Update on SuperKEKB Design

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June/14/2006 3rd SuperB workshop at SLAC Machine parameters and luminosity estimation

- Recent status of crab cavity
 - since 2nd SuperB WS (I reported at Frascati).

Luminosity

(Estimation of geometrical luminosity)

- Luminosity formula $L = f_{col} \int dx dy dz_1 dz_2 ds \rho_1(x, y, z_1; s) \rho_2(x, y, z_2; -s) \delta\left(s - \frac{z_1 - z_2}{2}\right)$ $= f_{col} \int dx dy dz_1 ds \rho_1(x, y, z_1; s) \rho_2(x, y, z_1 - 2s; -s)$ • Dortiolo domaity $s = \frac{z_1 - z_2}{2}$ $z_2 = -\infty \sim +\infty$
- Particle density

$$\rho(x, y, z; s) = \frac{N}{2\pi\sigma_x(s)\sigma_y(s)} \exp\left(-\frac{x^2}{2\sigma_x^2(s)} - \frac{y^2}{2\sigma_y^2(s)}\right) \frac{1}{\sqrt{2\pi\sigma_z}} \exp\left(-\frac{z^2}{2\sigma_z^2}\right)$$

• Beam size



Traveling Focus

The particles of the head and tail of a bunch are focused in different places, so that the focus point is running from the head to the tail.



Traveling Focus



Different particles have different waist.



Beam-beam tune shift

• Beam-beam tune shift

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BB kick = Deflection by Coulomb force

$$\xi_{x,y} = \frac{\beta_{x,y}}{4\pi} k_{x,y} \begin{cases} \Delta x' = -k_x x \quad \Delta x' = -\frac{N_+ r_e}{\gamma_-} F_x \\ \Delta y' = -k_y y \quad \Delta y' = -\frac{N_+ r_e}{\gamma_-} F_y \end{cases}$$

• Beam-beam tune shift with beam distribution

$$\xi_x = \frac{r_e}{4\pi\gamma_-} \int dz \rho_+(z) \beta_x(s) \frac{\partial F_x}{\partial x} \Big|_{x=z\theta,y=0} \delta\left(s - \frac{z}{2}\right) \qquad \text{Crossing angle: } 2\theta \\ \xi_y = \frac{r_e}{4\pi\gamma_-} \int dz \rho_+(z) \beta_y(s) \frac{\partial F_y}{\partial y} \Big|_{x=z\theta,y=0} \delta\left(s - \frac{z}{2}\right) \qquad x = z\theta \end{cases}$$

• Bassetti-Erskine formula (Coulomb force)

$$\begin{split} F &= F_{y} + iF_{x} \\ &= \frac{2\sqrt{\pi}}{\Sigma} \Biggl[w\Biggl(\frac{x+iy}{\Sigma}\Biggr) - \exp\Biggl(-\frac{x^{2}}{2\sigma_{x}^{2}} - \frac{y^{2}}{2\sigma_{y}^{2}}\Biggr) w\Biggl(\frac{x/\kappa + i\kappa y}{\Sigma}\Biggr) \Biggr] \\ & \kappa = \sigma_{y}(s)/\sigma_{x}(s) \\ w(z) &= \exp\Bigl(-z^{2})\left\{1 - \operatorname{erf}\left(-iz\right)\right\} \\ \frac{\partial F_{x}}{\partial x} \Bigr|_{y=0} &= \frac{4}{\Sigma^{2}} \Biggl\{1 - \kappa \exp\Bigl(-\frac{x^{2}}{2\sigma_{x}^{2}}\Bigr) \Biggr\} - \frac{4\sqrt{\pi}}{\Sigma^{3}} x \operatorname{Im}\Biggl[w\Biggl(\frac{x}{\Sigma}\Biggr) \Biggr] + \frac{2\sqrt{\pi}}{\Sigma} \Biggl(\frac{x}{\sigma_{x}^{2}}\Biggr) \exp\Bigl(-\frac{x^{2}}{2\sigma_{x}^{2}}\Biggr) \operatorname{Im}\Biggl[w\Biggl(\frac{\kappa}{\Sigma}x\Biggr) \Biggr] \\ \frac{\partial F_{y}}{\partial y} \Bigr|_{y=0} &= -\frac{4}{\Sigma^{2}} \Biggl\{1 - \frac{1}{\kappa} \exp\Bigl(-\frac{x^{2}}{2\sigma_{x}^{2}}\Biggr) \Biggr\} - \frac{4\sqrt{\pi}}{\Sigma^{3}} x \operatorname{Re}\Biggl[iw\Biggl(\frac{x}{\Sigma}\Biggr) \Biggr] + \frac{2\sqrt{\pi}}{\Sigma} \Biggl(\frac{2x}{\Sigma^{2}}\Biggr) \exp\Bigl(-\frac{x^{2}}{2\sigma_{x}^{2}}\Biggr) \operatorname{Re}\Biggl[iw\Biggl(\frac{\kappa}{\Sigma}x\Biggr) \Biggr] \end{split}$$

