

# Crab crossing and crab waist at super KEKB

K. Ohmi (KEK)  
Super B workshop at SLAC  
15-17, June 2006

Thanks, M. Biagini, Y. Funakoshi, Y. Ohnishi, K.Oide,  
E. Perevedentsev, P. Raimondi, M Zobov

# Super bunch approach

K. Takayama et al, PRL, (LHC)

F. Ruggiero, F. Zimmermann (LHC)

P. Raimondi et al, (super B)

Short bunch

$$\frac{\sqrt{\varepsilon_x \beta_x}}{\theta \sigma_z} > 1$$

$$L \sim \frac{N^2}{\sqrt{\varepsilon_x \beta_x \varepsilon_y \beta_y}}$$

$$\xi_x \sim \frac{N}{\varepsilon_x}$$

$$\xi_y \sim N \sqrt{\frac{\beta_y}{\varepsilon_x \beta_x \varepsilon_y}}$$

$$\beta_y > \sigma_z$$

$$\times \frac{\sqrt{\varepsilon_x \beta_x}}{\theta \sigma_z} (< 1)$$

Overlap factor

Long bunch

$$L \sim \frac{N^2}{\theta \sigma_z \sqrt{\varepsilon_y \beta_y}}$$

$$\xi_x \sim \frac{N}{\theta \sigma_z} \sqrt{\frac{\beta_x}{\varepsilon_x}}$$

$$\xi_y \sim \frac{N}{\theta \sigma_z} \sqrt{\frac{\beta_y}{\varepsilon_y}}$$

$$\beta_y > \frac{\sqrt{\varepsilon_x \beta_x}}{\theta}$$

$\xi_x$  is smaller due to cancellation of tune shift along bunch length

# Essentials of super bunch scheme

$$L \sim \frac{N^2}{\theta \sigma_z \sqrt{\varepsilon_y \beta_y}}$$

$$\xi_x \sim \frac{N}{\theta \sigma_z} \sqrt{\frac{\beta_x}{\varepsilon_x}}$$

$$\xi_y \sim \frac{N}{\theta \sigma_z} \sqrt{\frac{\beta_y}{\varepsilon_y}}$$

$$\beta_y > \frac{\sqrt{\varepsilon_x \beta_x}}{\theta}$$

Keep  $\sqrt{\frac{\beta_y}{\varepsilon_y}}$ ,  $\sqrt{\frac{\beta_x}{\varepsilon_x}}$  and  $\frac{\sqrt{\varepsilon_x \beta_x}}{\beta_y}$ .

$$\varepsilon_y \beta_y \rightarrow 0$$

$$L \rightarrow \infty$$

- Bunch length is free.
- Small beta and small emittance are required.

# Short bunch scheme

$$L \sim \frac{N^2}{\sqrt{\varepsilon_x \beta_x \varepsilon_y \beta_y}}$$

$$\xi_x \sim \frac{N}{\varepsilon_x}$$

$$\xi_y \sim N \sqrt{\frac{\beta_y}{\varepsilon_x \beta_x \varepsilon_y}}$$

$$\beta_y > \sigma_z$$

Keep  $\varepsilon_x$ ,  $\beta_x$  and  $\sqrt{\frac{\beta_y}{\varepsilon_y}}$ .  
 $\varepsilon_y \beta_y \rightarrow 0$

$$L \rightarrow \infty$$

- Small coupling
- Short bunch
- Another approach: Operating point closed to half integer

$$v_x \rightarrow +0.5 \quad \xi_y \rightarrow \infty \quad L \rightarrow \infty$$

We need  $L=10^{36} \text{ cm}^{-2}\text{s}^{-1}$

- Not infinity.
- Which approach is better?
- Application of lattice nonlinear force
- Traveling waist, crab waist

# Nonlinear map at collision point

$$H = a_i x_i + b_{ij} x_i x_j + c_{ijk} x_i x_j x_k$$

$$\mathbf{x} = x_i = (x, p_x, y, p_y, z, \delta (= \Delta E / E))$$

$$\begin{aligned} M = \exp(- : H :) \mathbf{x}^* &= \mathbf{x} - [H, \mathbf{x}] + \frac{1}{2} [H, [H, \mathbf{x}]] + \dots \\ &= a_i + b_{ij} x_j + c'_{ijk} x_j x_k + \dots \end{aligned}$$

- 1<sup>st</sup> orbit
- 2<sup>nd</sup> tune, beta, crossing angle
- 3<sup>rd</sup> chromaticity, transverse nonlinearity. z-dependent chromaticity is now focused.

# Waist control-I traveling focus

$$\mathbf{M} = e^{-:H_I:} \mathbf{M}_0 e{:H_I:}$$

$$H_I = ap_y^2 z$$

$$\bar{y} = y + \frac{\partial H_I}{\partial P_y} = y + azP_y \qquad \bar{\delta} = \delta - \frac{\partial H}{\partial z} = \delta - ap_y^2$$

- Linear part for y. z is constant during collision.

$$\begin{pmatrix} \bar{\beta} & -\bar{\alpha} \\ -\bar{\alpha} & \bar{\gamma} \end{pmatrix} = T \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix} T^t = \begin{pmatrix} \beta + \frac{a^2 z^2}{\beta} & \frac{az}{\beta} \\ \frac{az}{\beta} & \frac{1}{\beta} \end{pmatrix} \qquad \alpha=0$$

$$T = \begin{pmatrix} 1 & az \\ 0 & 1 \end{pmatrix}$$

# Waist position for given z

- Variation for s

$$M(s) \begin{pmatrix} \beta + \frac{a^2 z^2}{\beta} & \frac{az}{\beta} \\ \frac{az}{\beta} & \frac{1}{\beta} \end{pmatrix} M^t(s) = \begin{pmatrix} \beta + \frac{(s+az)^2}{\beta} & \frac{s+az}{\beta} \\ \frac{s+az}{\beta} & \frac{1}{\beta} \end{pmatrix}$$

- Minimum  $\beta$  is shifted  $s=-az$



# Realistic example- I

- Collision point of a part of bunch with  $z$ ,  $\langle s \rangle = z/2$ .
- To minimize  $\beta$  at  $s=z/2$ ,  $a=-1/2$
- Required H

$$H_I = -\frac{1}{2} p_y^2 z$$

- RFQ TM210

- $$V = \frac{1}{2\beta^* \beta} \frac{c^2}{\omega^2} \frac{pc}{e}$$

V~10 MV or more

# Waist control-II crab waist (P. Raimondi et al.)

$$\mathbf{M} = e^{-:H_I:} \mathbf{M}_0 e^{:H_I:}$$

$$H_I = axp_y^2$$

$$\bar{y} = y + \frac{\partial H_I}{\partial P_y} = y + axP_y \quad \bar{p}_x = p_x - \frac{\partial H}{\partial x} = p_x - ap_y^2$$

- Take linear part for y, since x is constant during collision.

$$\begin{pmatrix} \bar{\beta} & -\bar{\alpha} \\ -\bar{\alpha} & \bar{\gamma} \end{pmatrix} = T \begin{pmatrix} \beta & -\alpha \\ -\alpha & \gamma \end{pmatrix} T^t = \begin{pmatrix} \beta + \frac{a^2 x^2}{\beta} & \frac{ax}{\beta} \\ \frac{ax}{\beta} & \frac{1}{\beta} \end{pmatrix}$$

$$T = \begin{pmatrix} 1 & ax \\ 0 & 1 \end{pmatrix}$$

# Waist position for given x

- Variation for s

$$M(s) \begin{pmatrix} \beta + \frac{a^2 x^2}{\beta} & \frac{ax}{\beta} \\ \frac{ax}{\beta} & \frac{1}{\beta} \end{pmatrix} M^t(s) = \begin{pmatrix} \beta + \frac{(s+ax)^2}{\beta} & \frac{s+ax}{\beta} \\ \frac{s+ax}{\beta} & \frac{1}{\beta} \end{pmatrix}$$

- Minimum  $\beta$  is shifted to  $s=-ax$

# Realistic example- II

- To complete the crab waist,  $a=1/\theta$ , where  $\theta$  is full crossing angle.
- Required H

$$H_I = \frac{1}{\theta} x p_y^2$$

- Sextupole strength

$$K_2 = \frac{1}{2} \frac{B'' L}{p/e} \approx \frac{1}{\theta} \frac{1}{\beta_y^* \beta_y} \sqrt{\frac{\beta_x^*}{\beta_x}} \quad K_2 \sim 30-50$$

Not very strong

# Crabbing beam in sextupole

- Crabbing beam in sextupole can give the nonlinear component at IP
- Traveling waist is realized at IP.

$$H_I = ap_y^2 z$$

$$z^* = \sqrt{\frac{\beta(s)}{\beta^*}} \zeta(s) x(s)$$

$$K_2 = \frac{1}{2} \frac{B'' L}{p/e} \approx \frac{1}{\theta} \frac{1}{\beta_y^* \beta_y} \sqrt{\frac{\beta_x^*}{\beta_x}} \quad K_2 \sim 30-50$$

