

# Materials and Material R&D in Support of ILC

2<sup>nd</sup> ILC Workshop  
Snowmass August 13 – 27, 2005

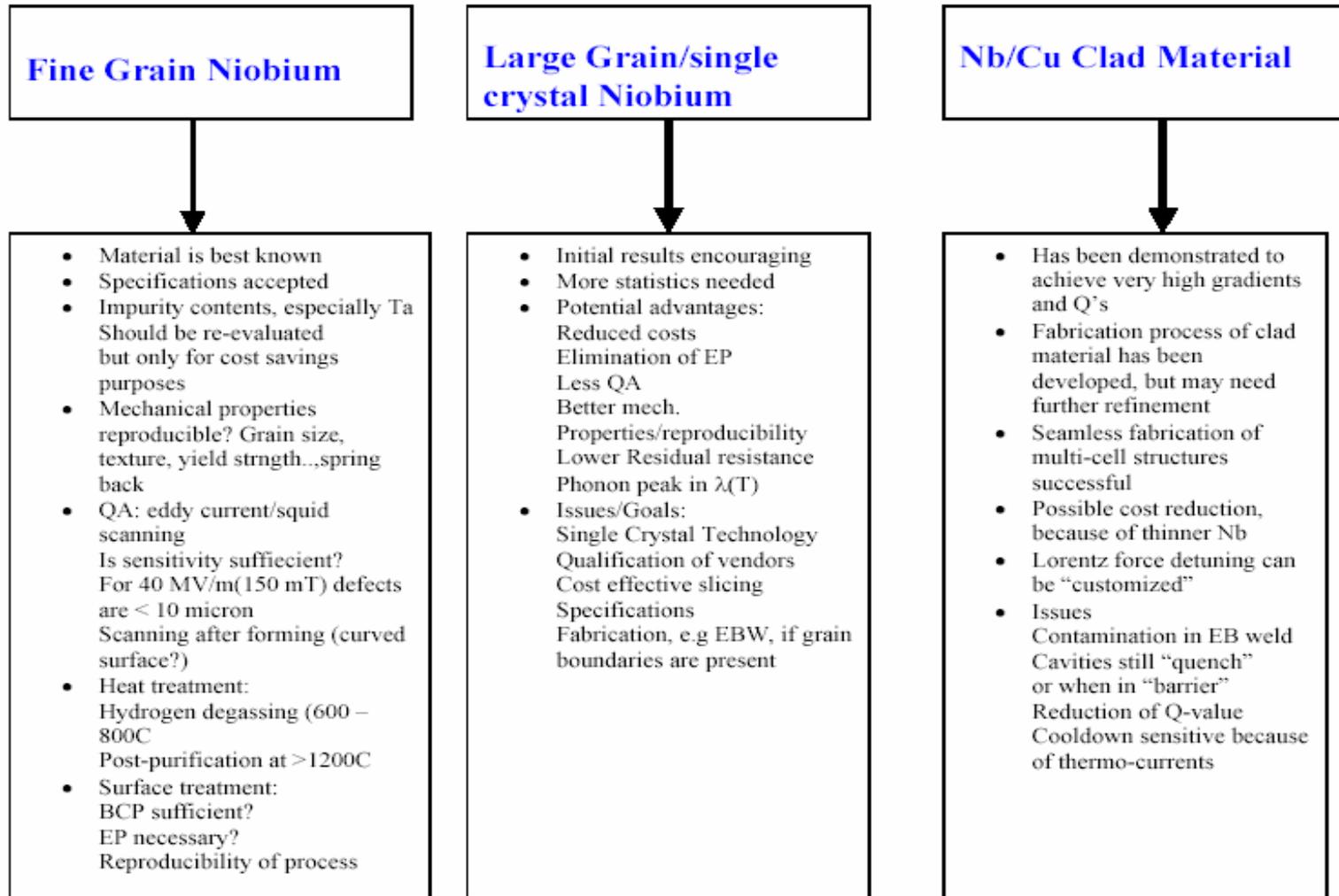
# Performance Limitations of SC Nb Cavities

- **Critical Magnetic Field**  $H_{\text{crit}} \sim 185 \text{ mT}$   
Reduced  $H_p/E_{\text{acc}}$  (LL, RE –shape)  
 $E_{\text{acc}} \geq 50 \text{ MV/m}$  , but  $E_{\text{peak}} \geq 110 \text{ MV/m}$
- **Field Emission:** Contamination Control  
Clean Processing and Assembly  
Prevention of Re-contamination
- “Q – drop” : remedy is “in-situ” baking  
more effective on “smooth” (EP) surfaces?
- **Defects:**  $H_{\text{RF}} < H_{\text{crit}}$  (need for QA)
- **Residual Resistance(Q-slope):** might influence operations  
Temp.

# Material R & D

- R & D in direct support of ILC
  - Standard fine grain niobium(RRR,impurity contents)
  - Large grain/single crystal niobium
  - NbCu clad material, seamless fabrication
- “Basic” R & D aimed at understanding physics
  - Surface physics ( oxidation,...)
  - Effect of hydrogen, grain boundaries,flux penetration..
  - Q vs E (“slope”, “drop”, residual resistance,special devices...)
  - Critical Magnetic field

# R & D in direct support of ILC

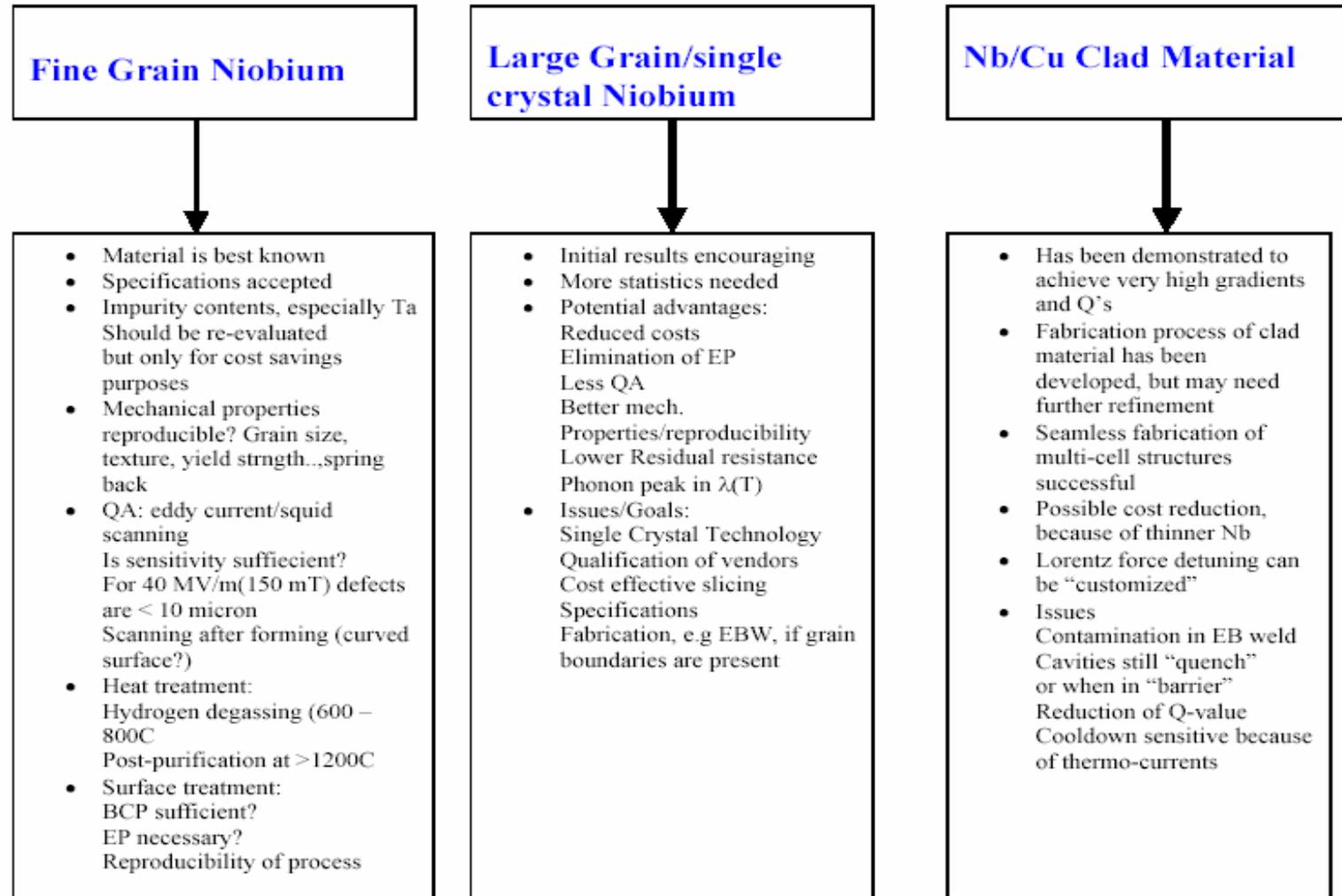


# Summary Fine Grain Niobium

- Many examples of high performance cavities (single+multi-cell) exist
- Present specifications seem to be adequate **unless cost savings can be realized with modifications in impurity contents (e.g Ta)**
- Material is readily available
- QA of sheets are carried out only at DESY to eliminate defects in starting material; is sensitivity good enough?  
Scanning of curved surfaces necessary?
- Heat treatments: 600C, 800C, >1200C?
- Electropolishing + “in situ” baking necessary to achieve high Q-values at gradients  $\geq 30$  MV/m
- **Better Micro-structure control might be necessary**  
(micro yielding, spring back, reproducible mechanical properties)