SuperKEKB	Crab crossing		Finite crossing		
E (LER/HER)	3.5 / 8.0				GeV
I (LER/HER)	10 / 4.4				А
N (LER/HER)	1.26x10 ¹¹ / 5.5x10 ¹⁰				
n _b	5000				
ε _x	18	9.0	6.0	6.0	nm
ε _y	0.18	0.045	0.06	0.06	nm
β_x^*	20	20	10	5	cm
β_y^*	3	3	1	0.5	mm
σ_x^*	60	42	25	17	μm
σ_{y}^{*}	0.73	0.37	0.25	0.17	μm
σ_{z}	3	3	6	6	mm
$\theta_{\rm x}$	0 (30)	0 (30)	30	30	mrad
${\xi_{\mathrm{x0}}}^{*1}$	0.196	0.395	0.042	0.022	
${\xi_{y0}}^{*1}$	0.267 (0.241 ^{*2})	0.758	0.197	0.169	
L _{geometrical}	5.3(<mark>5.6^{*2}</mark>)	15	9.1	12	$x10^{35}$ cm ⁻² s ⁻¹

*1nominal tune shift *2travel focus

In the real machine,

Finite crossing scheme degrades luminosity due to nonlinear terms.

To alleviate this, we introduce crab crossing or crab waist.

See ohmi-san 's talk(Beam-beam simulations)

SuperKEKB	Crab crossing		Crab waist		
E (LER/HER)	3.5 / 8.0				GeV
I (LER/HER)	10 / 4.4				А
N (LER/HER)	1.26x10 ¹¹ / 5.5x10 ¹⁰				
n _b		5000			
ε _x	18	9.0	6.0	6.0	nm
ϵ_{y}	0.18	0.045	0.06	0.06	nm
β_x^*	20	20	10	5	cm
β_y^*	3	3	1	0.5	mm
σ _z	3	3	6	6	mm
$\theta_{\rm x}$	0 (30)	0 (30)	30	30	mrad
ν_{s}	0.025	0.025	0.01	0.01	
ξ_{x0}^{*1}	0.196	0.395	0.042	0.022	
ξ_{y0}^{*1}	0.267	0.758	0.197	0.169	
L (W.S*2)	6.1	8.0	6.7	10	x10 ³⁵ cm ⁻² s ⁻¹
L (S.S*3)	6.0	8.3	4.8	9.0	x10 ³⁵ cm ⁻² s ⁻¹

*¹nominal tune shift *²Weak-Strong simulation *³Strong-Strong simulation



What is crab crossing and Recent status of the crab cavity

KEKB Crab Crossing

The crab crossing scheme allows a large crossing angle collision without introducing any synchrotron-betatron coupling resonances. $^{1, 2)}$

- 1) R.B.Palmer, SLAC-PUB-4707,1988
- 2) K.Oide and K.Yokoya, SLAC-PUB-4832,1989



Conceptual Design of KEKB Crab Cavity



We use TM110 to make horizontal kick.

Squashed Cell Shape Cavity

The squashed cell shape cavity scheme was studied extensively by Akai at Cornell in 1991 and 1992 for CESR-B under KEK-Cornell collaboration.

We adopted this design as "base design"!



Crab crossing with a crab cavity

x-position at IP induced by kick with a crab cavity:

$$x^{*} = \frac{\sqrt{\beta_{x}^{*}\beta_{x}^{crab}}}{2\sin \pi v_{x}} \cos\left(\pi v_{x} - |\psi_{x}^{*} - \psi_{x}^{crab}|\right) \Theta_{x}^{crab}} = \frac{\sqrt{\beta_{x}^{*}\beta_{x}^{crab}}}{2} \Theta_{x}^{crab}, \quad \text{if} \quad \Delta \psi_{x} = \psi_{x}^{*} - \psi_{x}^{crab} = \frac{\pi}{2} + n\pi$$

Betatron phase advance
Dipole kick changes
equilibrium position.
(If v_{x} =integer, orbit diverges.)
(If v_{x} =integer, orbit diverges.)
Kick angle due to
crab cavity
 Θ_{x} crab
 Ω_{x}^{crab} Ω_{x}^{crab}
Etatron oscillation:

If $f_{external}$ is independent on x, $x=x_0+x_{COD}$.