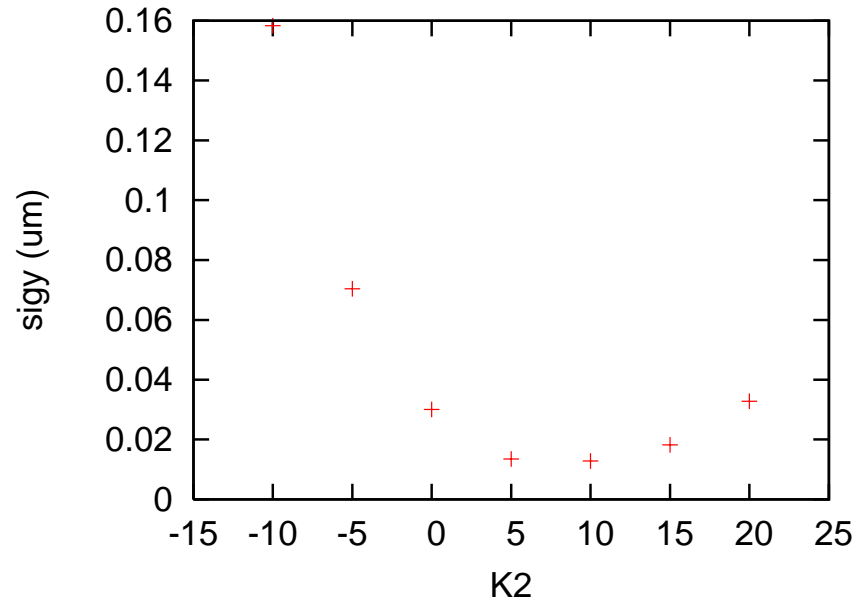
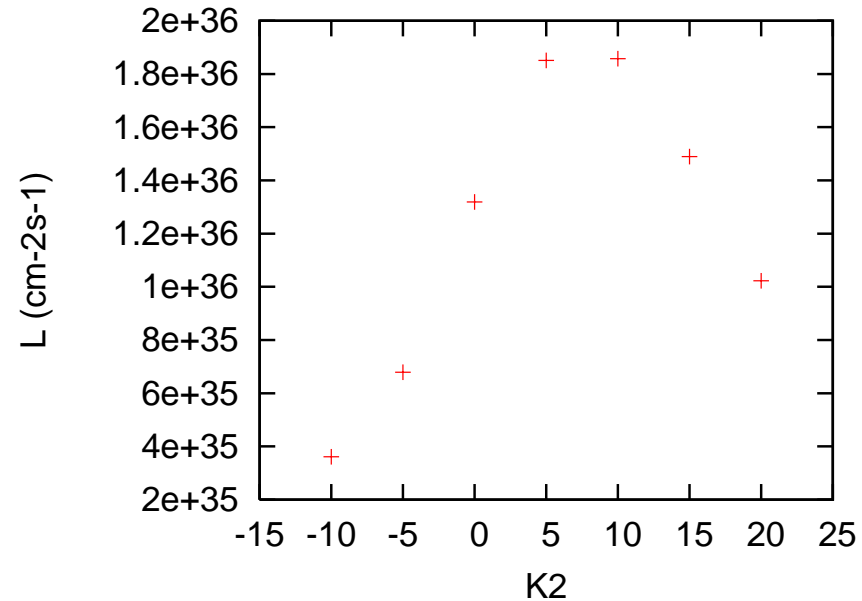
# Super B (LNF-SLAC)

	Base	PEP-III
C	3016	2200
$\epsilon_X$	4.00E-10	2.00E-08
$\epsilon_Y$	2.00E-12	2.00E-10
$\beta_X$ (mm)	17.8	10
$\beta_Y$ (mm)	0.08	0.8
$\sigma_Z$ (mm)	4	10
ne	2.00E+10	3.00E+10
np	4.40E+10	9.00E+10
$\phi/2$ (mrad)	25	14
$\xi_X$	0.0025	
$\xi_Y$	0.1	

$$\xi_y = \int_{-\infty}^{\infty} \frac{\partial F_y}{\partial y} \Big|_{x=\phi z} \rho(z) \delta(s + z/2) dz ds$$

# Luminosity for the super B

- Luminosity and vertical beam size as functions of K2
- $L > 1e36$  is achieved in this weak-strong simulation.



# DAFNE upgrade

	DAFNE
C	97.7
$\epsilon_x$	3.00E-07
$\epsilon_y$	1.50E-09
$\beta_x$ (mm)	133
$\beta_y$ (mm)	6.5
$\sigma_z$ (mm)	15
ne	1.00E+11
np	1.00E+11
$\phi/2$ (mrad)	25
$\xi_x$	0.033
$\xi_y$	0.2479



# Luminosity for new DAFNE

- $L$  ( $\times 10^{33}$ ) given by the weak-strong simulation
- Small  $v_s$  was essential for high luminosity

ne	tune	vs	L(K2=10)	15	20
6.00E+10	0.53, 0.58	0.012		4.27	3.79
6.00E+10	0.53, 0.58	-0.01		4.35	3.93
1.00E+11	0.53, 0.58	-0.01	4.07	5.66	5.53
6.00E+10	0.53, 0.58	0.012	$\sigma_z=10\text{mm}$	4.32	2.47
6.00E+10	0.53, 0.58	-0.01	$\sigma_z=10\text{mm}$	4.65	2.7
6.00E+10	0.057, 0.097	-0.01		5.19(3.3)	
1.00E+11	0.057, 0.097	-0.01		13.21(4.8)	

() strong-strong , horizontal size blow-up

# Super KEKB

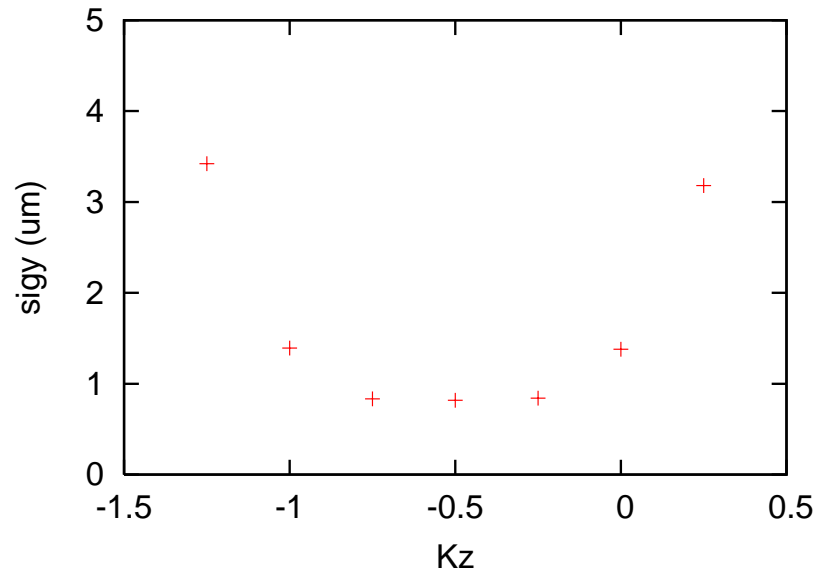
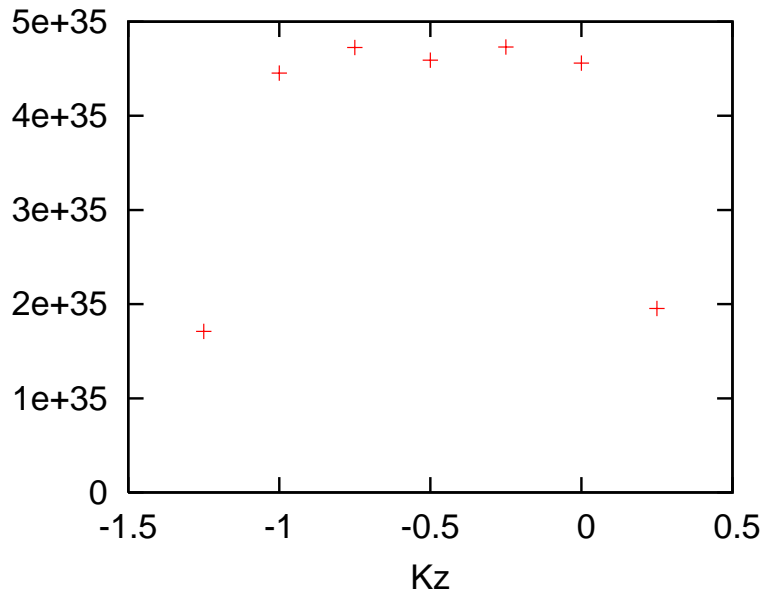
	SuperKEKB	Crab waist			
$\epsilon_x$	9.00E-09	6.00E-09	6.00E-09	6.00E-09	6.00E-09
$\epsilon_y$	4.50E-11	6.00E-11	6.00E-11	6.00E-11	6.00E-11
$\beta_x$ (mm)	200	100	50	100	50
$\beta_y$ (mm)	3	1	0.5	1	0.5
$\sigma_z$ (mm)	3	6	6	4	4
$\nu_s$	0.025	0.01	0.01	0.01	0.01
$n_e$	5.50E+10	5.50E+10	5.50E+10	3.50E+10	3.50E+10
$n_p$	1.26E+11	1.27E+11	1.27E+11	8.00E+10	8.00E+10
$\phi/2$ (mrad)	0	15	15	15	15
$\xi_x$	0.397	0.0418	0.022	0.0547	0.0298
$\xi_y$	0.794->0.24	0.1985	0.179	0.178	0.154
Lum (W.S.)	8E+35	6.70E+35	1.00E+36	3.95E+35	4.80E+35
Lum (S.S.)	8.25E35	4.77E35	9E35	3.94E35	4.27E35

