be determined accurately in our current system.

5. ABSOLUTE DISTANCE AND VIBRATION MEASUREMENT

The typical measurement residual versus the distance measurement number in one scan using the above technique is shown in Fig.3(a), where the scanning rate was 0.5 nm/s and the sampling rate was 125 kS/s. Measured distances minus their average value for 10 sequential scans are plotted versus number of measurements (N_{meas}) per scan in Fig.3(b). The standard deviations (RMS) of distance measurements for 10 sequential scans are plotted versus number of measurements (N_{meas}) per scan in Fig.3(c). It can be seen that the distance errors decrease with an increase of N_{meas} . The RMS of measured distances for 10 sequential scans is $1.6 \mu m$ if there is only one distance measurement per scan ($N_{meas} = 1$). If $N_{meas} = 1200$ and the average value of 1200 distance measurements in each scan is considered as the final measured distance of the scan, the RMS of the final measured distances for 10 scans is 41 nm for the distance of $449828.965 \mu m$, the relative distance measurement precision is 91 ppb.

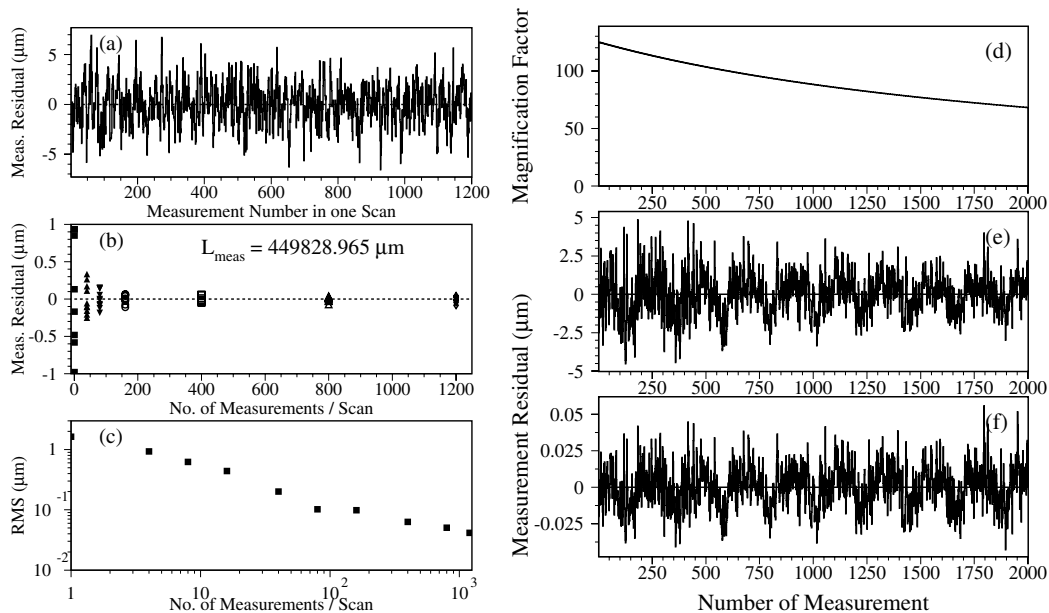


Figure 3: Distance measurement residual spreads versus number of distance measurement N_{meas} (a) for one typical scan, (b) for 10 sequential scans, (c) is the standard deviation of distance measurements for 10 sequential scans versus N_{meas} . The frequency and amplitude of the controlled vibration source are 1 Hz and 9.5 nanometers, (d) Magnification factor versus number of distance measurements, (e) Distance measurement residual versus number of distance measurements, (f) Corrected measurement residual versus number of distance measurements.

The standard deviation (RMS) of measured distances for 10 sequential scans is approximately $1.5 \mu m$ if there is only one distance measurement per scan for closed box data. By using the multiple-distance-measurement technique, the distance measurement precisions for various closed box data with distances ranging from 10 cm to 70 cm collected in the past year are improved significantly; precisions of approximately 50 nanometers are demonstrated under laboratory conditions, as shown in Table 1. All measured precisions listed in Table 1. are the RMS's of measured distances for 10 sequential scans. Two FSI demonstration systems, 'air FSI' and 'optical fiber FSI', are constructed for extensive tests of multiple-distance-measurement technique, 'air FSI' means FSI with the laser beam transported entirely in the ambient atmosphere, 'optical fiber FSI' represents FSI with the laser beam delivered to the interferometer and received back by single-mode optical fibers.

Distance (cm)	Precision(μm)		Scanning Rate (nm/s)	FSI System (Optical Fiber or Air)
	open box	closed box		
10.385107	1.1	0.019	2.0	Optical Fiber FSI
10.385105	1.0	0.035	0.5	Optical Fiber FSI
20.555075	-	0.036, 0.032	0.8	Optical Fiber FSI
20.555071	-	0.045, 0.028	0.4	Optical Fiber FSI
41.025870	4.4	0.056, 0.053	0.4	Optical Fiber FSI
44.982897	-	0.041	0.5	Optical Fiber FSI
61.405952	-	0.051	0.25	Optical Fiber FSI
65.557072	3.9, 4.7	-	0.5	Air FSI
70.645160	-	0.030, 0.034, 0.047	0.5	Air FSI

Table I: Distance measurement precisions for various setups using the multiple-distance-measurement technique.