Bunch is crabbing

in the whole ring.

Crab crossing with a crab cavity

Transverse kick of crab cavity:

$$\frac{dp_x}{dt} = ecB \qquad z = ct$$

$$\Theta_x^{crab} = \frac{p_x}{E} = \frac{eV_{\perp}\sin(2\pi f_{rf} z/c)}{E} f_{rf}$$
 frequency

Half crossing angle is:

$$\tan \frac{\theta_x}{2} = \frac{dx^*}{dz} = \frac{\sqrt{\beta_x^* \beta_x^{crab}}}{2} \frac{d\Theta_x^{crab}}{dz}\Big|_{z=0}$$
$$= \frac{2\pi f_{rf} eV_\perp \sqrt{\beta_x^* \beta_x^{crab}}}{2c(E/e)}$$





Deflecting voltage of the crab cavity:

$$V_{\perp} = \frac{2c(E/e)}{2\pi f_{rf}\sqrt{\beta_x^*\beta_x^{crab}}}\tan\frac{\theta_x}{2}$$

Requirement for the crab cavity at KEKB

KEKB	LER	HER	
Е	3.5	8	GeV
f _{rf}	5(MHz	
$\theta_{\rm x}$	2	mrad	
β_x^*	0.59	0.56	m
β_x^{crab}	45	250	m
V_{\perp}	1.4	1.4	MV

We have achieved 1.4 MV at horizontal test on June/8/2006.

Superconducting crab cavity for KEKB



Results of Q-value at the vertical test for the crab cavities





LER cavity has achieved the best performance for the peak electric field.

HER cavity is worse performance than that of LER, however it satisfies the requirement.

Horizontal test of crab cavity

Mt. Tsukuba

HER Crab cavity



Assembly of the first crab cavity.

Coaxial beam pipe assembly





Installation was very difficult !





Assembly of HER crab cavity has been done on April 21!



The cavity was moved for the horizontal test.



Installation of the crab cavity in the test stand



Horizontal test of HER crab cavity



Crab cavity cool-down toward 4K

The cavity was cooled down very slowly.



Horizontal Test for HER Crab Cavity

Due to the adjustment of the helium flow

The resonant frequency was lowered by about 300kHz than the operation frequency(508.8MHz). Now we are investigating the reason.



The loaded Q value measured by network analyzer was 1.6×10^5 . It was consistent with the estimation (2×10^5) by HFSS. In high power test, the loaded Q value was 1.7×10^5 .

What needs to be fixed

- Discrepancy between resonant frequency and operation frequency is about 300kHz.
- Range of tuner position is smaller than that of expected.
- Tuner feedback stability



Near future plan

- Tuner reforming
- Cavity pre-tuning
- HPR for the cavity
- Re-assembly of the HER crab cavity
- Assembly of the LER crab cavity

Two crab cavities will be ready for the installation to the tunnel in the end of this year(hopefully).

Optics for crab cavity



Summary

- Machine parameters are reconsidered.
- Both of crab crossing and crab waist are hopeful to achieve higher luminosity.(→BB simulation)
 - Extremely small beta has to be achieved for the crab waist.
- Traveling focus provides luminosity gain about 5-7%.
- In case of crab crossing, better betatron tune is 0.503/.55, however it might be prevented by physical aperture around IR due to dynamic effects.(→IR issues)
 - Other things such as electron cloud, CSR, etc. should be also solved at SuperKEKB.
- Crab cavity is assembled successfully and have been operated at the horizontal test.
- Required deflecting voltage of 1.4 MV has been achieved.

Major achievements expected at SuperKEKB

M. Hazumi



Backup slides

Projection of integrated luminosity and expected discoveries at SuperKEKB



Discoveries at SuperKEKB and required integrated luminosities (discovery = significance > 5σ)

Item	Integrated luminosity (ab ⁻¹)		New physics	
$B \rightarrow \tau \nu$	0.5		charged Higgs	
$B \rightarrow D\tau v$	1*		charged Higgs	
New CP violation in $B^0 \rightarrow \eta$ Ks	10**		SUSY breaking, extra dimension, GUT, baryogenesis/leptogenesis	
New CP violation in $B^0 \rightarrow \phi Ks$	15**		SUSY breaking, extra dimension, GUT, baryogenesis/leptogenesis	
$B \rightarrow \mu \nu$	30***		SUSY MFV	
$B \rightarrow K_{VV}$	50*		EW baryogenesis, dark matter, SUSY	

- * From SuperKEKB. Estimations will be updated in Autumn 2006.
- ** Assuming WA values as of August 2005.
- *** Guestimation assuming Br= $4x10^{-7}$, full rec. eff. = 0.1%, and no background. Need simulation studies.