Horizontal blow-up is recovered by choice of tune. (M. Tawada)

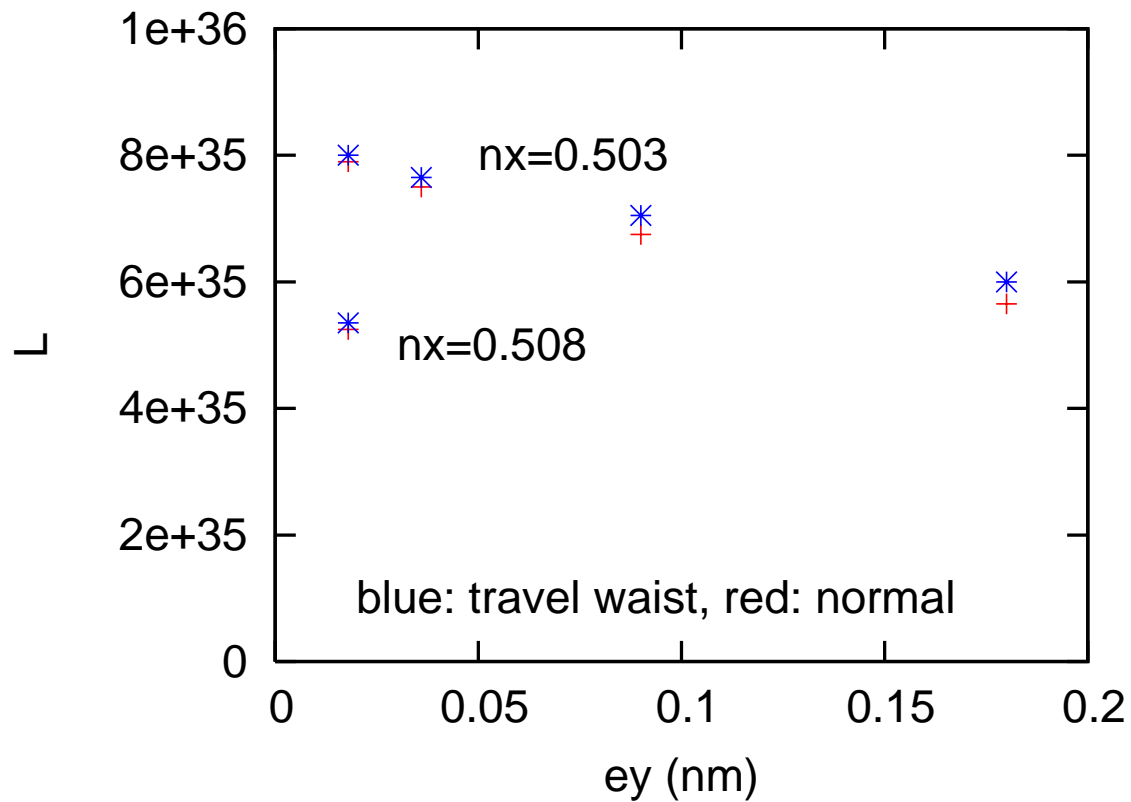
# Traveling waist

- Particles with  $z$  collide with central part of another beam. Hour glass effect still exists for each particles with  $z$ .
- No big gain in Lum.!
- Life time is improved.

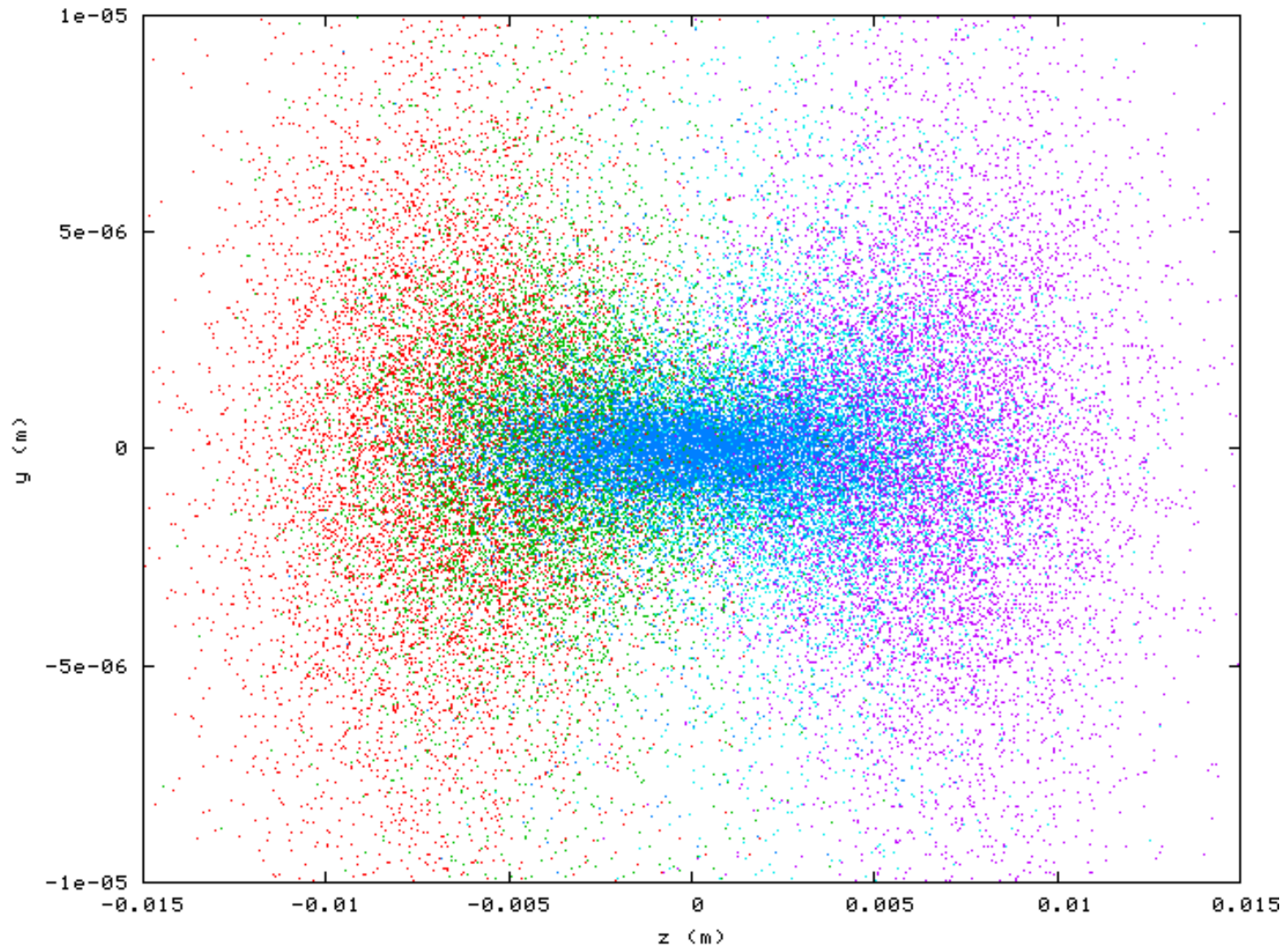
$$\begin{aligned}\varepsilon_x &= 24 \text{ nm} \\ \varepsilon_y &= 0.18 \text{ nm} \quad \beta_x = 0.2 \text{ m} \\ \beta_y &= 1 \text{ mm} \quad \sigma_z = 3 \text{ mm}\end{aligned}$$