**This material is the BCD choice**

# R & D in direct support of ILC

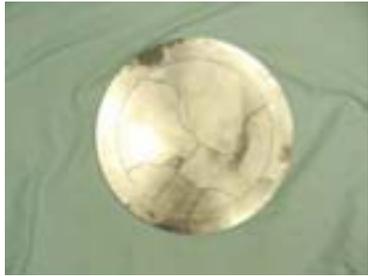


# Large Grain/Single Crystal Niobium[1]

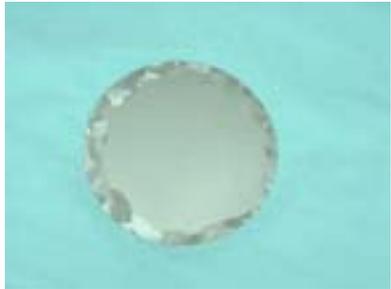
- Since the first ILC workshop we have fabricated and tested 5 single cell cavities ( 1300 MHz – 1500 MHz) from sliced material ( wire EDM and saw cut) from 3 different ingots ("A", "B", "C"), 3 different shapes, CBMM
- We have fabricated and tested 2 single crystal cavities from ingot "A" at 2.3 GHz, CBMM
- We have fabricated two 2.3 GHz cavities with material from a second vendor (WC) with somewhat smaller grains (not yet tested)
- We have fabricated and tested a single cell cavity from large grain niobium from China-Ningxia
- We have fabricated a 7-cell HG -Jlab-Upgrade cavity, which has been tested
- We are in the process of fabricating an ILC\_LL 7-cell cavity
- We have received a large grain ingot ("D") of dia 10.5" with 800 ppm Ta for fabricating single and multi-cell ILC cavities

# Large Grain/Single Crystal Niobium[2]

CBMM



Ingot "D", 800 ppm Ta



Ingot "A", 800 ppm Ta



Ingot "B", 800 ppm Ta

Ninxia



Ingot "C", 1500 ppm Ta

Wah Chang



Heraeus



# Summary of Large grain/Single Crystal Tests at Jlab

Suppl.	Ingot	RRR/Ta [ppm]	Type/ Nc	F [GHz]	Q [ $10^{10}$ ] (2K, $E_{\max}$ )	$E_{\text{acc}}$ [MV/m]	Fabrication
CBMM	A	280/800	HG / 1	1.5	<b>1.25</b>	<b>34</b>	<i>W-EDM</i>
CBMM	B	280/800	HG /1	1.5	<b>9.3</b>	<b>32</b>	<i>W-EDM</i>
CBMM	C	280/1500	ILC_LL / 1	1.3	<b>1.4</b>	<b>34</b>	<i>S-cut / W-EDM</i>
CBMM	B	280/800	OC / 1	1.5	<b>0.5</b>	<b>25</b>	<i>S-cut (80 <math>\mu\text{m}</math>)</i>
CBMM	B	280/800	HG / 1	1.5	<b>0.48</b>	<b>27.5</b>	<i>S-cut, removal test ~ 75 micron removal</i>
CBMM	A (single)	280/800	HG / 1	2.2	<b>0.5</b>	<b>38</b> <i>(185/165 mT)</i>	<i>W-EDM</i>
CBMM	A (single)	280 / 800	ILC_LL/1	2.3	<b>0.7</b>	<b>45</b>	<i>W-EDM</i>
CBMM	A	280/800	HG /7	1.5	<b>0.85</b>	<b>18-19</b> <i>(FE, MP, quench?)</i>	<i>W-EDM</i>
CBMM	C	280/1500	ILC_LL /7	1.3			<i>S-cut / W-EDM In fabrication</i>
Ninxia		330-360/150	OC / 1	1.5	<b>0.21</b>	<b>33</b> <i>(Q-drop still after bake)</i>	<i>S-Cut, machined</i>
Wah Chang	C1/C2	> 300 / < 500	HG/1	2.2		<i>Not yet tested</i>	<i>W-EDM</i>
Wah Chang	B1/B2	> 300 / < 500	HG/1	2.2		<i>Not yet tested</i>	<i>W-EDM</i>

# Large Grain/Single Crystal Niobium[3]

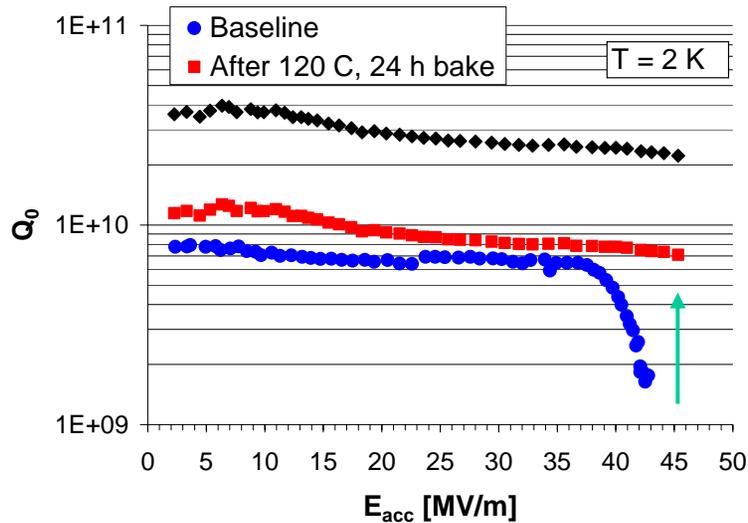
Nb Discs

LL cavity 2.3GHz



$$E_{\text{peak}}/E_{\text{acc}} = 2.072$$

$$H_{\text{peak}}/E_{\text{acc}} = 3.56 \text{ mT/MV/m}$$

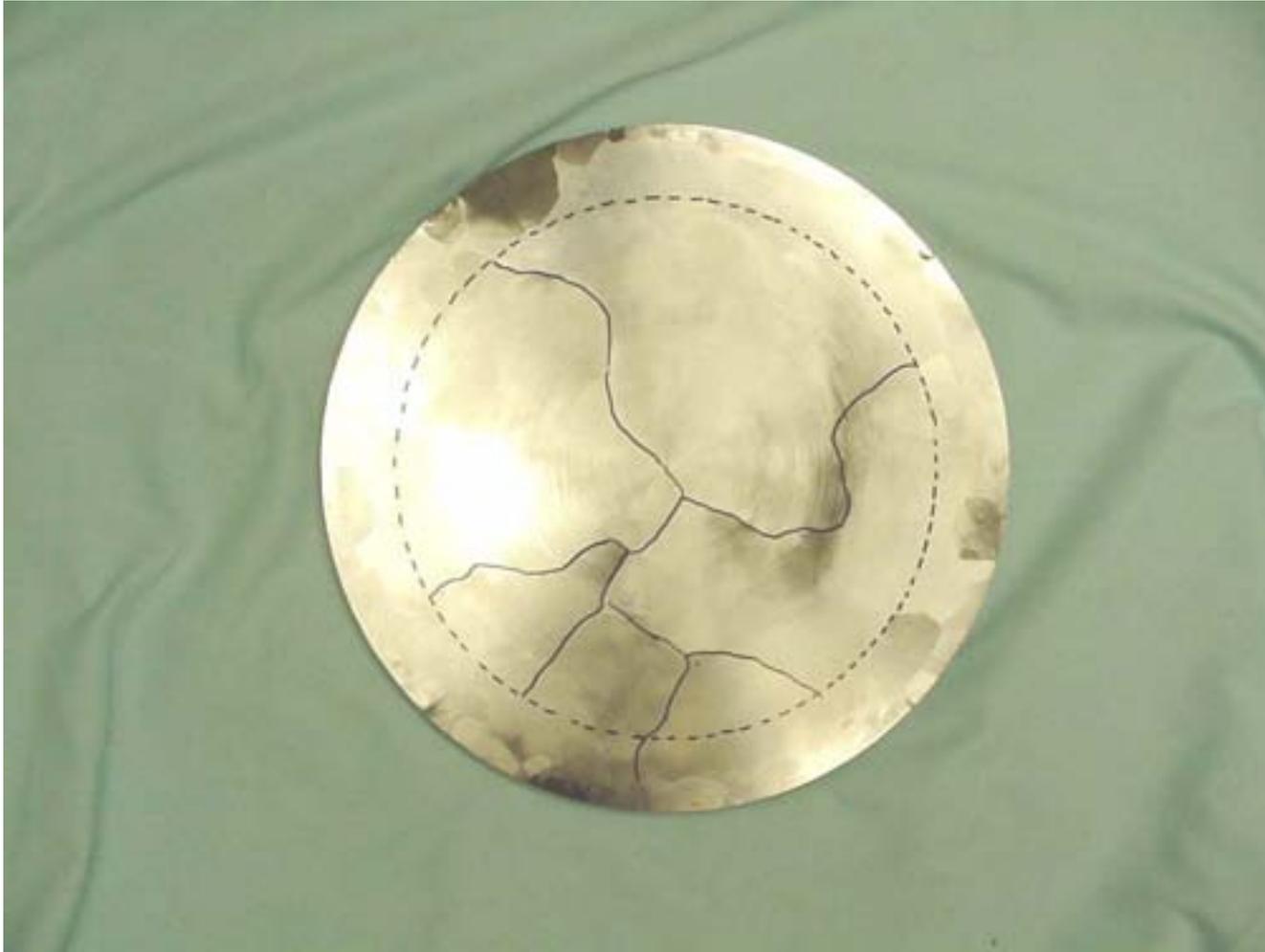


# Large Grain/Single Crystal Niobium[4]

- Main effort should be verification of positive results on single cell cavities in multi-cell cavities and materials from different vendors
- Jlab has plans for fabricating 2 high gradient 7-cell cavities and 2 TESLA type 9-cell cavities from ingot “D”[CBMM] with Ta contents of 800 ppm; however there are problems with funding and internal priorities for EBW
- DESY [W.Singer] plans to fabricate single cell cavities from Heraeus material
- Wah Chang advertised to offer large grain/single crystal niobium for sale: any takers right now and quick fabrication+testing?
- Ninxia/Beijing University offered large grain niobium