Luminosity

• Luminosity formula (well-known)



Luminosity

• Luminosity formula for machine design



Lattice parameters w/o and w/ beam-beam effect

SuperKEKB		bare lattice	with beam-beam	unit
Beam current (LER/HER)	Ι	9.4/4.1	9.4/4.1	А
Beam energy (LER/HER)	Е	3.5/8.0	3.5/8.0	GeV
Emittance	ε _x	24	130 Dynan	nic ^{nm}
Horizontal beta at IP	β_x^*	20	1.9 effect	cm
Vertical beta at IP	β_y^*	3	2.4	mm
Horizontal beam size	σ_x^*	69	50	mm
Vertical beam size	σ_y^*	0.73	1.0	mm
Bunch length	σ _z	3	3	mm
Crossing angle (30 mrad crab crossing)	$\theta_{\rm x}$	0	0	mrad
Luminosity reduction	R _L	0.86	0.82	
ξ_x reduction	$R_{\xi x}$	0.99	0.98	
ξ_y reduction	$R_{\xi y}$	1.11	1.16	
Reduction ratio	$R_L^{}/R_{\xi y}^{}$	0.78	0.70	
Horizontal beam-beam (estimated with S-S simulation)	ξ _x	0.152	0.030	
Vertical beam-beam (estimated with S-S simulation)	ξ _y	0.215	0.187	
Luminosity	L	4.0 x 10 ³⁵		cm ⁻² s ⁻¹

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Head-on and finite-crossing collision



- Head-on collision will boost the beam-beam parameter up to 0.19.
- Crab cavity is one of the most important components, because it can realize head-on collision.

Head-on collision with crab cavity

Finite-crossing collision without crab cavity



Development of crab cavity applicable for high beam current(~10 A)



This is different from the cavity will be installed at KEKB. 37

Cold test of porototype crab cavity

Time variation of the cavity and cryostat vacuum





The temperature dependence of the frequency



The cold test was done !



Traveling focus

Traveling focus (in longitudinal direction)

$$H_{\pm} = \frac{a}{2} z p_y^2$$

$$y = y + \frac{\partial H_{\pm}}{\partial p_{y}}$$
$$= y + azp_{y}$$

 $\begin{pmatrix} y \\ p_y \end{pmatrix} = \begin{pmatrix} 1 & az \\ 0 & 1 \end{pmatrix} \begin{pmatrix} y \\ p_y \end{pmatrix}$

Transformation of Twiss parameters:

$$\begin{pmatrix} \beta & \alpha \\ \alpha & \gamma \end{pmatrix} = \begin{pmatrix} 1 & az \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \beta & 0 \\ 0 & 1/\beta \end{pmatrix} \begin{pmatrix} 1 & az \\ 0 & 1 \end{pmatrix}^{T} = \begin{pmatrix} \beta + az^{2}/\beta & az/\beta \\ az/\beta & 1/\beta \end{pmatrix}$$

Waist point moves along z position.

$$\beta(z) = \beta + \frac{az^2}{\beta}$$

Crab waist (Traveling focus in transverse plane)

$$H_{\pm} = \frac{a}{2} x p_y^2$$

Swap z and x in the left

$$y = y + \frac{\partial H_{\pm}}{\partial p_{y}}$$
$$= y + axp_{y}$$

$$\begin{pmatrix} y \\ p_y \end{pmatrix} = \begin{pmatrix} 1 & ax \\ 0 & 1 \end{pmatrix} \begin{pmatrix} y \\ p_y \end{pmatrix}$$

Transformation of Twiss parameters:

$$\begin{pmatrix} \beta & \alpha \\ \alpha & \gamma \end{pmatrix} = \begin{pmatrix} 1 & ax \\ 0 & 1 \end{pmatrix} \begin{pmatrix} \beta & 0 \\ 0 & 1/\beta \end{pmatrix} \begin{pmatrix} 1 & ax \\ 0 & 1 \end{pmatrix}^{T} = \begin{pmatrix} \beta + ax^{2}/\beta & ax/\beta \\ ax/\beta & 1/\beta \end{pmatrix}$$

Waist point moves along x position.

$$\beta(x) = \beta + \frac{ax^2}{\beta}$$