# Small coupling



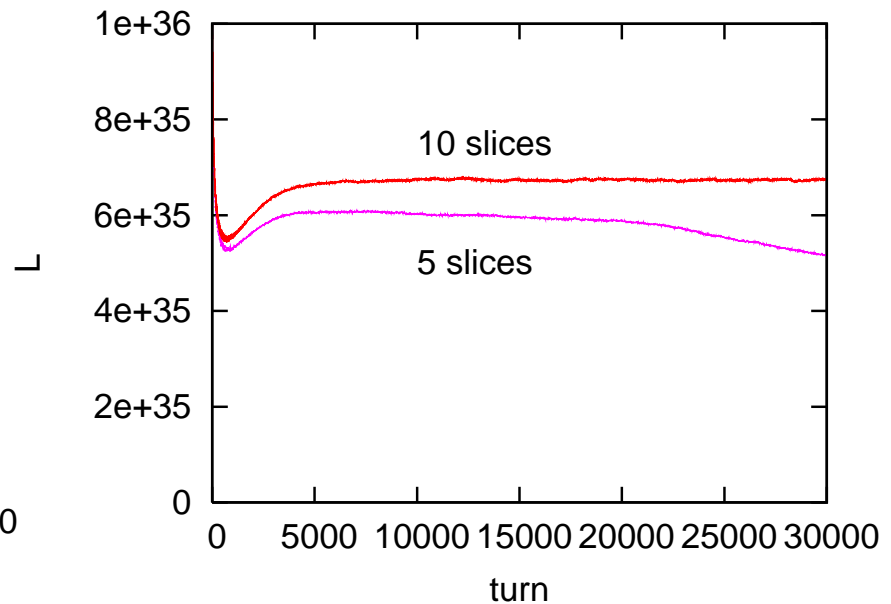
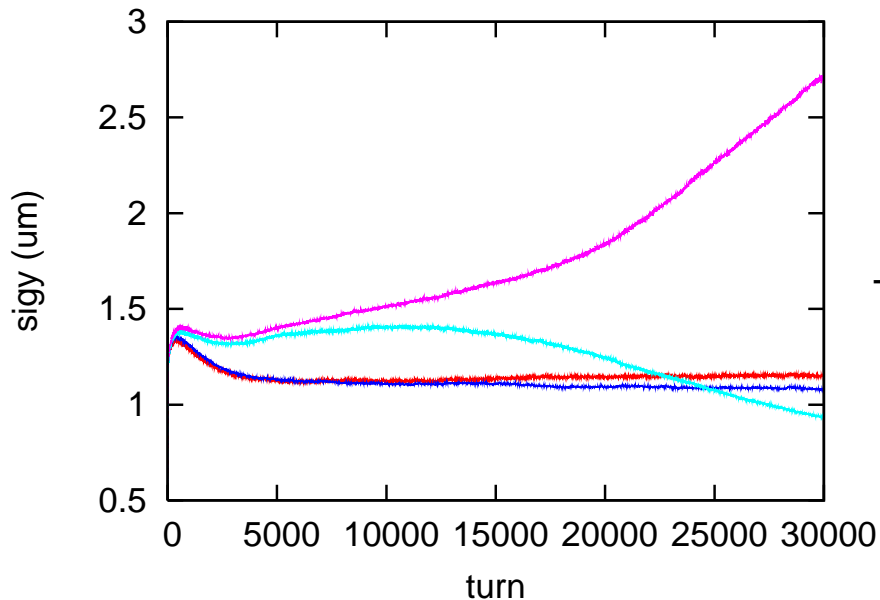
# Traveling of positron beam



# Increase longitudinal slice

$\varepsilon_x=18\text{nm}$ ,  $\varepsilon_y=0.09\text{nm}$ ,  $\beta_x=0.2\text{m}$   $\beta_y=3\text{mm}$   $\sigma_z=3\text{mm}$

Lower coupling becomes to give higher luminosity.



# Why the crab crossing and crab waist improve luminosity?

- Beam-beam limit is caused by an emittance growth due to nonlinear beam-beam interaction.
- Why emittance grows?
- Studies for crab waist is just started.

# Weak-strong model

- 3 degree of freedom
- Periodic system
- Time (s) dependent

$$H(x, p_x, y, p_y, z, p_z; s) = H'(J_1, \varphi_1, J_2, \varphi_2, J_3, \varphi_3; s)$$

$$\varphi(s + L) = \varphi(s) + 2\pi\nu$$



# Solvable system

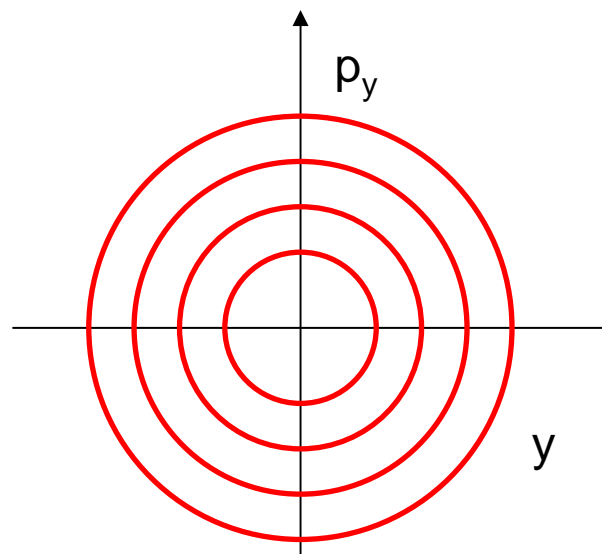
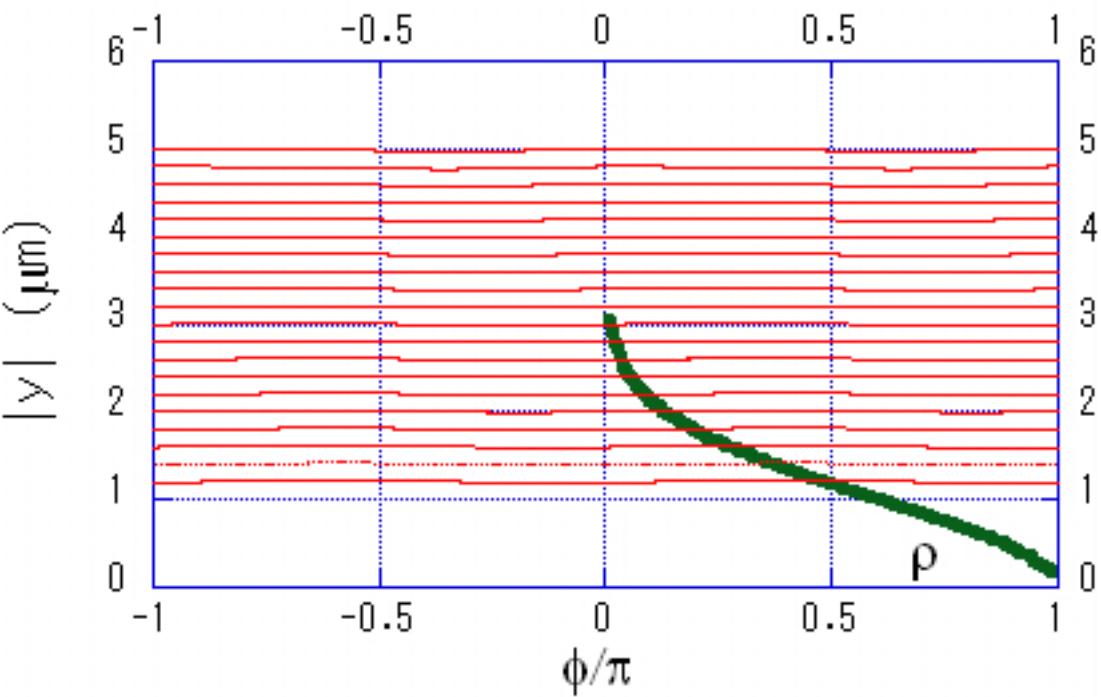
- Exist three J's, where H is only a function of J's, not of  $\varphi$ 's.
- For example, linear system.
- Particles travel along J. J is kept, therefore no emittance growth, except mismatching.

$$\frac{dJ}{ds} = -\frac{\partial H}{\partial \varphi} = 0 \quad J = \text{const}$$

$$\frac{d\varphi}{ds} = \frac{\partial H(J)}{\partial J} \quad \oint d\varphi = 2\pi\nu(J)$$