# Large Grain/Single Crystal Niobium[5]

Ingot “D”, CBMM



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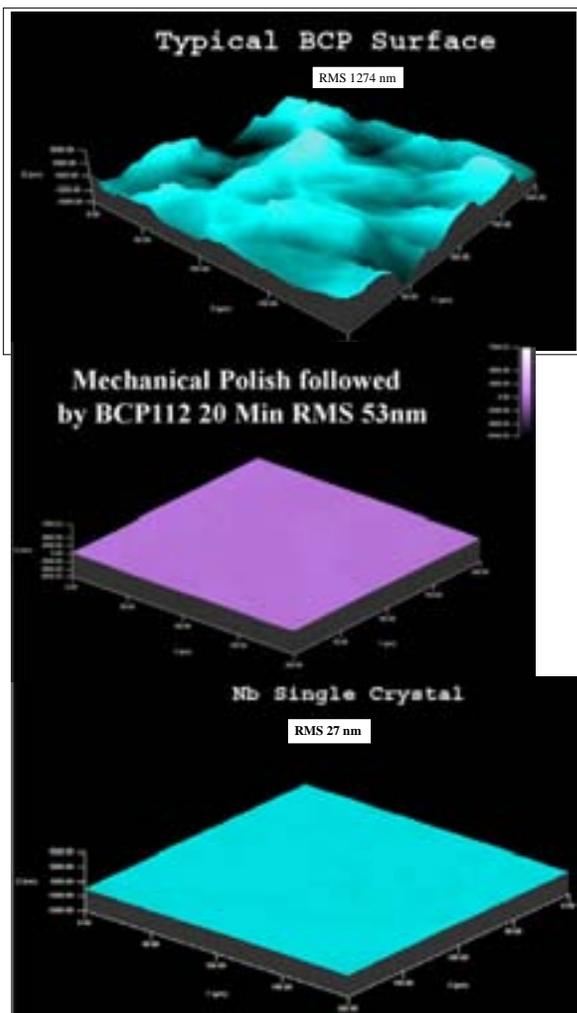
# Large Grain/Single Crystal Niobium[6]

## Potential Advantages

- Reduced costs
- Comparable performance
- Very smooth surfaces with BCP, no EP necessary
- Possibly elimination of “in situ” baking because of “Q-drop” onset at higher gradients
- Possibly very low residual resistances (high Q’s), favoring lower operation temperature (B. Petersen), less “cryo power” and therefore lower operating costs
- Higher thermal stability because of “phonon-peak” in thermal conductivity
- Good or better mechanical performance than fine grain material (e.g. predictable spring back..)
- Less material QA (eddy current/squid scanning)

# Surface Roughness (1)

BCP provides very smooth surfaces as measured by A.Wu, Jlab



RMS: 1274 nm fine grain bcp

53 nm after ~ 35 micron, single Crys

27 nm after ~ 80 micron, single Crys

251 nm fine grain ep

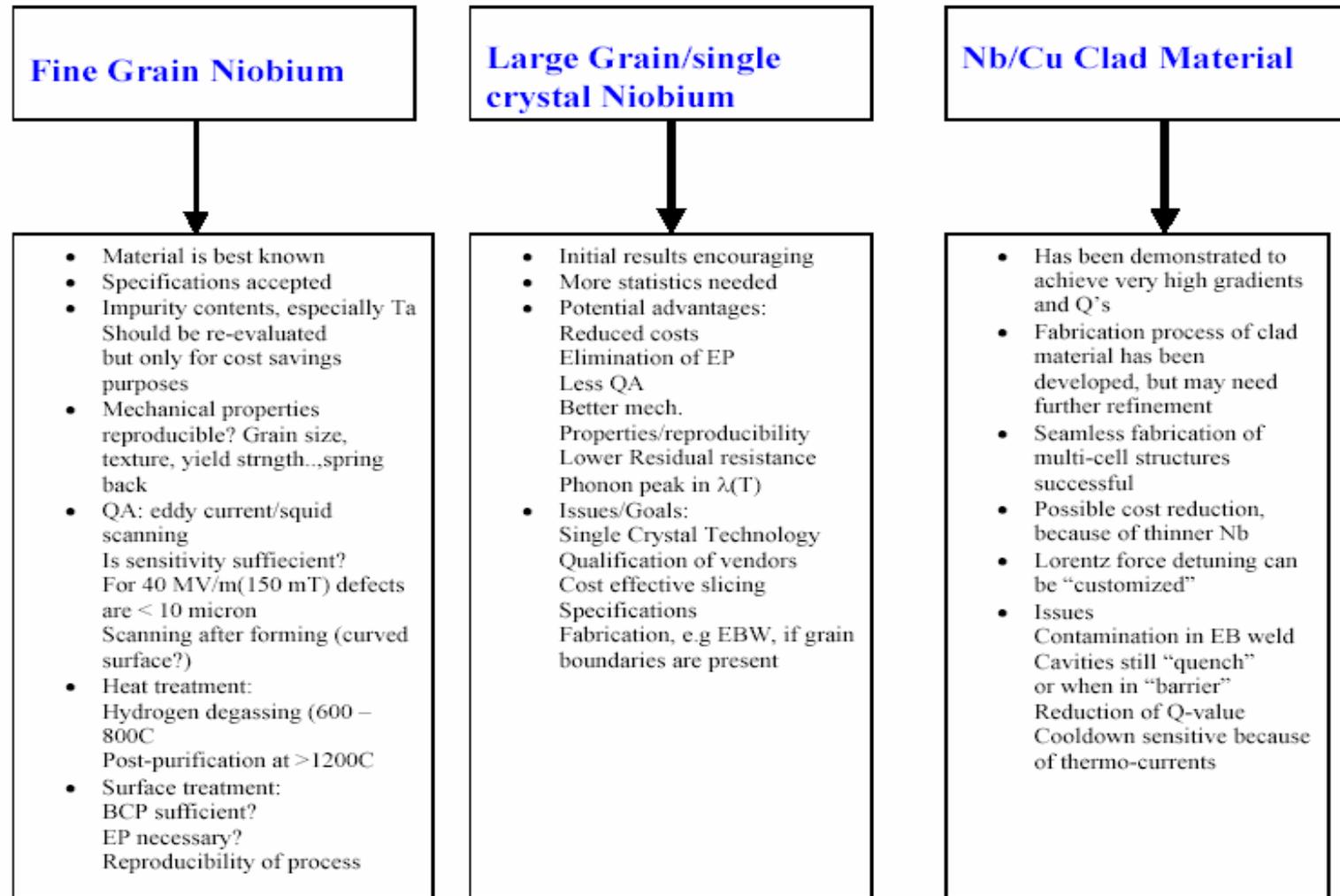


# Large Grain/Single Crystal Niobium[7]

## R & D topics/Issues:

- Technology to provide single crystals(prefered option)
- Effective cutting: wire EDM too slow?
- Forming: how uniform, grain slippage
- Welding: do grain boundaries cause problems?
- Is there a chance of vacuum leaks through grain boundaries?
- Surface roughness: appropriate acid agitation during bcp, uniformity of material removal, preferential etching at GB?
- Mechanical properties depending on grain orientation?
- Is oxidation depending on crystal orientation?
- Internal stresses and strains due to deep drawing using neutron diffraction techniques (NIST proposal)

# R & D in direct support of ILC



## Nb/Cu clad Material[1]

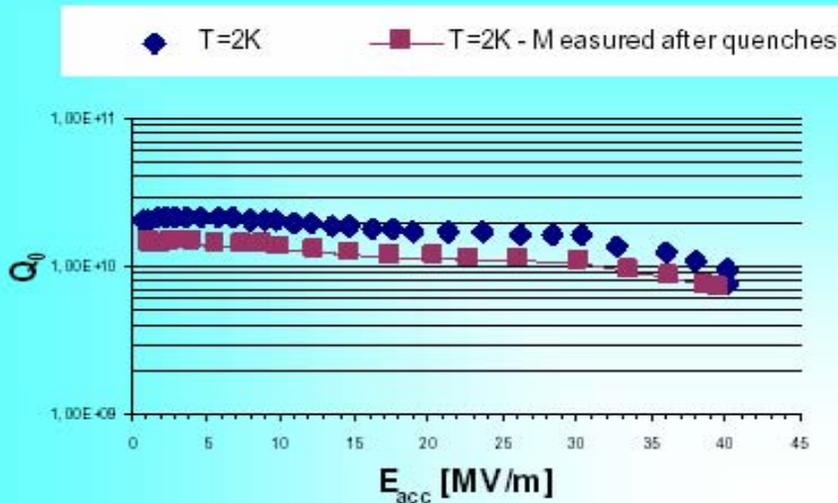
- Is being pursued at DESY (W. Singer et al) and KEK (K. Saito et al), seamless fabrication
- One topic of the European CARE program (W. Singer)
- So far good performance only demonstrated on single cell cavities, but technology for 3-cell cavities is developed (hydroforming)
- Demonstration on complete multi-cells TESLA-type cavity necessary

# Nb/Cu clad Material[2]

## Advantages

- cost effective: allows saving a lot of Nb (ca. 4 mm cavity wall has only ca. 1 mm of Nb and 3 mm Cu). Especially significant for large projects like ILC
- bulk Nb microstructure and properties (the competing sputtering technique does not have such advantages)
- the treatment of the bulk Nb BCP, EP, annealing at 800°C, bake out at 150°C, HPR, HPP can be applied (excluding only post purification at 1400°C).
- high thermal conductivity of Cu helps for thermal stabilization
- stiffening against Lorentz - force detuning and microphonics can be easily done by increasing of the thickness of Cu layer.
- fabrication by seamless technique allows elimination of the critical for the performance welds especially on equator

# Nb/Cu clad Material[3]



NbCu cavities hydroformed from explosively bonded tubes at DESY.