Based on our studies, the slow fluctuations are reduced to a negligible level by using the plastic box and PVC pipes to suppress temperature fluctuations. The dominant error comes from the uncertainties of the interference fringes number determination; the fringes uncertainties are uncorrelated for multiple distance measurements. In this case, averaging multiple distance measurements in one scan provides a similar precision improvement to averaging distance measurements from multiple independent scans. But, for open box data, the slow fluctuations are dominant, on the order of few microns in our laboratory. The measurement precisions for single and multiple distance open-box measurements are comparable, which indicates that the slow fluctuations cannot be adequately suppressed by using the multiple-distance-measurement technique. A dual-laser FSI system[6] intended to cancel the drift error is currently under study in our laboratory .

In order to test the vibration measurement technique, a piezoelectric transducer (PZT) was employed to produce vibrations of the retroreflector. For instance, the frequency of the controlled vibration source was set to 1.01 ± 0.01 Hz with amplitude 9.5 ± 1.5 nanometers. The magnification factors, distance measurement residuals and corrected measurement residuals for 2000 measurements in one scan are shown in Fig.3(d), Fig.3(e) and Fig.3(f), respectively. The extracted vibration frequencies and amplitudes using this technique, $f_{vib} = 1.025 \pm 0.002$ Hz, $A_{vib} = 9.3 \pm 0.3$ nanometers, agree well with the expectation values.

In addition, vibration frequencies at 0.1, 0.5, 1.0, 5, 10, 20, 50, 100 Hz with controlled vibration amplitudes ranging from 9.5 nanometers to 400 nanometers were studied extensively using our current FSI system. The measured vibrations and expected vibrations all agree well within the 10-15% level for amplitudes, 1-2% for frequencies, where we are limited by uncertainties in the expectations. Vibration frequencies far below 0.1 Hz can be regarded as slow fluctuations, which cannot be suppressed by the above analysis techniques.

Detailed information about estimation of major error sources for the absolute distance measurement and limitation of our current FSI system is provided elsewhere[5].

6. DUAL-LASER FSI SYSTEM

A dual-laser FSI system has been built in order to reduce drift error and slow fluctuations occurring during the laser scan. Two lasers are operating simultaneously, the two laser beams are coupled into one optical fiber but isolated by using two choppers. The principle of the dual-laser technique is shown in the following. For the first laser, the measured distance $D_1 = D_{true} + \Omega_1 \times \epsilon_1$, and ϵ is drift error during the laser scanning. For the second laser, the measured distance $D_2 = D_{true} + \Omega_2 \times \epsilon_2$. Since the two laser beams travel the same optical path during the same period, the drift errors ϵ_1 and ϵ_2 should be very comparable. Under this assumption, the true distance can be extracted using the formula $D_{true} = (D_2 - \rho \times D_1)/(1 - \rho)$, where, $\rho = \Omega_2/\Omega_1$, the ratio of magnification factors from two lasers.

The laser beams are isolated by choppers periodically, so only half the fringes are recorded for each laser, degrading the distance measurement precision. Missing fringes during chopped intervals for each laser must be recovered through robust interpolation algorithms. The chopper edge transitions make this interpolation difficult. Several techniques are under study.

7. A POSSIBLE SILICON TRACKER ALIGNMENT SYSTEM

One possible silicon tracker alignment system is shown in Fig.4. The left plot shows lines of sight for alignment in R-Z plane of the tracker barrel, the middle plot for alignment in X-Y plane of the tracker barrel, the right plot for alignment in the tracker forward region. Red lines/dots show the point-to-point distances need to be measured using FSIs. There are 752 point-to-point distance measurements in total for the alignment system. More studies are needed to optimize the distance measurements grid.

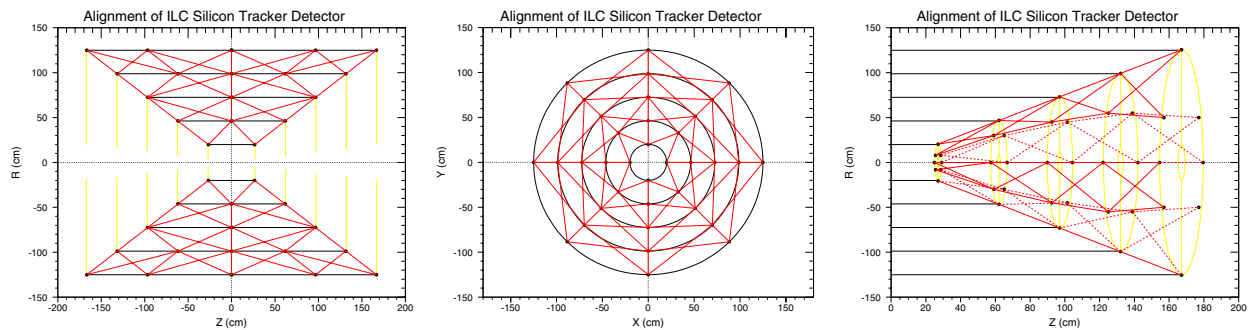


Figure 4: A Possible SiLC Tracker Alignment System.

Acknowledgments

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