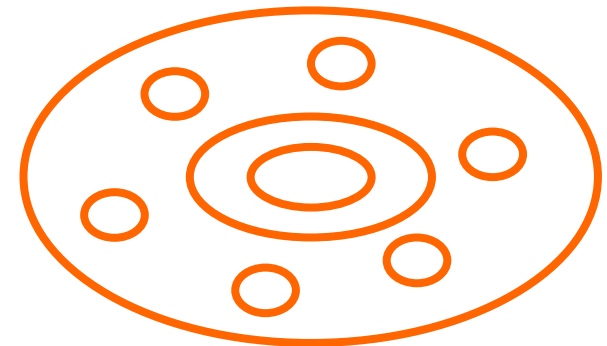
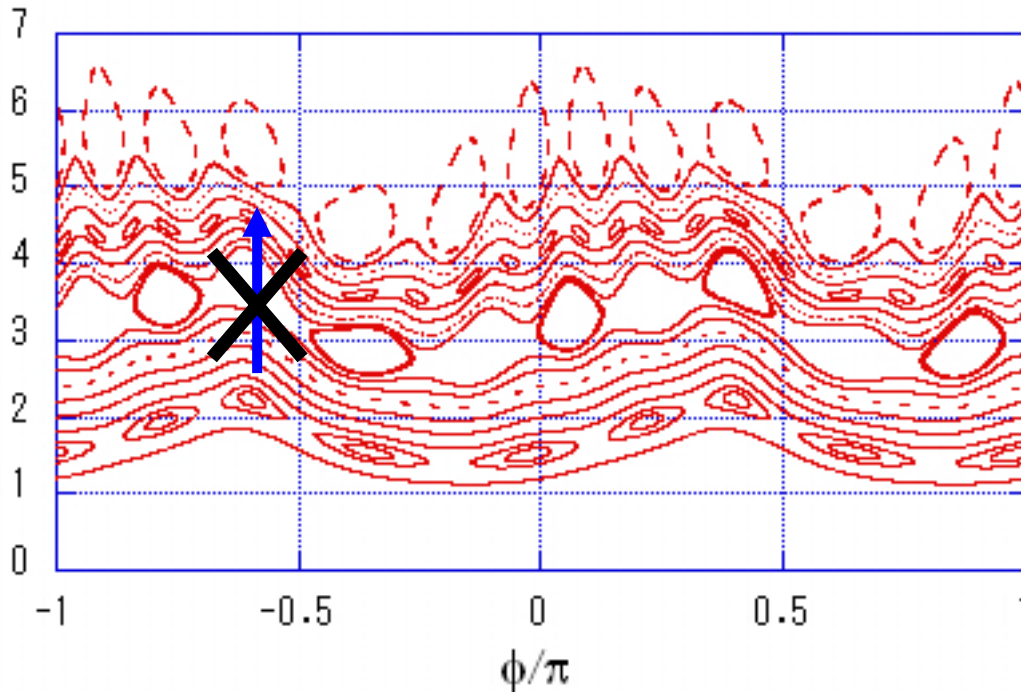
- Equilibrium distribution

$$\psi(J) \approx \exp\left(-\frac{J_1}{\varepsilon_1} - \frac{J_2}{\varepsilon_2} - \frac{J_3}{\varepsilon_3}\right) \quad \varepsilon: \text{emittance}$$

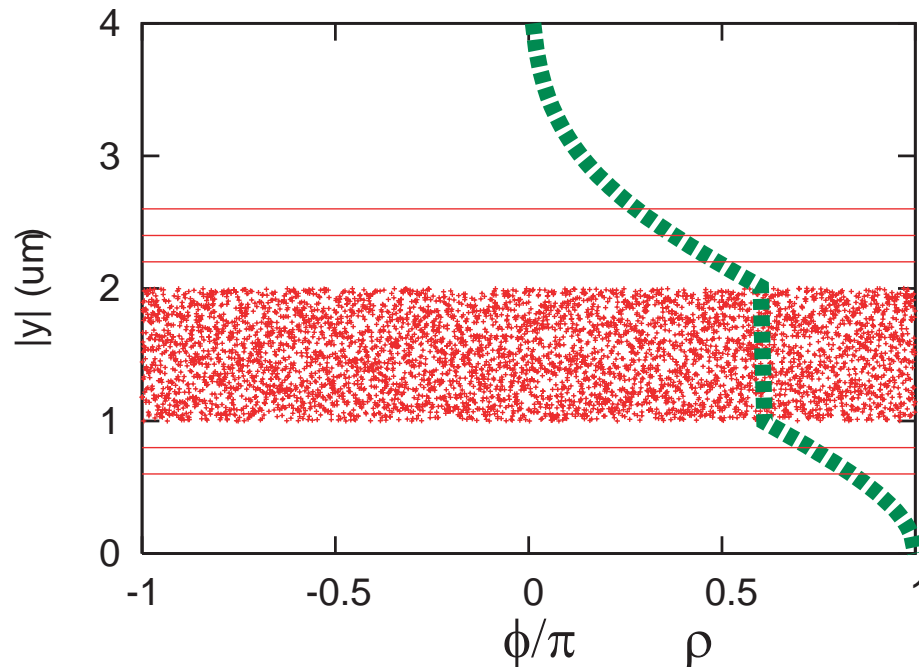


# One degree of freedom

- Existence of KAM curve
- Particles can not across the KAM curve.
- Emittance growth is limited. It is not essential for the beam-beam limit.



- Schematic view of equilibrium distribution
- Limited emittance growth

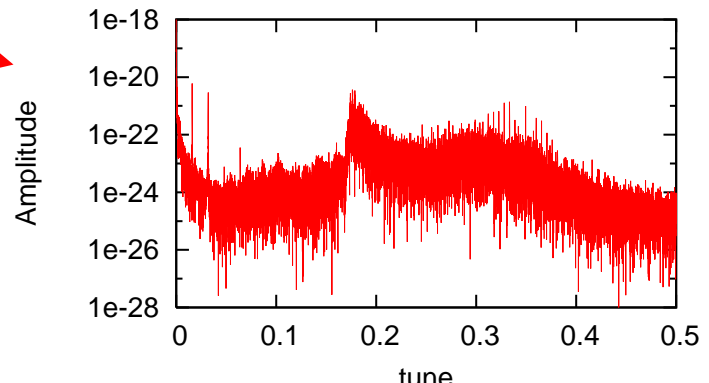
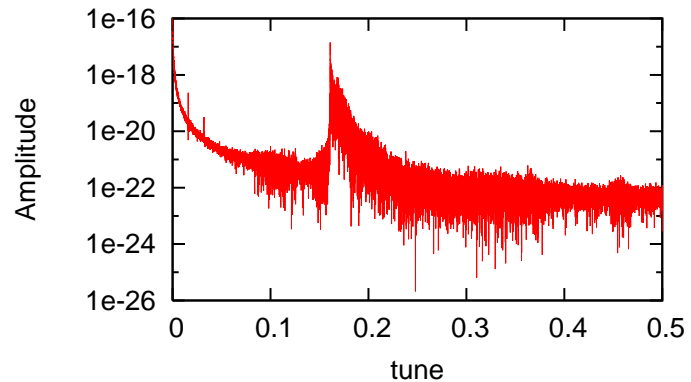
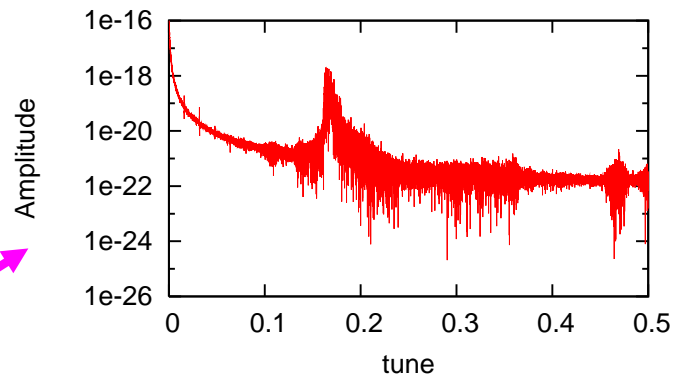
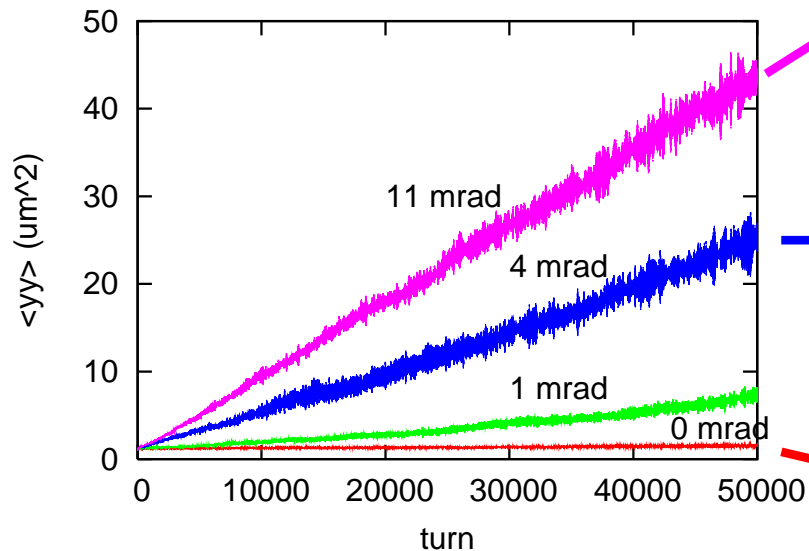


# More degree of freedom

Gaussian weak-strong beam-beam model

- Diffusion is seen even in symplectic system.