NbCu single cell cavity 1NC2 produced at DESY by hydroforming from explosively bonded tube. Preparation and HF tests at Jeff. Lab: 180  $\mu\text{m}$  BCP, annealing at 800°C, baking at 140°C for 30 hours, HPR (P. Kneisel).

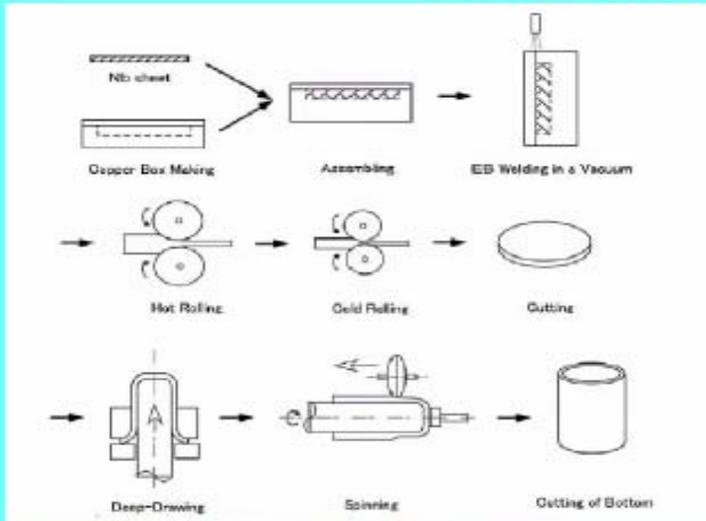
Difficult to get reproducibly high bonding quality. Hot bonding fabrication procedure of NbCu tubes seems to be more promising

**40 MV/m without EP**

W. Singer SRF 2005

# Nb/Cu clad Material[4]

## • Hot bonded NbCu tubes

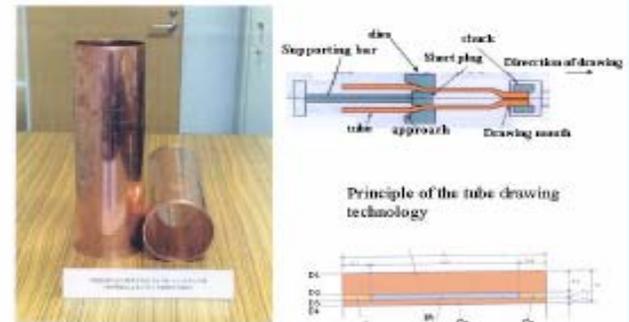


Fabrication principle of sandwiched hot rolled Cu-Nb-Cu tube (KEK and Nippon Steel Co.)

Fabrication principle of sandwiched coextruded Cu-Nb-Cu tube (KEK)



Hot roll bonded Cu-Nb-Cu tube produced at Nippon Steel Co.



Cu-Nb-Cu Sandwiched Tubes (KEK)

W. Singer SRF 2005

# Nb/Cu clad Material[5]

## Nb/Cu Clad Seamless Tubes and Cutting



# Nb/Cu clad Material[6]

## Problems

- Possibility of leaky welds because of Cu contamination
- Nb/Cu cavities still quench, resulting in Q-degradations
- Cooldown needs to be very uniform because of thermo – currents
- Cooldown of cryomodules would need modification
- Cracks sometimes appear in iris region during fabrication
- No industrialization efforts yet

# Nb/Cu clad Material[7]

## Conclusion

On laboratory level the most work is done.

Industrialization of seamless technique is the main remaining task

W. Singer SRF 2005

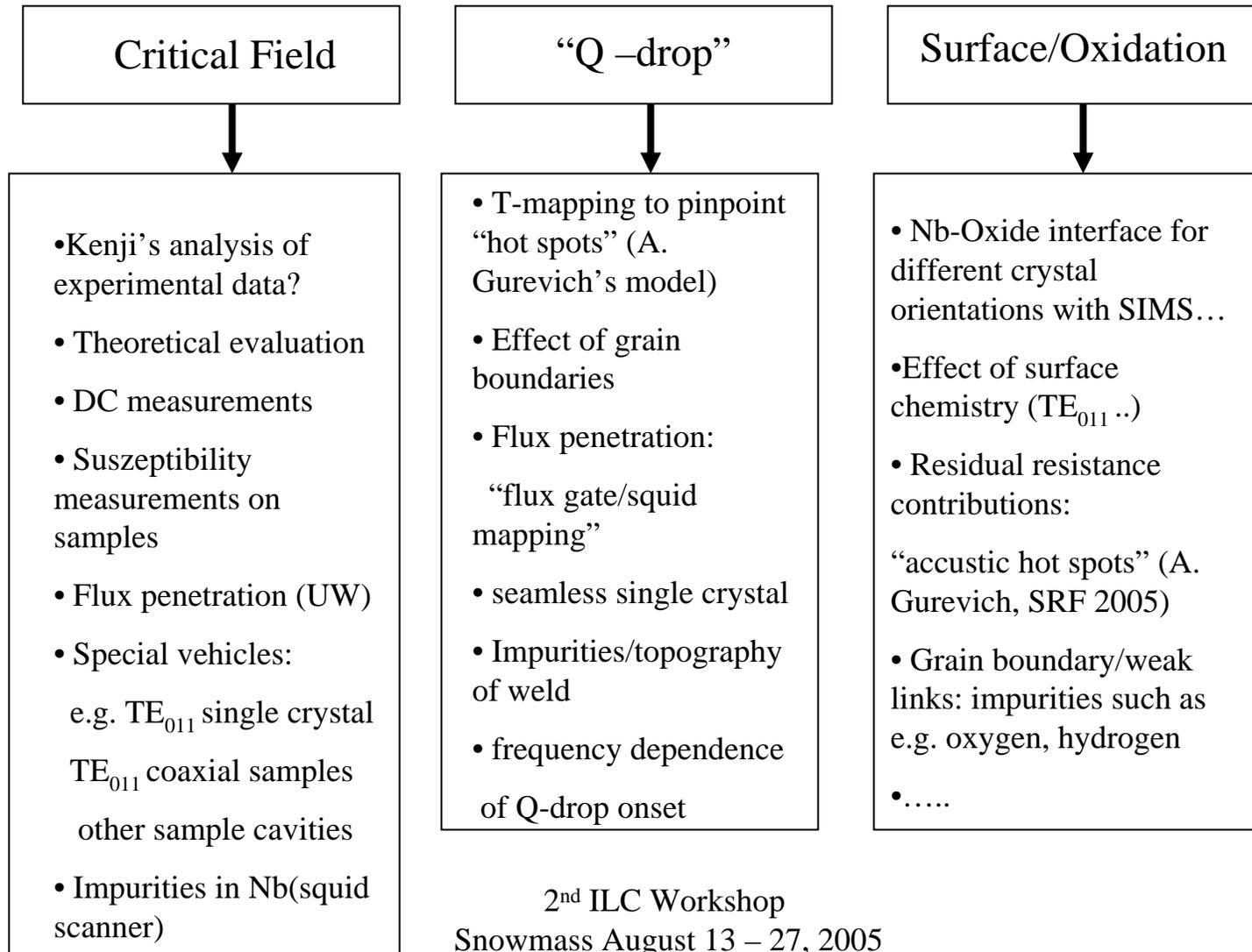
# Nb/Cu clad Material[8]

## R&D Topics

- How will the end groups be handled?  
Composite material, solid Nb, sputtered Nb flanged with sc joint?
- How will the He-vessel be handled? End dish to beam pipe?
- Complete cavities with end groups need to be fabricated and tested
- Test in module, cooldown uniformity?
- [Is “pipe-cooling” a possible concept?]
- Can the Lorentz force detuning be reduced? How can one vary the Cu thickness?

