



## EXCITATION SYSTEM IMPLEMENTATION

The digital functions are implemented on a commercial FPGA hardware fixture originally designed for frequency-domain characterization of D/A circuits[4]. We use this hardware platform with our own FPGA codes and additional synchronization inputs to implement the sequencer[5], with the Maxim 19693 D/A converter evaluation board for the fast analog output.

The system includes a synchronized master oscillator and a digital FPGA sequencer with turn and injection fiducial signals from the SPS timing system. The SPS RF clock (nominally 200 MHz) is multiplied via a step-recovery-diode harmonic converter to generate a  $n \times 200$  MHz system clock which is filtered by a tunable bandpass filter to select the operating harmonic. For  $n = 10$  the 2 GHz signal results in a 4 GS/sec. data rate, though any harmonic can be used, and for ease of synchronization in these measurements the  $n = 8$  harmonic is used, which generates a 3.2 GS/sec. data stream. During the SPS acceleration cycle the RF frequency changes by several kHz, and this multiplier technique keeps the digital clocks in phase synchronism with the circulating beam. A fast turn fiducial identifies the beginning of each turn, so that the logic of the system can count RF buckets and identify particular bunches (the SPS typically fills bunch trains on a 40 MHz or 5 RF bucket pattern), while an injection fiducial provides a means to synchronize the 15,000 turn data sequence to the accelerating

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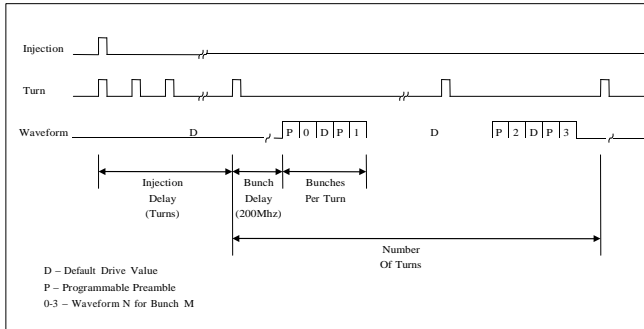


Figure 2: Timing diagram showing the injection trigger, turn fiducial and excitation. A programmable holdoff delay in turns allows positioning of the excitation at arbitrary points in the acceleration cycle, while the sequencer uses the RF clock to count buckets and position the excitation signal on the selected bunches.

## POWER AMPLIFIER ARRAY

The excitation signal needs to be converted to a differential set of paired signals to drive a 4 element stripline kicker. A set of low-power hybrids is used to generate 0 and 180 degree signal pairs, these are further split with in-phase power dividers to generate the 4 paired excitation drive signals. Four 80 W 20-1000 MHz amplifiers drive the individual stripline electrodes, each with a high-power

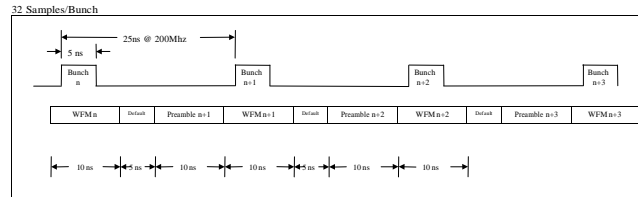


Figure 3: Timing detail of a single turn with several bunches, and the sequence of preamble, WFM data which is applied to the target bunch(es). The excitation memory is 512K, allowing up to 15,000 unique turns with 32 samples per bunch.

termination. These wideband amplifiers are commercial products[6] intended for communications purposes, but for our purpose the time response of the amplifiers is quite important. The amplifier is a multi-stage design with both type A and type AB stages, and in our testing we worked with the manufacturer to increase the output stage bias to improve the transient response, though with the concomitant derating of the amplifier power to 80 W. Figure 4 shows the frequency response of the modified amplifier, while Figure 5 shows the time-domain input and output signals for a 1 cycle 500 MHz RF signal. The amplifiers are packaged with power supplies, cooling, and a dual directional coupler to monitor the forward and reverse RF power. A diode detector and level comparator circuit is implemented to trip off the RF drive if excessive reverse power is sensed (such as from a damaged termination).

In the SPS installation the amplifiers and low-power phasing/splitting networks are placed in the accelerator tunnel to avoid cable power loss and dispersive effects. To control and monitor the amplifiers a simple hardware interface allows via opto-coupled logic signals remote on/off of each amplifier, sensing of any amplifier trip, reset of tripped amplifiers, and measurement of the temperature of each amplifier assembly. A general purpose RF multiplexer allows 1 of 4 signals (such as amplifier coupler signals, beam induced signals, etc.) to be sent back to the control room for study. This simple interface requires 2 high-bandwidth cables in conjunction with low-bandwidth twisted pairs, and allows external operation and verification of state of the drive system. For these initial experiments an existing exponential tapered pickup electrode array has been used as a kicker, though the response of this structure is rolling off above 200 MHz.[7] A high-bandwidth kicker system is in design for fabrication and installation in a future SPS shutdown[8].