# Diffusion due to crossing angle and frequency spectra of $\langle y^2 \rangle$

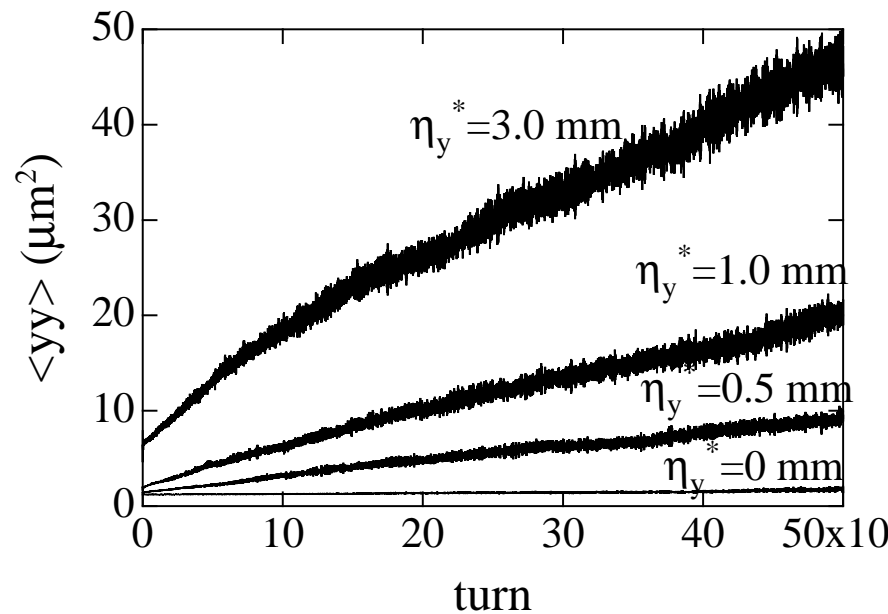
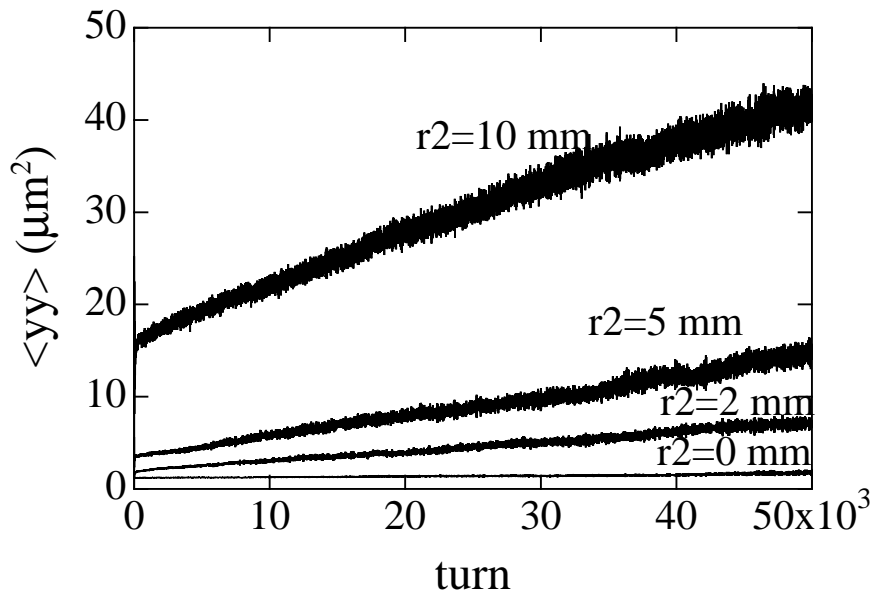


Only  $2\nu_y$  signal was observed.

# Linear coupling for KEKB

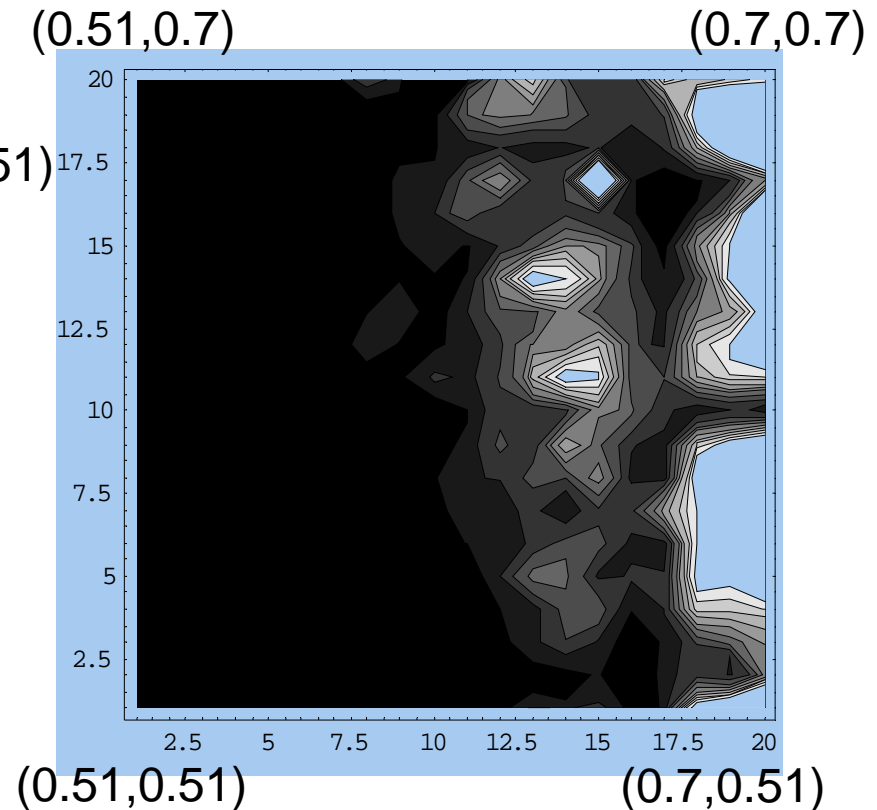
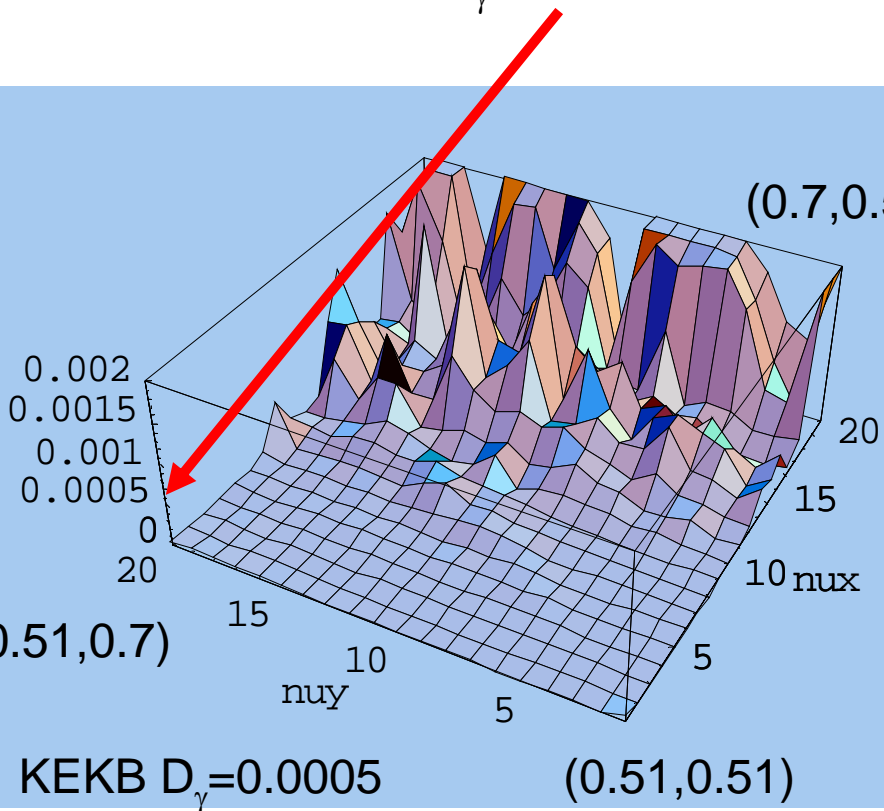
- Linear coupling ( $r$ 's), dispersions, ( $\eta$ ,  $\zeta$ =crossing angle for beam-beam) worsen the diffusion rate.