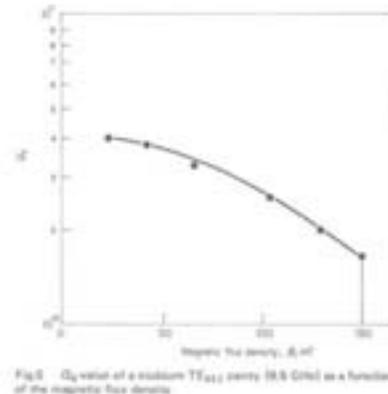
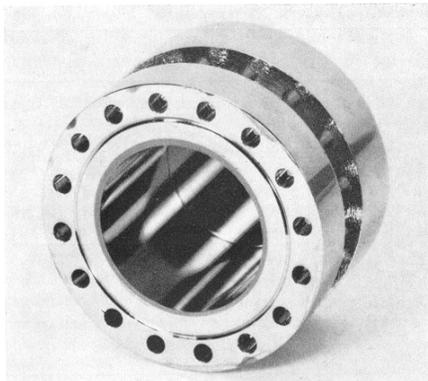
# Basic R&D: Understanding Physics

- There are 3 main issues, probably interconnected



# Critical field

- Analysis of experimental data by K.Saito suggest a limiting field of  $H \sim 180 \text{ mT}$  for high purity defect-free niobium
- Further verification could be done with e.g.
  - $\text{TE}_{011}$  cavity, single crystal, seamless (see Siemens cavity), X-band  $H \sim 159 \text{ mT}$  (K. Schnitzke et al; Phys. Lett 45A(1973)241)



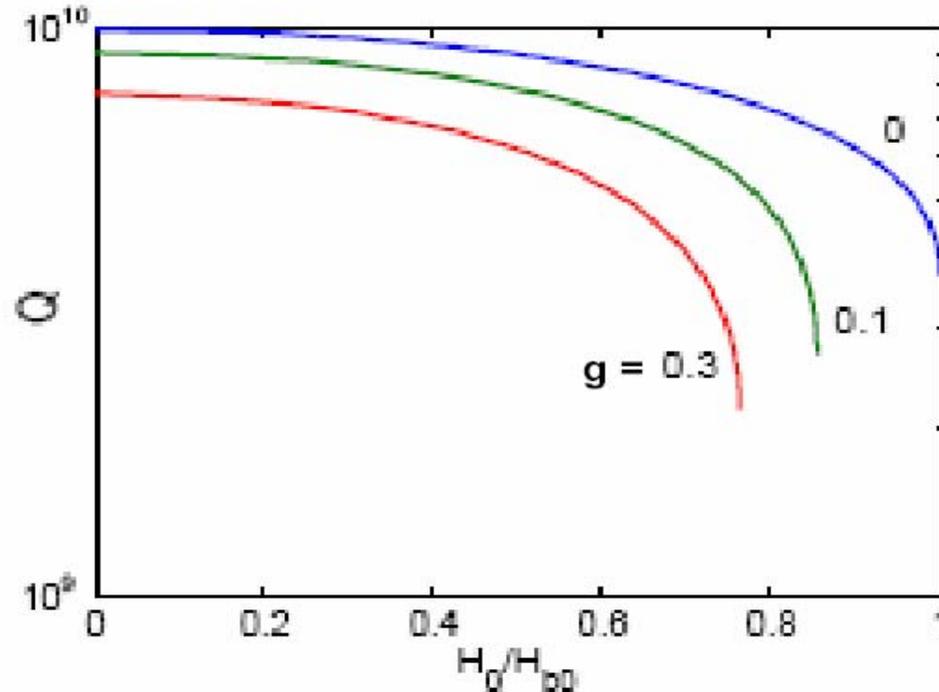
- Coaxial samples in coaxial  $\text{TE}_{011}$  cavity can also be used for different material and treatments
- Pulsed rf critical field measurements at 11.4 GHz (I.Campisi)

# Q-drop [1]

- Q-drop is common to BCP, EP and Single crystal cavities in high RRR niobium
- The “onset” field increases with increased grain size (reduced # of grain boundaries?)
- The baking effect is different in “fine grain” niobium treated by BCP and EP; it is similar for increased grain size (e.g. after post purification @  $T > 1250\text{C}$ )
- “Air baking “is less effective than “UHV” baking, but more/newer data available from B. Visentin (SRF 2005)

# Q – drop[1][A. Gurevich,SRF 2005]

**Q(H) for the linear BCS+hotspots ( $\Gamma_n = 0$ )**

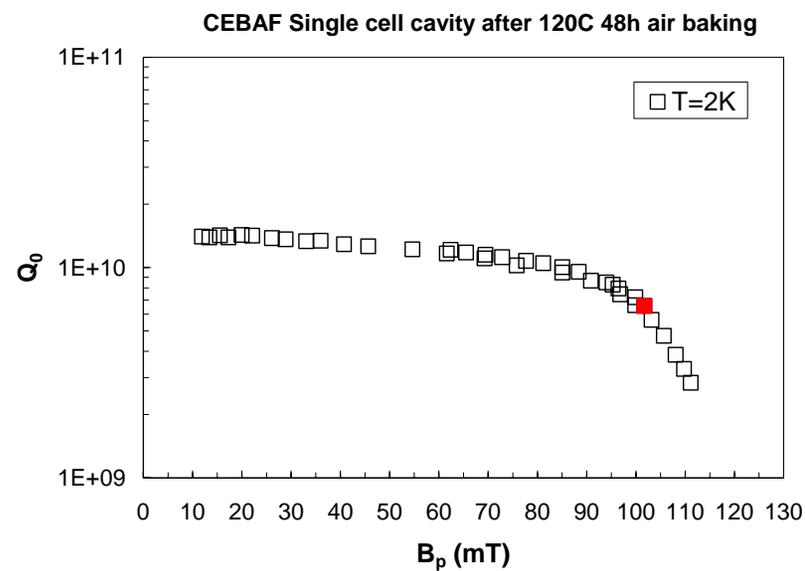
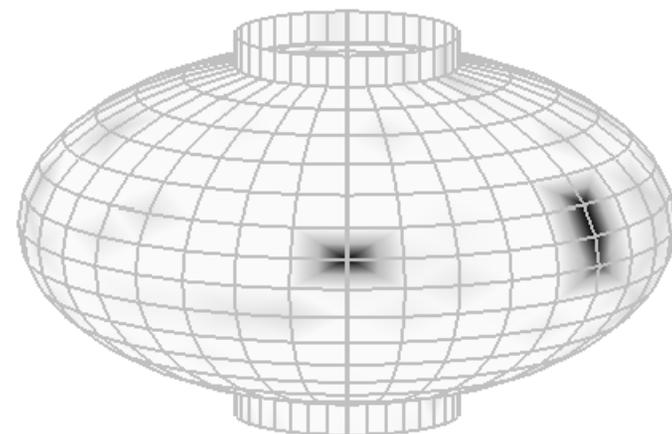
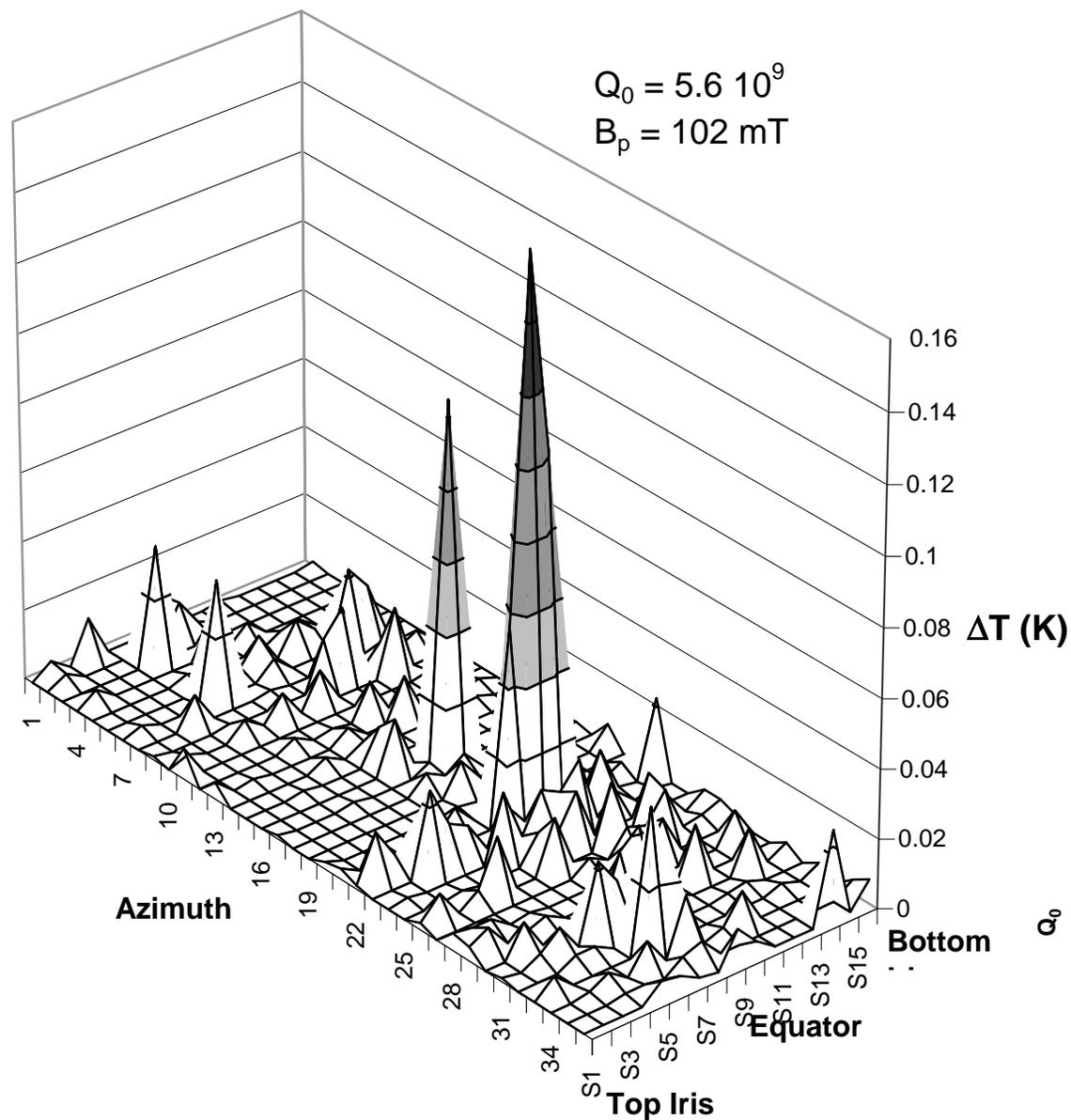


