MINIMIZING THE ENERGY SPREAD WITHIN A SINGLE BUNCH BY SHAPING ITS CHARGE DISTRIBUTION

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Introduction

When electrons or positrons in a bunch pass through the periodic structure of a linear accelerator, they leave behind them energy in the form of longitudinal wake fields. The wakefields thus induced by early particles in a bunch offset the energy of later particles. For a linear collider, the energy spread introduced within the bunches by this beam loading effect must be minimized because it limits the degree to which the particles can be focused to a small spot due to chromatic effects in the final focus system. For example, for the SLC, the maximum allowable energy spread is ±0.5%.

It has been known for some time that partial compensation of the longitudinal wake field effects can be obtained for any bunch by placing it ahead of the accelerating crest (in space), thereby letting the positive rising sinusoidal field offset the negative beam loading field. The work presented in this paper shows that it is possible to obtain complete compensation, i.e., to reduce the energy spread essentially to zero by properly shaping the longitudinal charge distribution of the bunch and by placing it at the correct position on the wave.

Optimizing the Bunch Shape

The energy gained by a single particle riding at an angle θ1 with respect to the crest of a traveling wave of accelerating gradient E0 over a length L is

\[ V = E_0 L \cos \theta_1 \, . \]  

(1)

In the case of a bunch consisting of many particles, this energy is modified by the presence of the wake fields left by particles ahead of θ1. For the examples worked out in this paper, we will use the SLAC constant-gradient structure although the technique should be applicable to any structure for which the longitudinal wake function is known. This wake function, \( w_L(\theta) \), is defined as the voltage excited by a unit charge traversing the structure. It is shown in Fig. 1 as calculated for a single average cavity of length \( d (d = 3.5 \text{ cm}) \) of the SLAC constant-gradient structure. At the cost of an error estimated to be on the order of 5%, we can neglect the fact that the actual cavities differ in iris diameter from this average cavity by about ±15%. We can then obtain the function \( w_L \) for the entire accelerator by simply multiplying \( w_L(\theta) \) by \( N \), the number of cavities (L/d).

With these definitions and a bunch charge distribution \( f(\theta') \) as illustrated in Fig. 2, Eq. (1) now becomes:

\[ V(\theta_1) = V_0 \cos \theta_1 - \int_0^{(\theta_0-\theta_1)} f(\theta') w_L(\theta_0 - \theta_1 - \theta') d\theta' \]  

(2)

where \( V_0 = E_0 L \), \( \theta_0 \) is the position of the head of the bunch with respect to the wave and \( \theta' \), the coordinate within the bunch, is made to vary from 0 (the head of the bunch) to \( \theta_0 - \theta_1 \) (the position where we want to know the net energy).

In order to reduce the energy spread within the bunch to zero, we must make \( V(\theta_1) \) independent of \( \theta_1 \). This requires that

\[ \frac{\partial V(\theta_1)}{\partial \theta_1} = 0 \, . \]  

(3)

By taking the partial derivative of Eq. (2) with respect to \( \theta_1 \) and setting it to zero, we get:

\[ -V_0 \sin \theta_1 - \int_0^{(\theta_0-\theta_1)} f(\theta') \frac{\partial w_L}{\partial \theta_1}(\theta_0 - \theta_1 - \theta') d\theta' + f(\theta_0 - \theta_1) W_L(0) = 0 \, . \]
or
\[
f(\theta_0 - \theta_1) = \frac{V_0}{W_L(0)} \sin \theta_1 + \int_0^{(\theta_0 - \theta_1)} \frac{f(\theta')}{W_L(0)} \frac{W_L'(0)}{W_L(0)} d\theta'.
\]

Letting \( \theta_0 - \theta_1 = x \) where \( x \geq \theta' \), Eq. (4) becomes:
\[
f(x) = \frac{V_0}{W_L(0)} \sin(\theta_0 - x) - \int_0^x \frac{W_L'(x - \theta')}{W_L(0)} f(\theta') d\theta' \tag{5}
\]

which is a Volterra integral equation of the second kind. This equation can be solved digitally through a multi-step method using Day's starting procedure in conjunction with Simpson's rule and the three-eighths rule. This wake function can be fitted with a polynomial so as to be represented by an analytical expression.