M. Tawada et al, EPAC04



# Two dimensional model

- Vertical diffusion for  $\xi=0.136$
- $D_C \ll D_\gamma$  for wide region (painted by black).
- No emittance growth, if no interference. Actually, simulation including radiation shows no luminosity degradation nor emittance growth in the region.
- Note KEKB  $D_\gamma=5 \times 10^{-4}$  /turn    DAFNE  $D_\gamma=1.8 \times 10^{-5}$  /turn





# 3-D simulation including bunch length ( $\sigma_z \sim \beta_y$ )

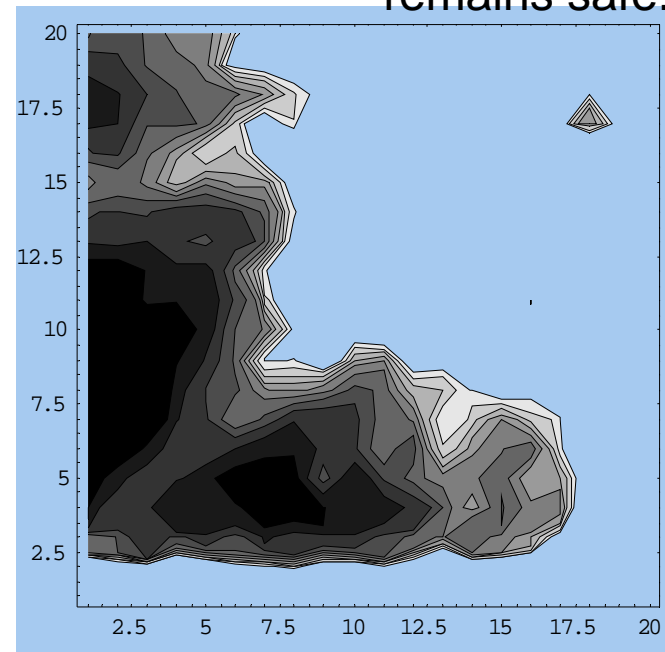
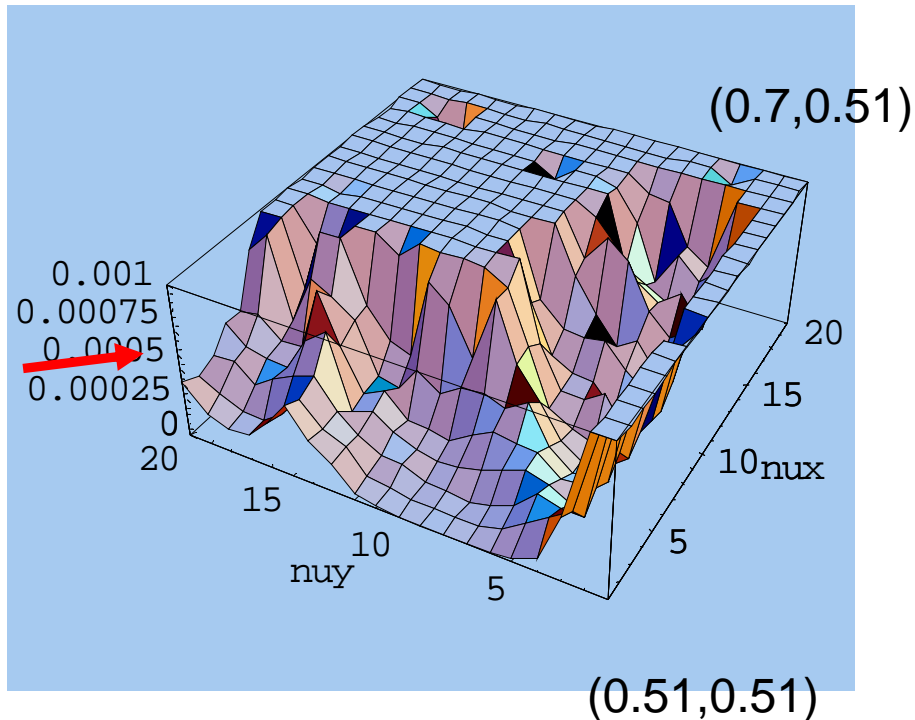
## Head-on collision

Global structure of the diffusion rate.

Fine structure near  $v_x=0.5$

Contour plot

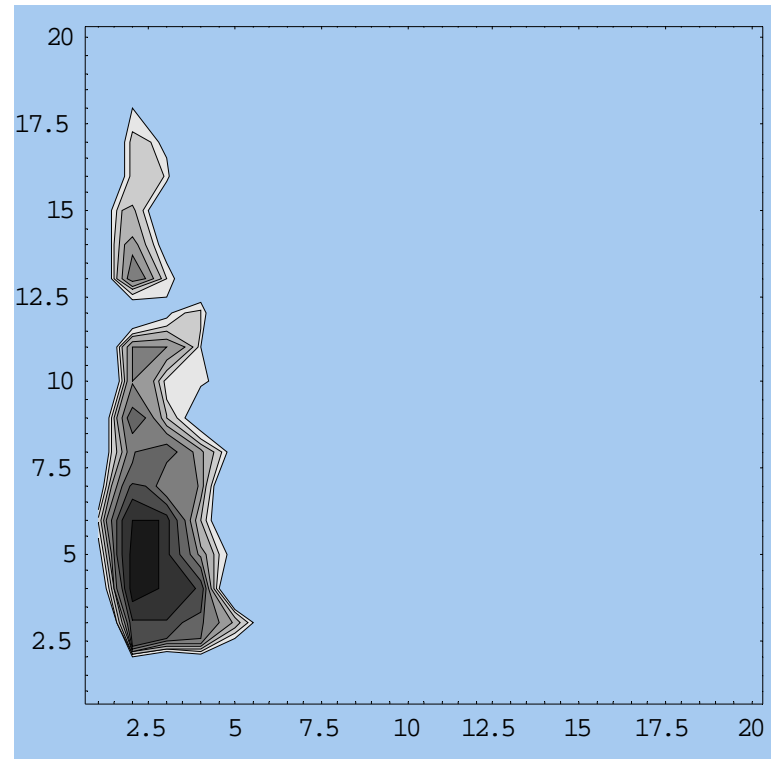
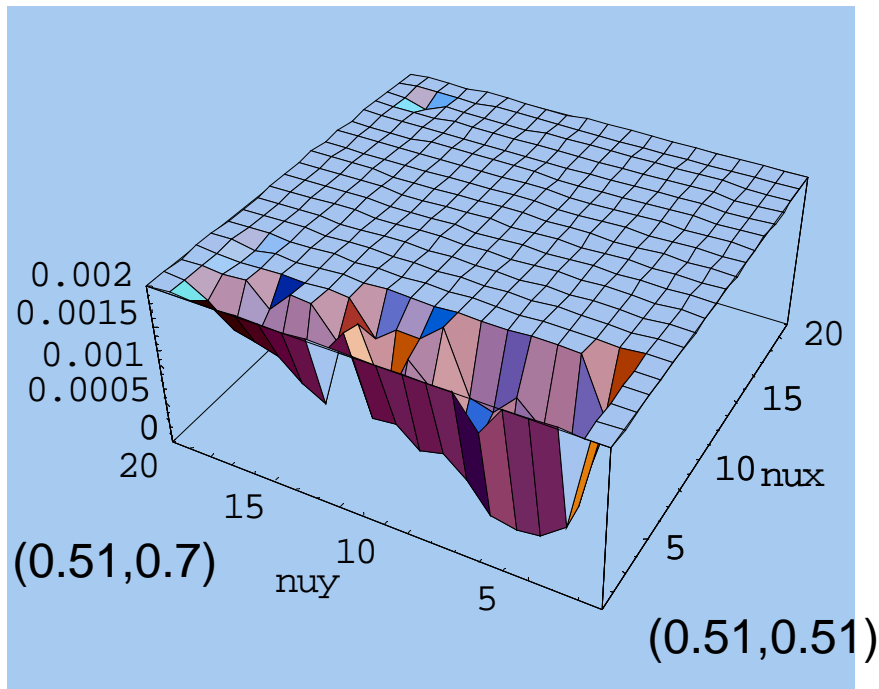
- Good region shrunk drastically.
- Synchrobeta effect near  $v_y \sim 0.5$ .
- $v_x \sim 0.5$  region remains safe.



# Crossing angle ( $\phi\sigma_z/\sigma_x\sim 1$ , $\sigma_z\sim\beta_y$ )

- Good region is only  $(v_x, v_y)\sim(0.51,0.55)$ .

(0.7,0.51)



# Reduction of the degree of freedom.

- For  $v_x \sim 0.5$ , x-motion is integrable.