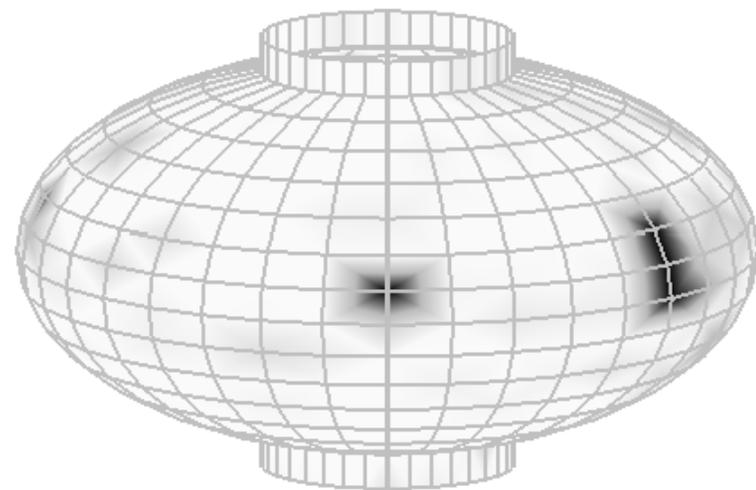
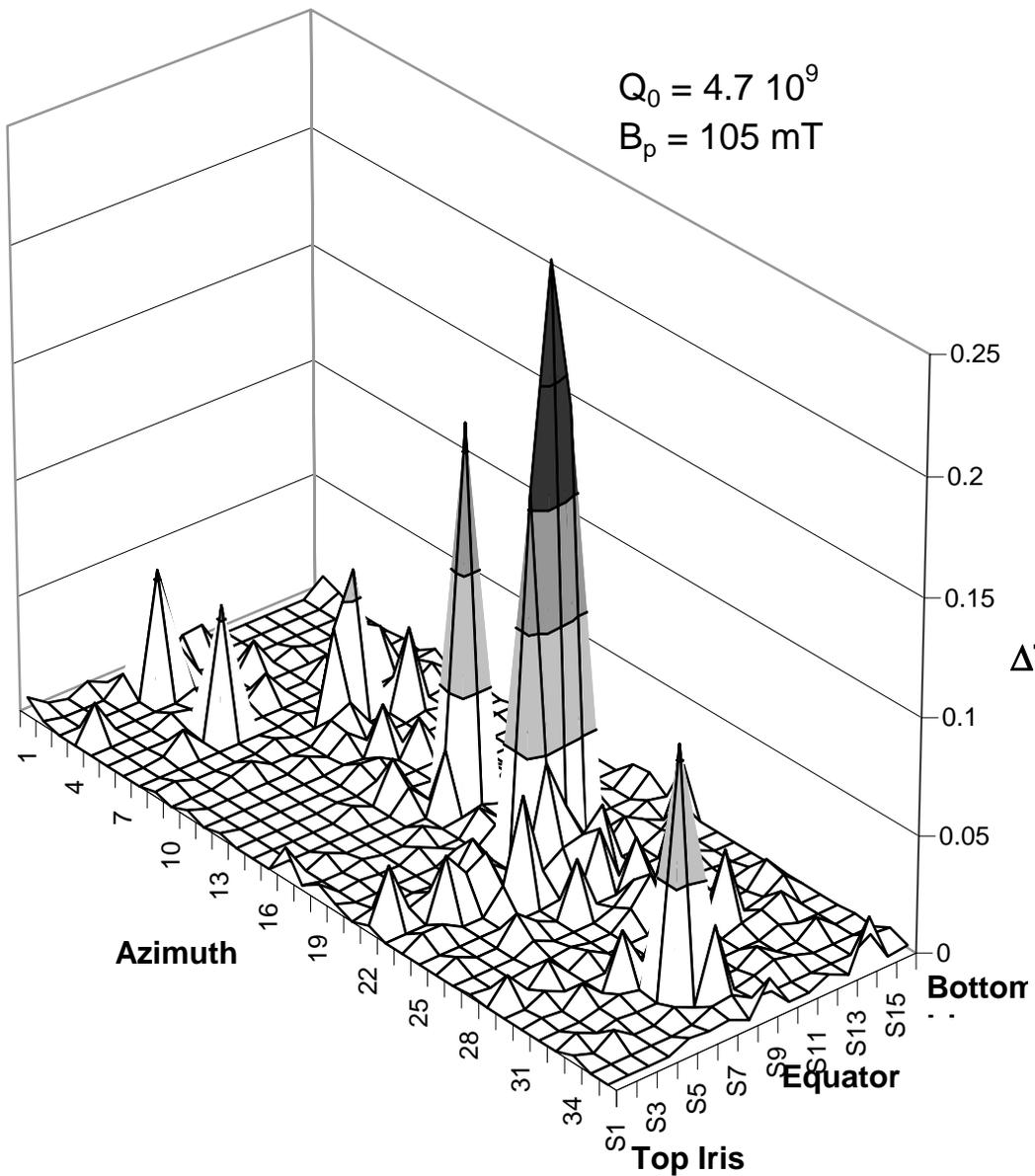
Hotspots reduce the breakdown field:

$$H_b \cong \left(1 - \frac{\sqrt{g}}{2}\right) H_{b0},$$

Hotspots increase the high-field Q slope:

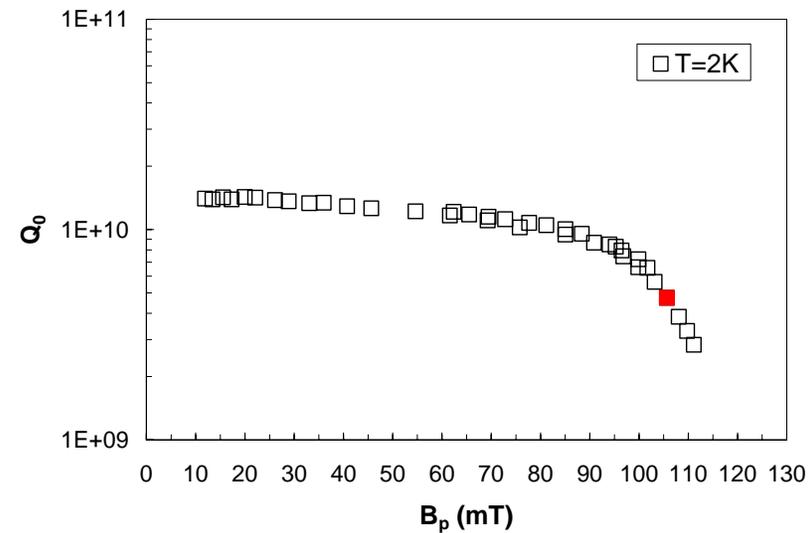
$$\frac{Q_0}{Q_b} = \frac{(1 + \sqrt{g})e}{1 + g} > e$$