Figures 3 and 4 give results for several examples. These examples were all worked out for a no-load energy \( V_0 \) of 54.75 GeV, an accelerator length \( L \) of 960 sections, each with 86 cavities (i.e., \( L = 2890 \text{ m} \), \( N = 82,560 \) cavities) and a bunch of integrated charge \( 5 \times 10^{10} \) e. The value of \( V_0 \) was chosen so as to yield a final beam energy just over 50 GeV. Figure 3 shows six different bunch shapes with the corresponding \( \theta_0 \)'s (positions of the head with respect to the wave) required to give essentially zero energy spread. The head of the bunch is on the left (zero-absissa) and the tail defined as the point where an integrated charge of \( 5 \times 10^{10} \) e is reached, is at the abscissa corresponding to the letter "T" on each curve. An interesting aspect of these curves is that if the bunches are extended beyond the "T" points as shown, the energy spread continues to be zero even though the charge in the extended bunch is greater than \( 5 \times 10^{10} \) e.

Table 1 gives a summary of the average energies \( \langle E \rangle \) and spectral qualities \( \langle (E_{\text{max}} - E_{\text{min}})/\langle E \rangle \rangle \) and the fractional standard deviation \( \sigma_E/\langle E \rangle \) for the cases shown in Figs. 3 and 4.

<table>
<thead>
<tr>
<th>( \theta_0 ) (degrees)</th>
<th>( E ) (GeV)</th>
<th>( (E_{\text{max}} - E_{\text{min}})/\langle E \rangle ) (%)</th>
<th>( \sigma_E/\langle E \rangle ) (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>26</td>
<td>49.210</td>
<td>0.008</td>
<td>0.003</td>
</tr>
<tr>
<td>23</td>
<td>50.399</td>
<td>0.009</td>
<td>0.003</td>
</tr>
<tr>
<td>20</td>
<td>51.450</td>
<td>0.010</td>
<td>0.003</td>
</tr>
<tr>
<td>17</td>
<td>52.360</td>
<td>0.014</td>
<td>0.004</td>
</tr>
<tr>
<td>15.5</td>
<td>52.755</td>
<td>0.010</td>
<td>0.004</td>
</tr>
<tr>
<td>Trimmed Gaussian</td>
<td>52.809</td>
<td>0.14</td>
<td>0.038</td>
</tr>
<tr>
<td>Gaussian (( \delta ))</td>
<td>52.795</td>
<td>3.5</td>
<td>0.352</td>
</tr>
</tbody>
</table>

The sixth example, shown also for \( \theta_0 = 15.5^\circ \), is that of a trimmed Gaussian fitted to the shape of the "ideal" \( \theta_0 = 15.5^\circ \) case. It has a \( \delta \) of 0° but is truncated at \( \pm 7.5^\circ \). These results all compare extremely favorably with the energy spread \( \sigma_E/\langle E \rangle \) of 0.35% which one obtains for a Gaussian bunch of \( 5 \times 10^{10} \) e with a length \( 6 \sigma_z \), a \( \sigma_z \) of 4° and a \( \theta_0 \) of 20° (the seventh example in Table 1), or for that matter, for the same bunch with charge reduced to \( 5 \times 10^{9} \) e. The energy spectra for all the above cases are illustrated in Fig. 5. Note that the examples of Table 1 are so narrow in energy that they can only be represented by a line.

**Discussion**

If we rewrite Eq. (5) in terms of the gradient \( E_0 \) instead of the total energy \( V_0 \), it becomes:
\[
f(x) = \frac{E_d}{w_L(\theta)} \sin(\theta_0 - x) - \int_0^x \frac{w_L'(x - \theta')}{w_L(\theta)} f(\theta') d\theta'.
\]

We see that for a structure with a given \( w_L(\theta) \), once the gradient \( E_0 \) and the angular position \( \theta_0 \) of the head are chosen, the shape is fixed by Eq. (6) and is independent of the total energy \( V_0 \) and length \( L \). For a given gradient \( E_0 \), \( f(\theta) \) starts at a higher value as \( \theta_0 \) is made larger since...
The variations of $\sigma_E/E$ in both tables are close to hyperbolic.

**Conclusions**

We have shown in this paper that it is theoretically possible to find bunch shapes for the SLC which yield $5 \times 10^{10}$ or more particles within negligible energy spread at the end of the linear accelerator. As it turns out, these shapes depend only on the linac energy gradient and the angle at which the head of the bunch is placed with respect to the accelerating wave, and are independent of the total energy or length of the accelerator. Excursions away from this angle in parts of the linac, designed to cause Landau damping of the transverse wake field effect, are of course permissible as long as overall "phase closure" to preserve the desired average $\theta_0$ is accomplished. Some of these theoretical bunch shapes are not too different from shapes that ought to be realizable from injectors or damping rings. How to realize them exactly is not the subject of this paper.

**References**

1. See for example, SLAC Linear Collider, Conceptual Design Report, SLAC-229, pp. 17 and 117.
2. Ibid, pp. 112-116.