(work with E. Perevedentsev)

$$\lim_{v_x \rightarrow 0.5^+} D_{C,y} = 0$$

if zero-crossing angle and no error.

$$L \propto \frac{1}{\Delta v_x + (\text{crossing angle}) + (\text{coupling}) + (\text{fast noise})}$$

- Dynamic beta, and emittance

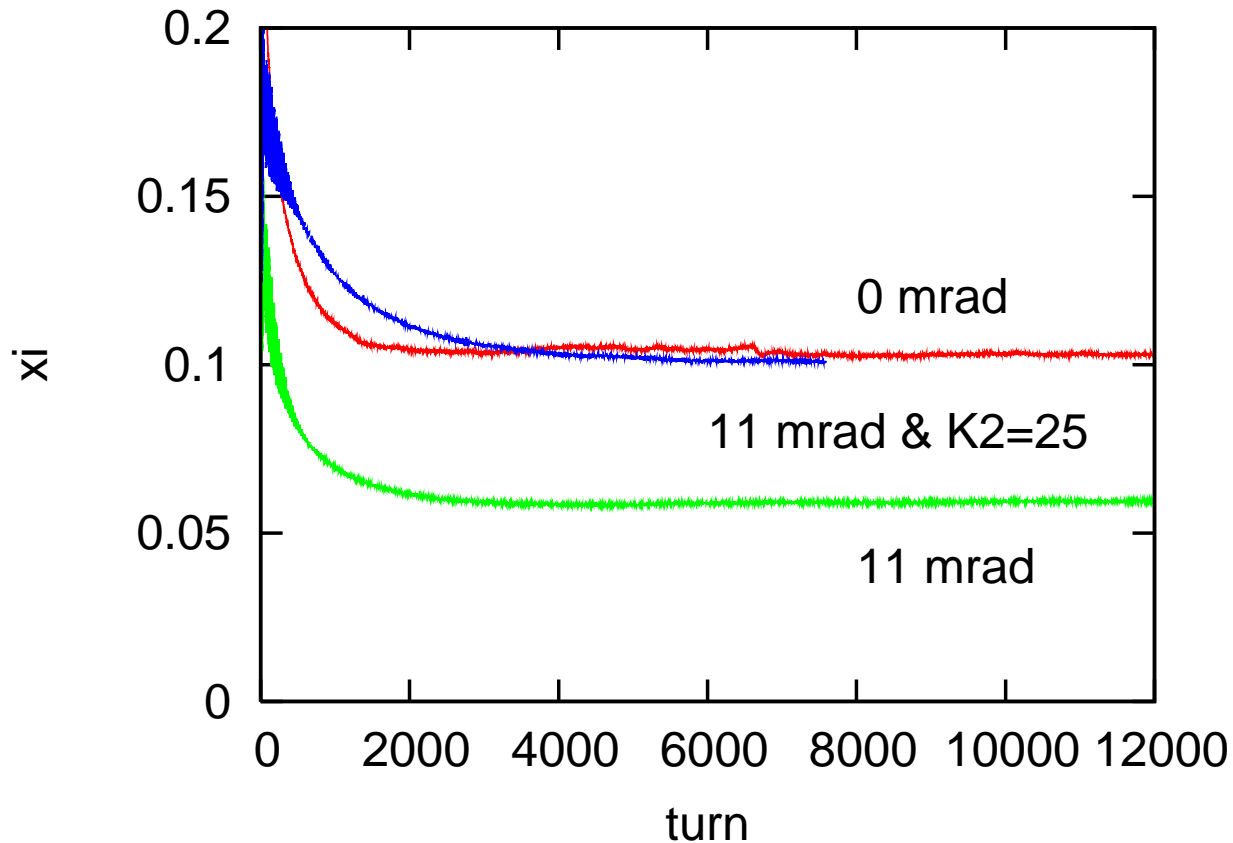
$$\lim_{v_x \rightarrow 0.5^+} \langle x^2 \rangle < \sigma_{x,0}^2$$

$$\lim_{v_x \rightarrow 0.5^+} \langle p_x^2 \rangle = \infty$$

- Choice of optimum  $v_x$

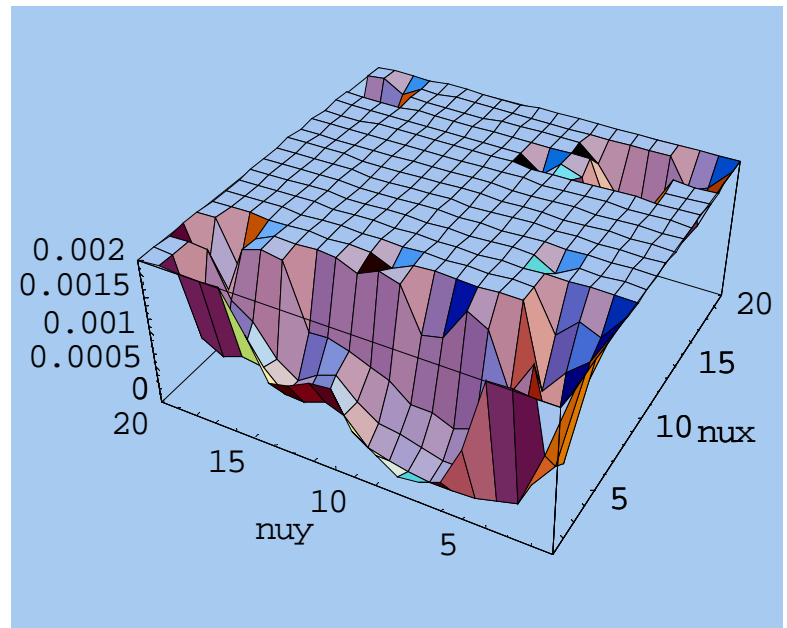
# Crab waist for KEKB

- $H=25 \times p_y^2$ .
- Crab waist works even for short bunch.



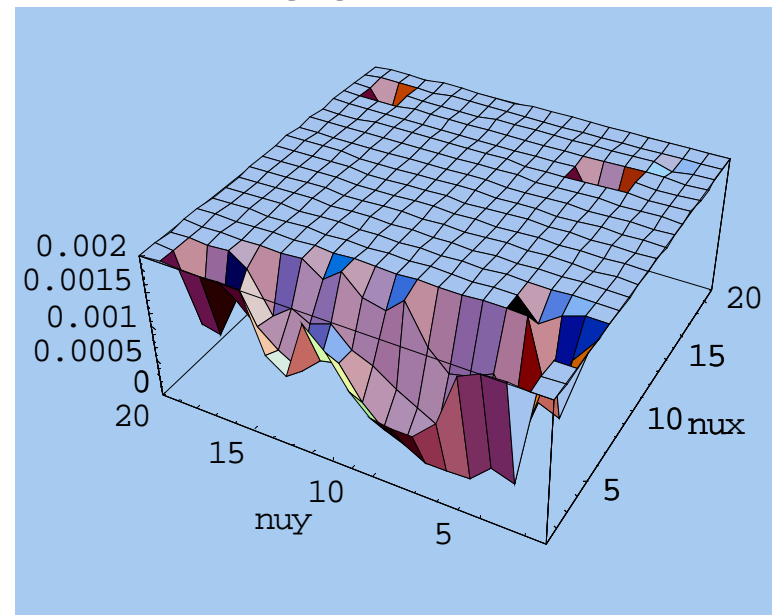
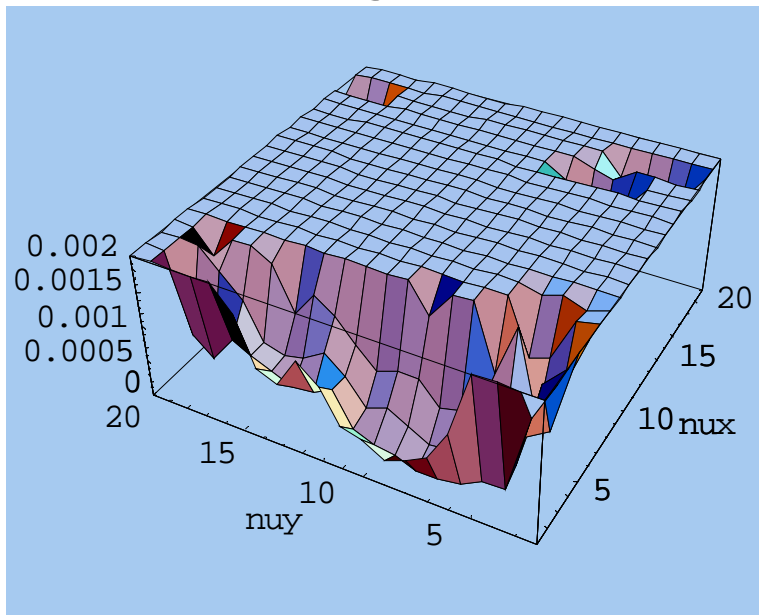
# Sextupole strength and diffusion rate

$K_2=20$



30

25



# Why the sextupole works?

- Nonlinear term induced by the crossing angle may be cancelled by the sextupole.

- Crab cavity

$$\exp(-: F :) = \exp(-: \theta p_x z :) \exp(: \theta p_x z :) = 1$$

- Crab waist

$$\exp(-: F :) = \exp(-: \theta p_x z :) \exp(-K_2 : xp_y^2 :) = \dots$$

Need study

$$\exp(: F :) M_{BB} \exp(-: F :)$$

# Conclusion

- Crab-headon  
 $L_{\text{peak}}=8 \times 10^{35}$ . Bunch length 2.5mm is required for  $L=10^{36}$ .
- Small beam size (superbunch) without crab-waist.  
Hard parameters are required  $\varepsilon_x=0.4\text{nm}$   $\beta_x=1\text{cm}$   
 $\beta_y=0.1\text{mm}$ .
- Small beam size (superbunch) with crab-waist.  
If a possible sextupole configuration can be found,  $L=10^{36}$  may be possible.
- Crab waist scheme is efficient even for shot bunch scheme.