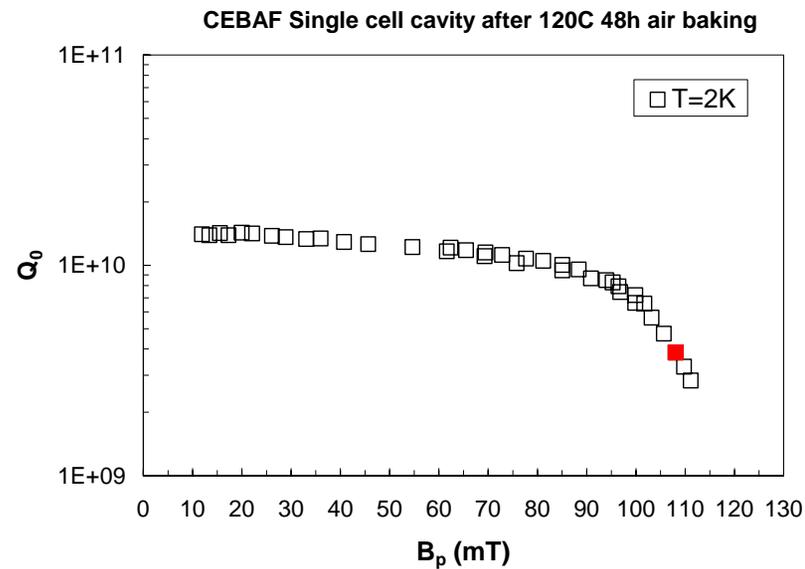
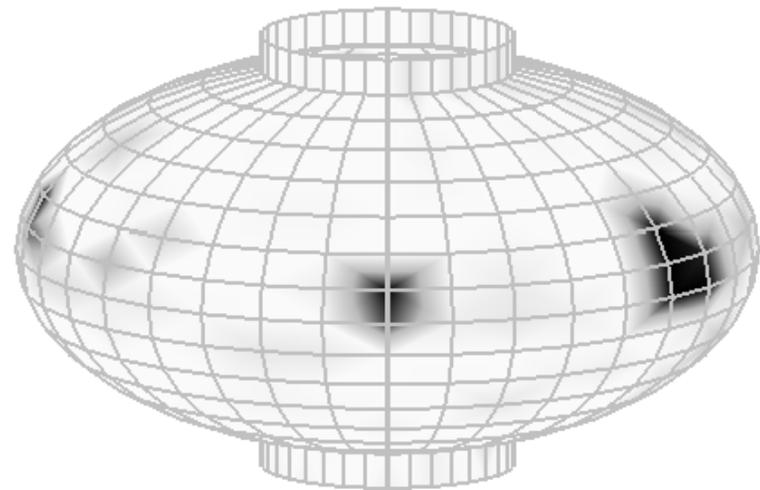
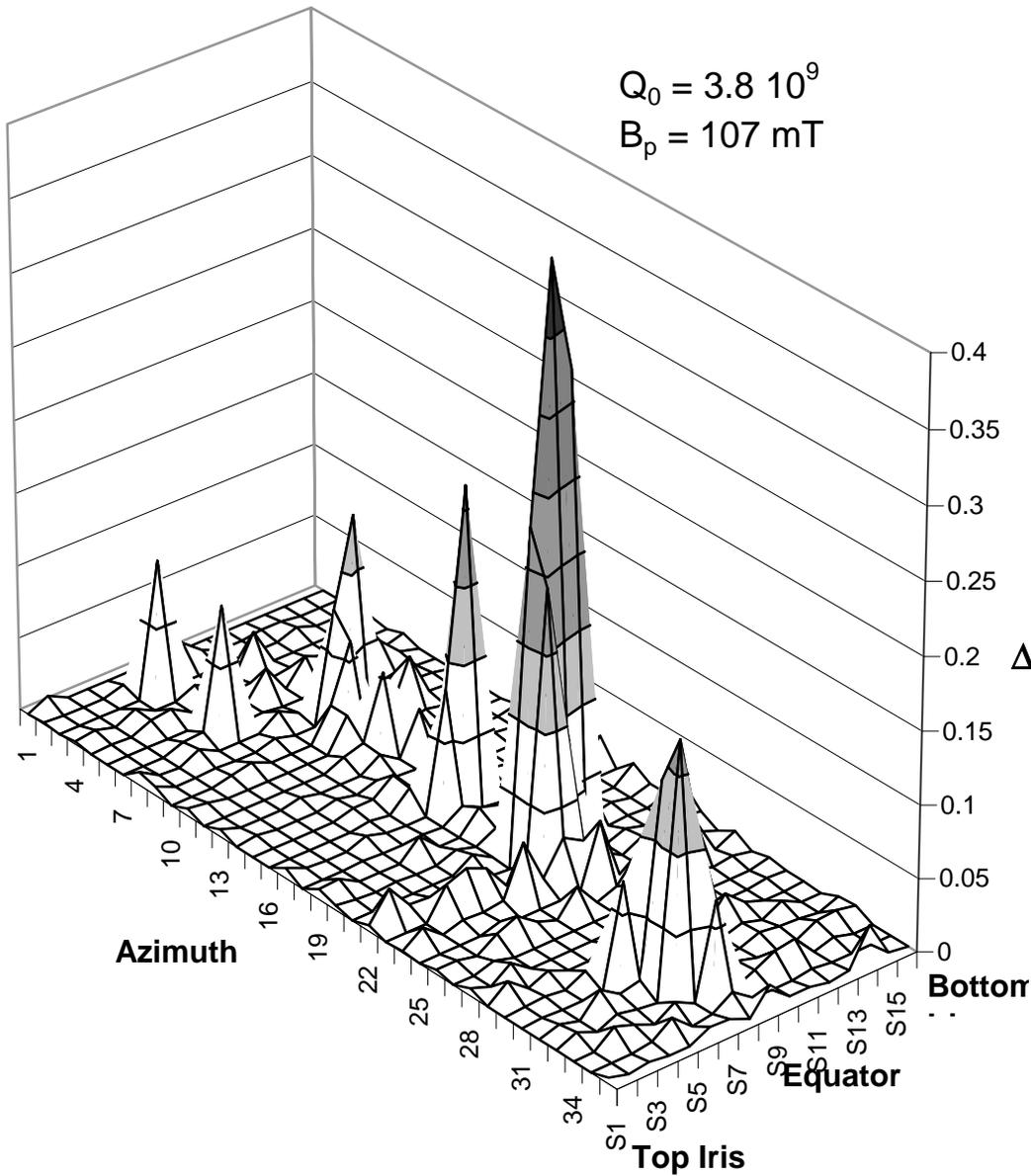




$\Delta T \text{ (K)}$

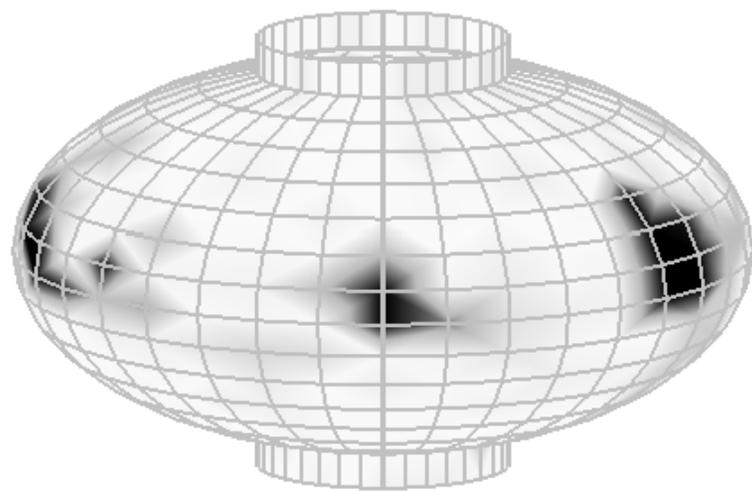
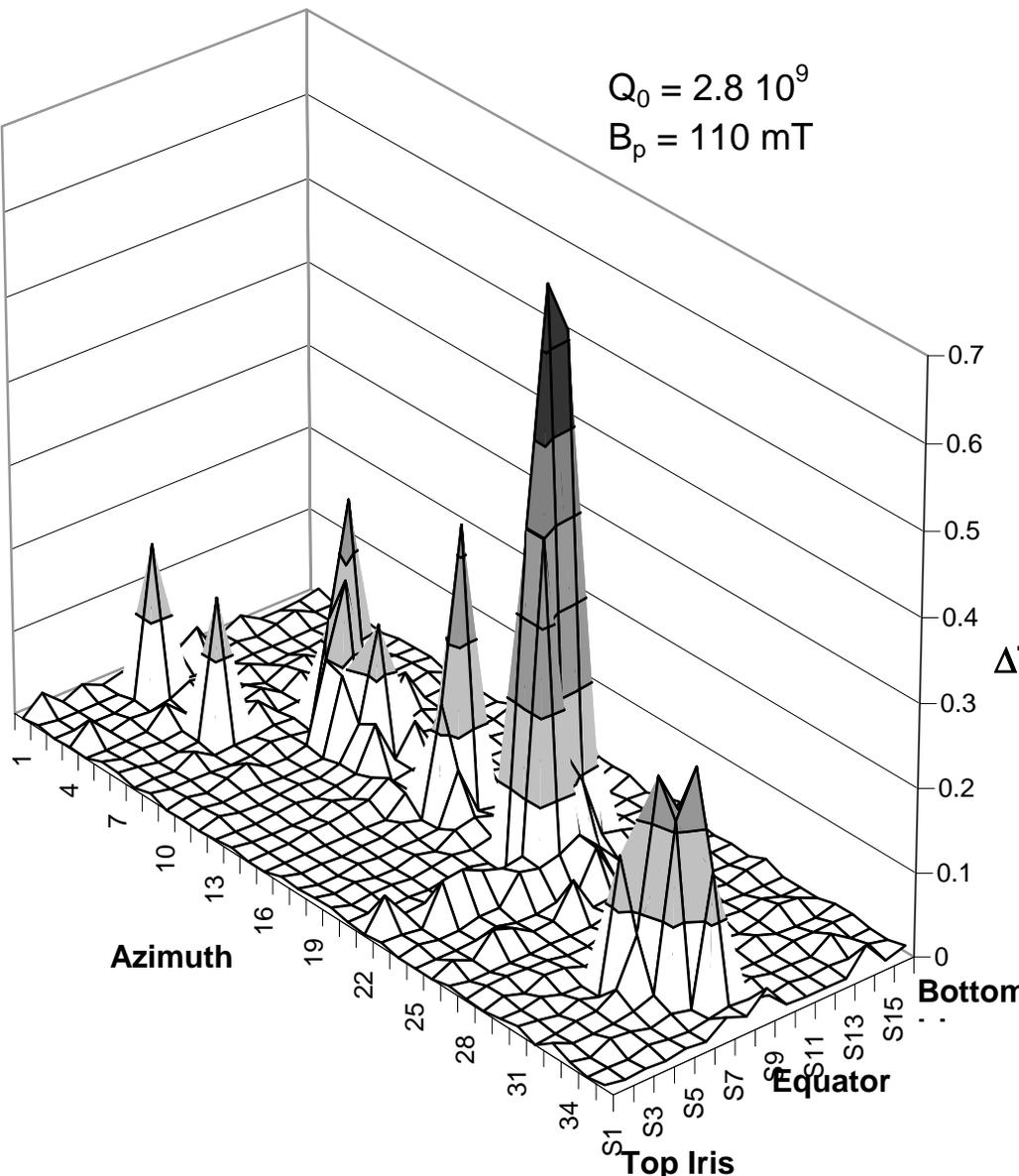
CEBAF Single cell cavity after 120C 48h air baking