## OPERATION AT THE SPS

The FPGA system is configured and controlled via a USB interface from a host PC, which allows the core gate array configuration to be loaded. Software GUI tools allow the selection of a particular bunch to drive, the synchronization method, the specification of the type of excitation,

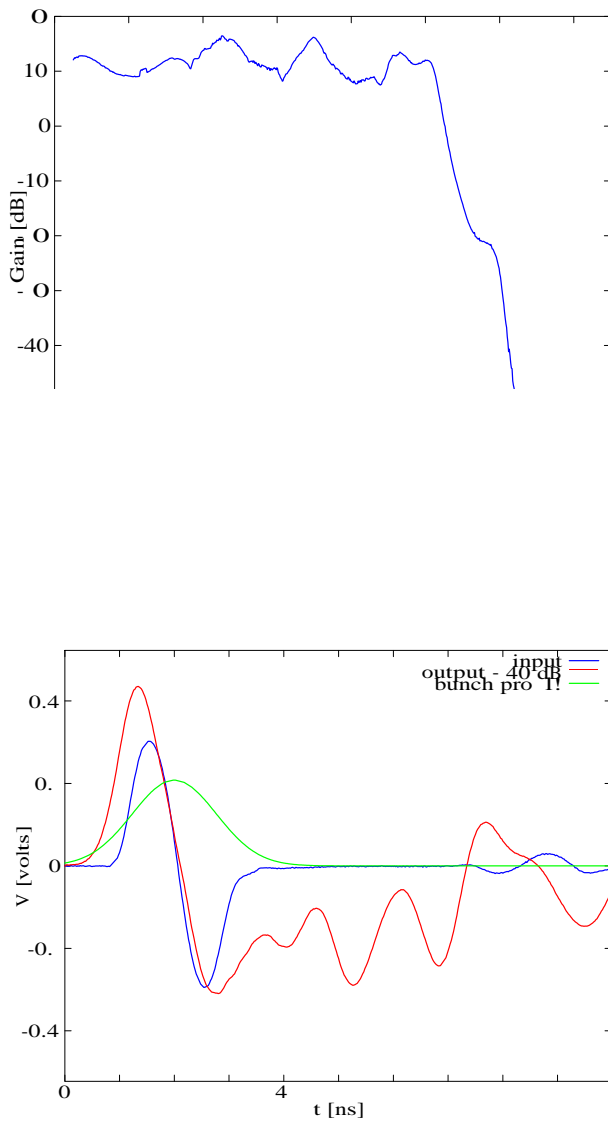


Figure 5: Time domain signals for a 500 Mhz single-cycle burst, with a 2 ns gaussian bunch shown for time scale. The amplifier response has significant ringing, but in this application the majority of the kick signal applied to the bunch is free from the ringing response.

etc. The system supports the use of frequency chirps and random noise bursts in addition to steady-state narrowband excitations targeted to a single mode.

The phasing adjustment of the 16/32 sample output burst relative to the passage of the selected bunch in the kicker is critical. To excite barycentric (mode zero) motion, all the individual samples in the burst are in phase, though the kick waveform is amplitude modulated at the betatron frequency over the turn sequence. To excite mode 1 (head-tail) motion the individual drive signals are calculated to drive head and tail oppositely (again the entire waveform is amplitude modulated at the betatron tune  $\pm$  synchrotron tune). However, if a mode zero (barycentric) chirp signal is slightly mis-phased, so that it only overlaps the begin-

ning or the end of the bunch, a higher-frequency mode with head tail differential motion can be excited. As the bunch is roughly 2 ns long, this requires careful timing on the sub-nanosecond level for consistent and repeatable mode-specific excitation at full amplitude.

## SUMMARY

This system was installed in the SPS in July 2011, and has been used to study the beam motion in August, November 2011 and April 2012. Even with the limited bandwidth kicker, we are able to selectively excite up through mode 4. To date these measurements have served to verify the response of the beam against theoretical expectations, and we are now preparing to study as we increase the beam current, and go to multiple bunch trains. With these conditions the system dynamics from Ecloud and TMCI effects will start to be evident via the beam response measurements. This excitation system with associated beam motion sampling then becomes a beam diagnostic, capable of measuring small tune shifts in parts of the beam. The system development is also a vital test-bed to prove system functions for a future feedback system.

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