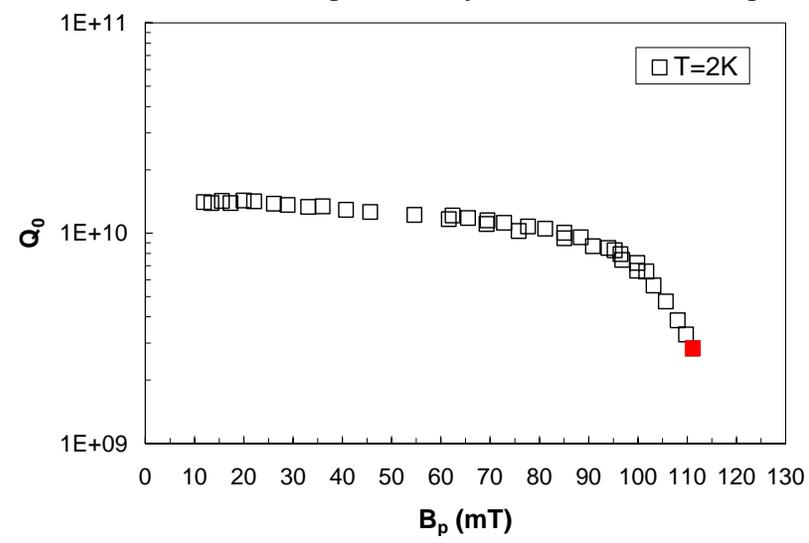
$$Q_0 = 2.8 \cdot 10^9$$

$$B_p = 110 \text{ mT}$$



$\Delta T$  (K)

CEBAF Single cell cavity after 120C 48h air baking



# Q – drop[3][A. Gurevich,SRF2005]

## Conclusions

- Ultimate cavity performance (in the absence of vortex penetration) is limited by nonlinear BCS pairbreaking and heating effects.
- Acoustic resonances and mechanisms of the residual resistance
- Hotspots limit the high-field cavity performance:
  - New mechanism of nonlinearity, which can offset the BCS nonlinearity,
  - Reduce the breakdown field
  - Increase the high-field Q slope
- Mechanisms of hotspot formation
  - Acoustic hotspots
  - Vortex penetration along GBs
  - Nonuniform surface oxide layers

## Challenges

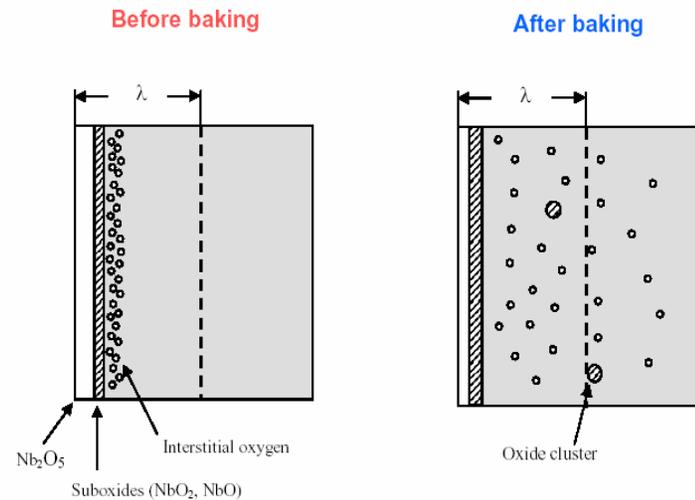
- Understanding nonequilibrium superconductivity and impurity surface scattering on nonlinear BCS resistance and rf breakdown
- Dynamics of vortex penetration and dissipation in rf field

# Q – drop[2]

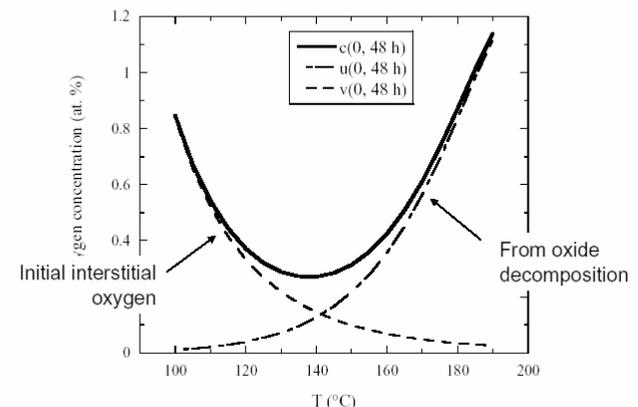
G. Ciovati (SRF 2005):

- Improved oxygen diffusion model taking into account the decomposition of the oxide layer
- Oxygen dilution changes  $\kappa$  of material to lower values,  $\rightarrow$  larger onset fields for Q-drop
- Smoother surface provides Surface barrier for flux penetration

## Schematic of the Nb surface



Oxygen concentration at the surface as function of baking temperature



Optimum baking temperature: lowers O conc. near the surface

# Q – drop[4]

- Proof “Hot Spot” Model :Suggestion was made(P.Bauer):
  - T-map “hot spot”
  - Cut cavity apart and analyze with e.g. Atom probe Tomography
  - Since “hot spots” on T-maps are near equator weld, one should investigate weld prior to cavity cutting and look for differences
- Flux penetration at grain boundaries
  - Superimpose a dc magnetic field (dc current through cavity walls) on the rf field – fluxons in penetration depth are moved by dc current and add to resistance (G. Ciovati)
  - Check flux penetration as function of surface conditions
- Frequency dependence of Q-drop onset :
  - No Q-drop observed at 9.5 GHz up to 155 mT ( Pfister, Cryogenics, Jan 1976, p.17) in reactor grade Nb ( single crystal?)
  - Measure f-dependence with e.g. coaxial cavity

# Q – drop[5]

- Oxygen diffusion model
  - Generate a “oxygen-free” niobium surface by “in situ” heat treatment at high temperatures in UHV (e.g. F. Palmer, 3<sup>rd</sup> SRF Workshop)
  - Introduce in a controlled way oxygen into the penetration depth, e.g. ion implantation?

# Surface/Oxidation[1]

- The goal is to link features of the metal/oxide interface to performances of cavities
- However, it is known that cavity surfaces are non-uniform (T-maps) and the challenge is to draw conclusions from at most mm<sup>2</sup> size spots investigated by surface analysis to m<sup>2</sup> cavity areas.
- Nevertheless, several areas seem of interest to explore:
  - Oxidation behavior of single crystal niobium of different crystallographic orientation compared to fine grain niobium oxidation
  - Impurities in grain boundaries such as oxygen, carbon, nitrogen..
- Atom Probe Tomography (see D.Seidman, SRF 2005) seems to be a new powerful tool in addition to standard methods such as e.g.SIMS (work in progress FNAL/Northwestern/UW)

# Surface/Oxidation[2]

## Conclusions and next steps

---

- Nanochemical, atomic scale analyses of the oxide surface and of the near-surface bulk niobium are being performed
  - “Smooth” transition from surface  $\text{Nb}_2\text{O}_5$  to  $\text{Nb}_2\text{O}$  (and into the bulk Nb)
  - Ability to detect small number of contaminant atoms in the oxide surface and in the near-surface bulk niobium
  - Levels of oxygen in the near-surface bulk niobium (metal) of 5-10 atomic percent, which is consistent with bulk Nb-O phase diagram
- More analysis to come
  - Interpretation of mass spectra
    - Improved analysis conditions
  - Improved specimen preparation techniques (reliability and repeatability)
    - Focused ion beam (FIB) milling and/or femtosecond laser ablation
- Many classes of samples

*David N Seidman  
13 July 2005*



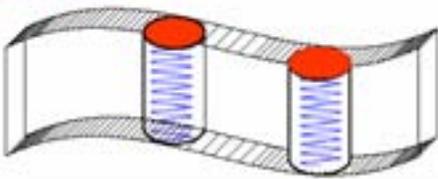
# Surface/Oxidation[3]

- Residual Resistance contribution from “acoustic hot spots” (A. Gurevich, SRF 2005)
- Verification by changing outer surface of the cavity after test

**Acoustic hotspots**

Distribution function of acoustic resonance frequencies due to:

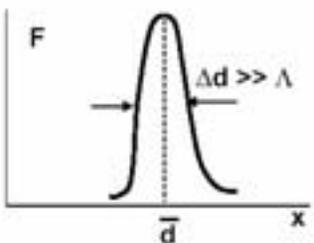
1. Smooth thickness wall variation by  $\Delta d \gg \Lambda \sim 1 \mu\text{m}$  on the scale -  $d = 2-3 \text{ mm}$
2. Spectrum of rf frequencies in coupled cavities



Hotspot in the regions where the local thickness  $d(x,y)$  satisfies the resonance condition  $n\Lambda = d$

Averaging with the thickness distribution function  $F(x)$ :

$$\bar{R}_i = R_{i0} \int_0^\infty \frac{\sinh(\gamma x / s) F(x) dx}{\cosh(\gamma x / s) - \cos(2\pi x / s)} \cong \sqrt{2} R_{i0}$$



Averaged  $R_i$  is of the order of  $R_{i0}$  and depends neither on the small  $\gamma$  nor the shape of  $F(x)$ . Effect of sound scattering and generation of Rayleigh surface waves

# Surface/Oxidation[4]

- Residual resistance: understanding low and medium field Q-slope
- Ongoing studies at Jlab utilizing T-mapping on large grain material with varying grain size, effect of grain boundaries

# RF SC Theory

- Calculations to estimate surface resistance contribution due to **magnetic vortex penetration** in RF fields (possibly Fermilab/University of Wisconsin, A. Gurevich, JLab – G. Ciovati?)
- Estimate surface resistance contribution of **weak-links (grain-boundaries, patches with suppressed superconductivity)** (possibly Fermilab/University of Wisconsin, A. Gurevich, JLab – G. Ciovati?)
- **Linear and Non-linear BCS resistance in the clean and dirty limits** (possibly Fermilab/University of Wisconsin, A. Gurevich)